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26 October 1966

To: V. Webb ✓  
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Thru: [REDACTED]

From: [REDACTED]

Subject: MISSION 1028-1 AND 1028-2 FINAL REPORT

Enclosed is the Final Performance Evaluation Report  
for Mission 1028-1 and 1028-2.

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Advanced Projects

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CORONA J

PERFORMANCE EVALUATION REPORT

MISSION 1028-1 and 1028-2

FTV 1610, J-26

9 September 1966

Approved: 

Mgr.

Advanced Projects

Approved: 

Mgr.

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## FOREWARD

This report details the performance of the payload system during the operational phase of the Program [REDACTED] Flight Test Vehicle 1610.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Level of Effort and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1028-1 and 1028-2 which was launched on 24 December 1965.

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## INTRODUCTION

This report presents the final performance evaluation of Missions 1028-1 and 1028-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-26 payload system and to identify the source of in-flight anomalies.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and ITEK at the facilities of NPIC and AFSPPF. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, values and MTF/AIM resolution are produced by AFSPPF. The vehicle attitude error values, frame correlation times are made at NPIC who also supply the Processing Summary and MTF/AIM resolution reports published by [REDACTED]

Computer programs developed by A/P are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

**SECTION I**  
**SYSTEM PERFORMANCE**

**A. MISSION OBJECTIVES**

The payload section of Mission 1028, placed into orbit by Flight Test Vehicle #1610 and LV-2A booster #451, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipments. Figure 1-1 presents an inboard profile of the J-26 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. The planned mission was two, 5 day photographic periods with no inactive period.

**B. MISSION DESCRIPTION**

The payload was launched from Vandenberg Air Force Base (VAFB) at 2106:15 Z (1306:15 PST) on 24 December 1965. Ascent and injection were normal and the achieved orbit was within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. Mission 1028-1 consisted of a five day photographic operation and was air recovered on 29 December 1965. Mission 1028-2 was air recovered, after a four day operation, on 2 January 1966. The -2 mission was limited by battery life.

The comparison of the planned and actual orbit parameters is tabulated as follows:



**ORBITAL PARAMETERS**

<u>Parameter</u>	<u>Predicted</u>	<u>Orbit 1 Actuals</u>
Period (Min.)	90.856	90.84
Perigee (N. M.)	99.99	97.44
Apogee (N. M.)	244.71	244.35
Inclination (Deg.)	79.99	80.01
Perigee Latitude (Deg. N.)	19.11	19.06
Eccentricity	0.02008	0.02033

**C. PANORAMIC CAMERAS**

The Master and Slave panoramic cameras operated throughout both missions with no significant problems and produced excellent photographic coverage. The cloud cover observed in the photography averaged 30% for the entire flight.

**D. STELLAR-INDEX CAMERAS**

The S/I Camera #D77 operated satisfactorily on the -1 mission. The stellar photography on S/I #D74 was partially degraded by light fog due to the index camera shutter failing to open throughout the -2 mission.

**E. OTHER SUBSYSTEMS**

The telemetry instrumentation, command, thermal control, clock, pressure make-up and recovery subsystems performed satisfactorily throughout both missions.

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SCHMATIC INBOARD PROFILES - CORONA J SYSTEM

MISSION 1028

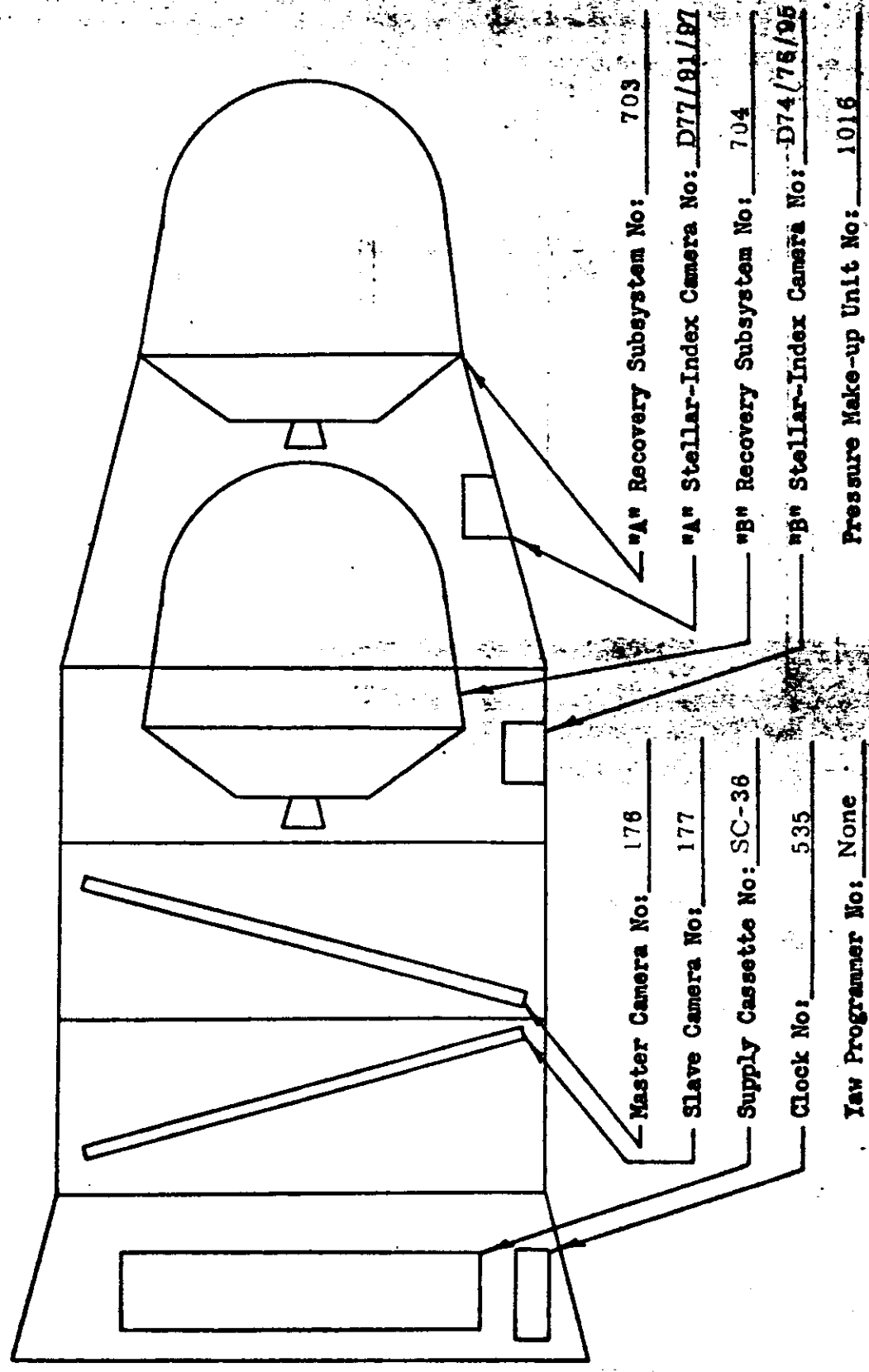


FIGURE 4-1

SECTION 2  
PRE-FLIGHT SYSTEMS TEST

A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

The J-26 payload system consisting of panoramic instruments 176 and 177 was in the TASC chamber at Sunnyvale for environmental testing during 30 July to 6 August 1965. Testing consisted of 14 orbits of operations in both the "A" and "B" modes with a vehicle deactivate/reactivate sequence conducted in between.

The lowest internal camera pressure experienced was 1.2 microns in the "B" mode. Corona was experienced from the input metering roller, however it did not exceed the specification tolerances.

Dynamic operation of both instruments was satisfactory during both "A" and "B" modes. Cycle rates were within  $\pm 1.5$  percent for the operations in the upper portion of the ramp.

Both stellar/index units performed satisfactorily.

The clock/IRIG "C" correlation indicated a drift of approximately 2 milliseconds/hour during the "A" and "B" modes and a discrepancy of approximately 1 second after the clock recycled.

The TLM instrumentation was satisfactory except for the instrument #2 cycle counter which randomly lost counts during the "B" mode operations.

The pressure-make-up system operated normally with an average gas consumption rate of 6.6 psi/min.

Both "A" and "B" recovery sequences were satisfactory. Both instruments stowed properly for the "A" mode C & W operation.

The deactivate/reactivate capability was successfully demonstrated between the "A" and "B" operations. Both instruments stowed normally for the deactivate operation sequence.

3. Panoramic Camera Performance

The dynamic performance of both panoramic instruments was satisfactory as observed on the TLM monitors for Center of Format switch, lens rotation, 99/101 clutch, and film transport.

The average 99/101 percent clutch ratios for both instruments were 6/6. The ratios did not vary by more than one on either side of the average value during the entire test.

The cycle rate data for all of the stereo operations are listed in Table 2-1. Instrument cycle rate predictability was +1.5 percent for the operations near the top of the ramp and +3 percent overall. The instruments operated within +1 percent of each other. During the "A" operations instrument #2 generally ran faster while for the "B" operations the opposite was true.

The supply metering monitor indicated that the lens of both instruments had an abnormally long coast period during a fast operation in the "A" mode.

The instruments operated for 5 cycles during the deactivate sequence. The cycle periods were 6.850 seconds for instrument #1 and 6.740 seconds for the #2 instrument.

4. Stellar/Index Performance

Normal stellar/index operations were observed on TLM monitors

for both units. The shutter and platen events occurred in proper relation to each metering cycle. Index and stellar metering ratios were consistently 7/3 and 8/3 throughout all operations observed with an occasional 6/3.

5. Clock Performance

Several clock readouts during the test were correlated with the IRIG "C" time. The results are listed on Table 2-2.

The results indicated a large discrepancy (approximately 1 sec.) following the clock (S/N 536) recycle. Also a drift of approximately 2 milliseconds per hour was observed. This clock was replaced by clock S/N 535 for flight.

6. Instrumentation Performance

The TLM instrumentation was satisfactory except for (1) the instrument #2 cycle counter which randomly lost counts during the "B" mode operations, and (2) a dirty commutator on the I/R monitor also observed during "B" operations.

The instrument #2 counter lost counts going from the "9" to the "0" position. The counter dropped 102 counts in approximately 2600 cycles.

7. Pressure Make-up System Performance

Satisfactory operation was observed for the PMU unit. The average consumption for the "A" operations was 6.6 psi/min.

8. Temperature Summary

Average instrument temperature for several orbits in the "A" and "B" mode are listed below:

<u>ORBIT</u>	<u>"A" Mode</u>			<u>"B" Mode</u>		
	<u>1</u>	<u>9</u>	<u>14</u>	<u>1</u>	<u>9</u>	<u>14</u>
Inst. #1	87	81	73	66	45	58
Inst. #2	85	74	69	62	42	62

J-26 176/177 TASC TEST OPERATIONS 7-31 TO 8-9-65

REV/MODE	RAMP	T.U.R.	INST 176			INST 177			176/177 DIFF.
			ACT.	NUM.	DEV.	ACT.	NUM.	DEV.	
1 A	7 7	390	3.490	3.515	0.72	3.508	3.496	-0.11	0.29
1 A	7 7	2275	2.945	2.588	1.66	2.555	2.580	0.96	0.39
2 A	4 1	2130	2.160	2.196	1.64	2.150	2.197	2.12	-0.46
2 A	5 8	725	2.850	2.884	1.17	2.850	2.872	0.75	-0.00
3 A	5 8	1550	2.400	2.445	1.85	2.400	2.439	1.62	-0.00
4 A	7 7	2280	2.550	2.591	1.57	2.550	2.583	1.26	-0.00
4 A	8 2	335	5.000	5.061	1.20	4.980	5.037	1.13	-0.40
5 A	8 2	1725	2.200	2.231	1.38	2.190	2.234	1.98	-0.45
5 A	8 2	2245	2.250	2.291	1.80	2.250	2.288	1.56	-0.30
5 A	11 1	1582	2.400	2.446	1.87	2.400	2.440	1.64	-0.00
6 A	11 1	2032	2.260	2.296	1.59	2.260	2.293	1.44	-0.00
6 A	5 8	1091	2.660	2.690	1.13	2.650	2.681	1.15	-0.38
6 A	5 8	1446	2.450	2.437	1.48	2.450	2.480	1.22	-0.00
7 A	7 7	1181	2.845	2.863	0.63	2.840	2.851	0.39	-0.18
7 A	7 7	1591	2.510	2.562	2.04	2.515	2.555	1.55	0.20
8 A	7 7	2531	2.735	2.768	1.21	2.735	2.758	0.83	-0.00
8 A	4 1	1016	2.690	2.701	0.42	2.685	2.692	0.25	-0.19
9 A	4 1	3211	3.475	3.521	1.31	3.470	3.502	0.92	-0.14
9 A	11 1	891	4.360	4.358	-0.04	4.360	4.334	-0.59	-0.00

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TABLE 3-1

REV/MODE	RAMP	T.U.R.	INST 176			INST 177			176/177 DIFF.	
			ACT.	NOM.	DEV.	ACT.	NOM.	DEV.		
10	A	11 1	1881	2.240	2.273	1.43	2.240	2.269	1.30	-0.00
10	A	11 1	2971	4.520	4.571	1.12	4.510	4.547	0.81	-0.22
10	A	7 7	141	3.590	3.625	0.98	3.570	3.606	0.99	-0.56
11	A	7 7	1911	2.450	2.490	1.59	2.450	2.483	1.33	-0.00
11	A	7 7	2281	2.560	2.591	1.20	2.550	2.583	1.28	-0.39
12	A	8 2	1156	2.940	2.936	-0.12	2.940	2.924	-0.56	-0.00
12	A	8 2	846	3.665	3.654	-0.31	3.640	3.633	-0.18	-0.68
13	A	11 1	1978	2.263	2.279	0.72	2.250	2.276	1.16	-0.57
14	A	11 1	3082	5.120	5.123	0.06	5.080	5.099	0.38	-0.78
1	B	7 7	385	3.520	3.518	-0.05	3.515	3.499	-0.45	-0.14
1	B	7 7	2210	2.570	2.556	-0.53	2.560	2.549	-0.44	-0.39
2	B	4 1	2130	2.170	2.196	1.19	2.177	2.197	0.89	0.32
2	B	5 8	732	2.860	2.880	0.70	2.870	2.868	-0.07	0.35
3	B	5 8	1550	2.430	2.445	0.63	2.430	2.439	0.39	-0.00
4	B	7 7	2280	2.610	2.591	-0.75	2.616	2.583	-1.30	0.23
4	B	8 2	341	5.105	5.046	-1.17	5.115	5.022	-1.85	0.20
5	B	11 1	1460	2.636	2.613	-0.89	2.646	2.604	-1.60	0.38
5	B	11 1	2040	2.300	2.300	-0.01	2.317	2.296	-0.90	0.74
6	B	5 8	1090	2.713	2.691	-0.81	2.720	2.682	-1.43	0.26
6	B	5 8	1445	2.497	2.487	-0.39	2.507	2.481	-1.06	0.40
7	B	7 7	1205	2.860	2.840	-0.72	2.875	2.828	-1.66	0.52
7	B	7 7	1591	2.575	2.562	-0.50	2.570	2.555	-0.61	-0.19

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TABLE 3-1

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REV/MODE	RAMP	T.U.R.	INST 176			INST 177			176/177 DIFF.	
			ACT.	NOM.	DEV.	ACT.	NOM.	DEV.		
8	B	7 7	2531	2.777	2.768	-0.31	2.780	2.758	-0.81	0.11
8	B	4 1	1014	2.740	2.705	-1.30	2.740	2.695	-1.67	-0.00
9	B	4 1	3211	3.545	3.521	-0.67	3.550	3.502	-1.36	0.14
9	B	11 1	891	4.430	4.358	-1.65	4.440	4.334	-2.44	0.23
10	B	11 1	1881	2.290	2.273	-0.77	2.297	2.269	-1.21	0.31
10	B	11 1	2970	4.680	4.567	-2.48	4.680	4.542	-3.03	-0.00
10	B	7 7	140	3.660	3.626	-0.95	3.660	3.606	-1.50	-0.00
11	B	7 7	1910	2.503	2.490	-0.54	2.507	2.483	-0.96	0.16
11	B	7 7	2280	2.610	2.591	-0.75	2.613	2.583	-1.18	0.11
12	B	8 2	1155	2.987	2.939	-1.64	2.997	2.926	-2.43	0.35
12	B	8 2	845	3.710	3.656	-1.47	3.705	3.636	-1.90	-0.13
13	B	4 1	2630	2.425	2.404	-0.88	2.430	2.399	-1.31	0.21
13	B	11 1	1973	2.293	2.278	-0.64	2.290	2.275	-0.65	-0.13
4	B	11 1	3078	5.170	5.102	-1.34	5.170	5.078	-1.82	-0.00
14	B	1 11	3680	2.290	2.283	-0.31	2.287	2.280	-0.32	-0.13

DEV. AND DIFF. ARE IN PERCENT  
 THE (-) SIGN INDICATES THAT THE INST IS SLOWER THAN  
 PREDICTED OR THAT INST 1 IS SLOWER THAN INST 2

TABLE 2-1

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**CLOCK/IRIG "C" CORRELATION**

**"A" MODE**

<u>Rev.</u>	<u>IRIG "C" TIME</u>			<u>CLOCK TIME</u> <u>(Seconds)</u>	<u>ERROR</u> <u>(Seconds)</u>
	<u>Day</u>	<u>Hour</u>	<u>Min</u> <u>Sec</u>		
1	212	8	8 38.840	409,553.463	--
6	213	9	1 20.830	499,115.468	+ .008
11	213	16	15 31.080	526,965.712	.000
12	214	13	58 54.050	66,498.754*	+ .986
14	215	8	39 57.575	133,762.253	+ .959

**"B" MODE**

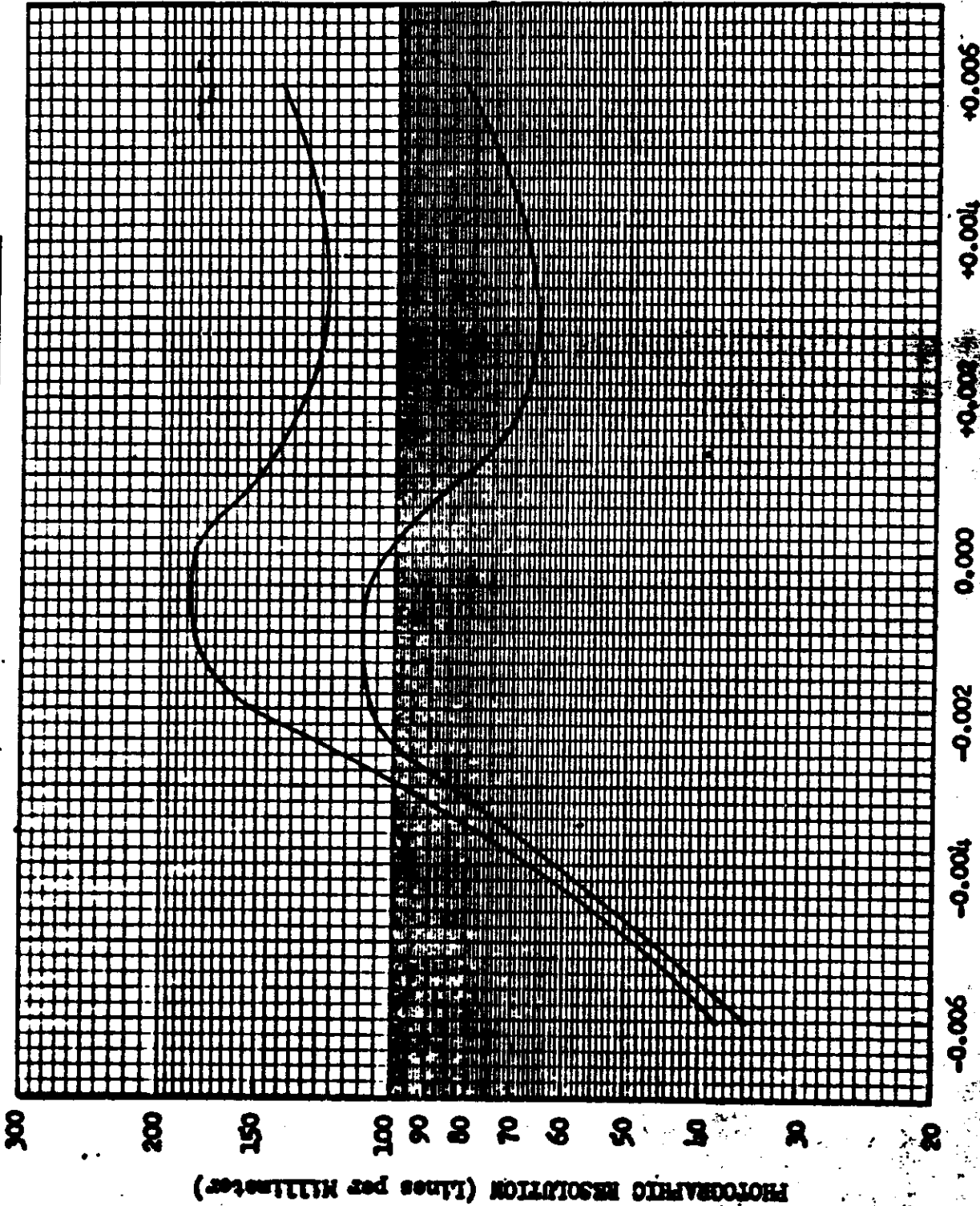
1	215	12	35 05.580	341,307.323	
4	216	8	44 42.000	413,889.975	.033
5	216	11	29 51.030	423,792.795	.038
6	216	12	59 48.105	429,189.866	.042
7	216	14	25 38.180	434,339.943	.040
10	217	8	31 1.275	499,463.001	.077

\*Clock recycled between Rev. 11 and 12.

TABLE 2-2

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PRE-FLIGHT DYNAMIC RESOLUTION



Camera No: 176

Payload No: J-26

Resolution (1/mm)

High Contrast: 180

Low Contrast: 109

Film Type: 3404

Test Date: 8/11/66

FIGURE 2-1

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PRE-FLIGHT DYNAMIC RESOLUTION

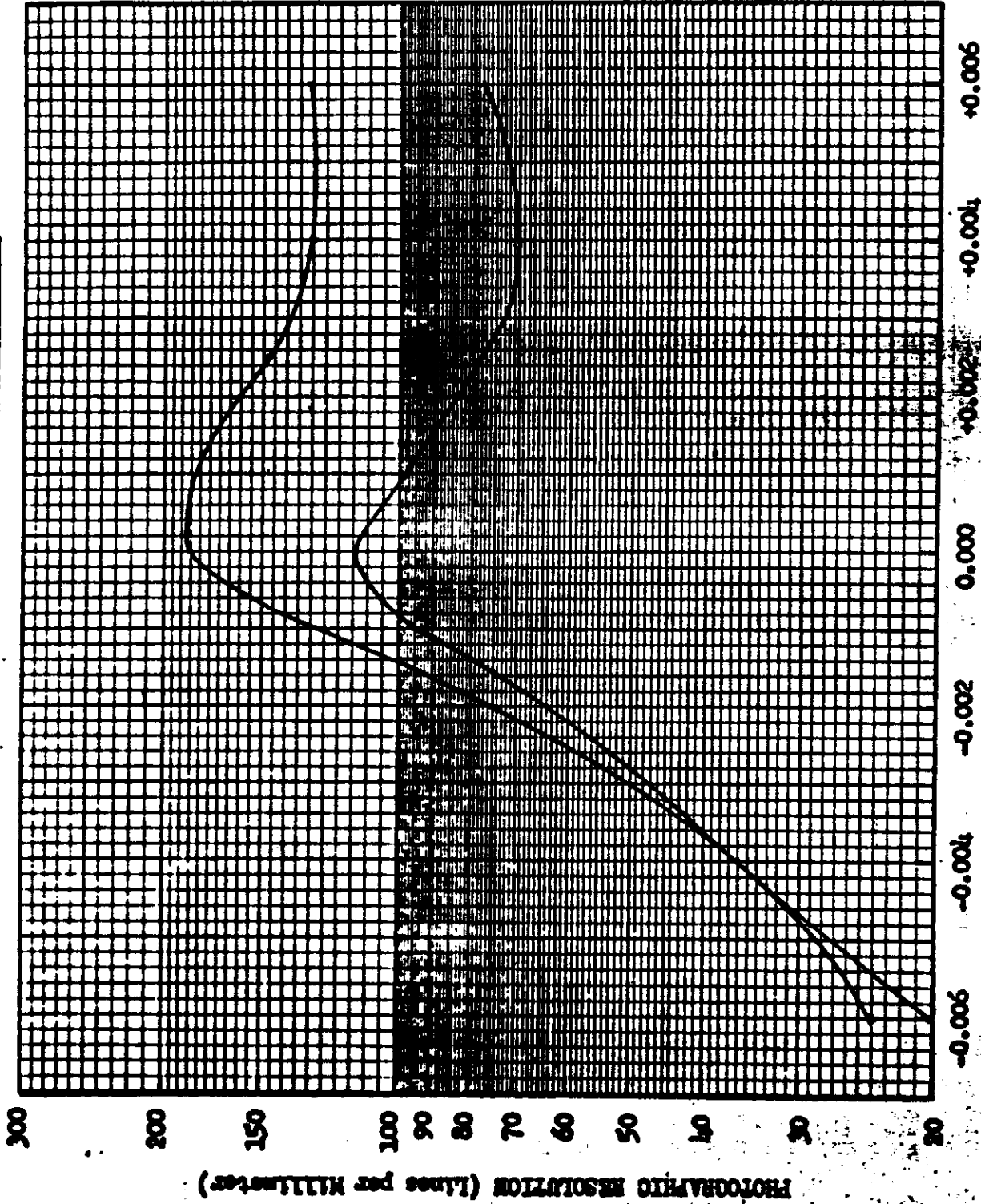


FIGURE 2-2

Camera No: 177  
 Payload No: J-26  
 Resolution (L/mm)             
 High Contrast: 186  
 Low Contrast: 114  
 Film Type: 304  
 Test Date: 8/11/65

PHOTOGRAPHIC RESOLUTION (lines per millimeter)

THROUGH FOCUS INCREMENTS (inches)

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### SECTION 3

#### FLIGHT OPERATIONS

##### A. SUMMARY

All launch, ascent and injection events occurred as programmed. Both Thor and Agena propulsion and guidance were normal. The desired orbit was achieved.

Both panoramic instruments operated satisfactorily throughout both missions. Average cycle rate differences from pre-flight calibrations indicated that both instruments ran approximately one percent slow.

The -1 Stellar/Index camera operated satisfactorily.

The -2 Stellar/Index camera operation was abnormal. An index shutter malfunction resulted in excessive over exposure of the index film during the -2 mission.

The clock system, instrumentation and command systems, and the PMU system functioned normally throughout the flight.

Both the -1 and -2 recovery systems were successfully recovered by air catch on orbits 81 and 144, respectively.

Results obtained from a power spectral density analysis of the vibration pickup data indicated overall rms g levels of 3.66 at ignition and 2.35 in the transonic region.

##### B. PANORAMIC CAMERA PERFORMANCE

Camera system dynamics were observed during several [REDACTED] acquisitions. Film transport was normal for both instruments. Cycle rate data, as shown on Table 3-1, indicates that both instruments were running approximately 1% slower than pre-flight calibrations. The instruments ran within 1% of each other throughout the flight. Average 99/101 clutch ratios for both instruments were 6 cycles in the 99 position and 6 cycles in the 101 position.

##### FMC Match

The achieved orbit was near nominal. The FMC match throughout the flight was within tolerance.

Panoramic Film Consumption

These data are based on cycle counter readings and nominal film supply.

	<u>Predicted</u>	<u>Actual</u>	
		<u>Master</u>	<u>Slave</u>
Pre-launch - Frames	100	110	110
-1 Mission - Frames	3000	2979	3007
-2 Mission - Frames	2949	2960	2932
Total Frames	6049	6049*	6049**

\* Depletion was predicted during Orbit 135 descending.

\*\* Depletion was predicted during Orbit 134 descending.

C. STELLAR/INDEX CAMERA PERFORMANCE

The -1 Stellar/Index camera operated normally during mission -1.

The -2 Stellar/Index camera did not function properly. The index film was excessively over exposed. Also the stellar film was intermittently fogged.

The TLM monitor for the index shutter, as observed on the day time engineering acquisitions, indicated that the shutter opened in the proper sequence at each seventh frame of panoramic camera operation. However, there is no way to determine from TLM the duration of the shutter open condition.

Smear pulses correlated with the index shutter monitor which indicates that the number 3 programmer and S/I control box were operating in the proper sequence.

D. INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

Instrumentation

The instrumentation system performed satisfactorily throughout both missions.

A + 35 G vibration pickup was installed on the forward pyro electrical box to monitor ascent levels. This special monitor performed satisfactorily.

#### Command System

The payload system responded normally to all stored and real-time commands. No operational problems were encountered during the flight.

#### E. CLOCK PERFORMANCE

The payload clock performance was satisfactory. The clock/system time correlation data obtained from the [redacted] acquisitions are included on Table 3-2.

#### F. PRESSURE MAKE-UP SYSTEM PERFORMANCE

The PMU system operated normally throughout the flight. Average gas consumption was 7.7 psi/min for a total instrument operate time of 245 minutes. The supply pressure dropped from 2660 psig at launch to 780 psig at the end of -2 mission.

The average consumption rate was 6.9 psi/min for the -1 mission and 8.4 psi/min for the -2 mission.

#### G. THERMAL ENVIRONMENT

The temperature data obtained from the [redacted] acquisitions are contained in Table 3-3. Average panoramic camera temperatures varied from 68 to 86° F during the flight. The actual system temperatures versus the predicted system temperatures for the major components are compared in Figures 3-1 to 3-3.

#### H. ASCENT VIBRATION

The vibration pick-up was installed on the pyro junction box cover in the recovery barrel. High activity occurred at launch ignition and in the transonic region. Results of a power spectral density analysis show overall rms g levels of 3.66 at ignition and 2.35 in the transonic region.

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J-26/1610 MISSION 1028 ENGINEERING OPERATIONS

REV/MODE	RAMP	T.U.R.	INST 176			INST 177			176/177 DIFF.	
			ACT.	CAL.	DEV.	ACT.	CAL.	DEV.		
09	A	8 2	82	5.448	5.560	2.02F	5.394	5.538	2.60F	-0.99
16	A	8 2	1688	2.270	2.232	1.69S	2.250	2.236	0.62S	-0.88
31	A	8 2	1670	2.260	2.234	1.18S	2.245	2.238	0.33S	-0.66
47	A	8 2	1775	2.247	2.228	0.87S	2.237	2.231	0.28S	-0.45
63	A	8 2	1787	2.250	2.227	1.02S	2.240	2.230	0.44S	-0.44
88	B	8 2	322	5.130	5.147	0.33F	5.090	5.123	0.65F	-0.78
94	B	8 2	1920	2.250	2.225	1.11S	2.245	2.228	0.76S	-0.22
95	B	8 2	1910	2.260	2.225	1.56S	2.240	2.228	0.54S	-0.88
110	B	8 2	1904	2.250	2.225	1.11S	2.238	2.228	0.45S	-0.52
126	B	7 3	2034	2.267	2.227	1.78S	2.255	2.230	1.10S	-0.53
142	B	7 3	2080	2.222	2.229	0.33F	2.205	2.233	1.24F	-0.77

DEV. AND DIFF. ARE IN PERCENT  
 THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2  
 F=FAST AND S=SLOW

TABLE 3-1

J-26 MISSION 1028 CLOCK/SYSTEM TIME CORRELATION

ORDER FIT 1

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.37240383D 05	0.228031136D 06	0.372403897D 05	-0.0067	9	
0.77053477D 05	0.267844225D 06	0.770534790D 05	-0.0020	16	
0.32594290D 05	0.309785034D 06	0.325942883D 05	0.0017	24	
0.72299778D 05	0.349490531D 06	0.722997856D 05	-0.0076	31	
0.33309788D 05	0.396900538D 06	0.333097930D 05	-0.0050	40	
0.73100383D 05	0.436691121D 06	0.731003763D 05	0.0067	47	
0.34100658D 05	0.484091391D 06	0.341006467D 05	0.0113	56	
0.73702350D 05	0.523693097D 06	0.737023530D 05	-0.0030	63	
0.29340467D 05	0.288602850D 05	0.293404533D 05	0.0137	71	
0.74546183D 05	0.740660170D 05	0.745461857D 05	-0.0027	79	
0.30051578D 05	0.115971406D 06	0.300515750D 05	0.0030	87	
0.69751498D 05	0.155671329D 06	0.697514983D 05	-0.0003	94	
0.30727510D 05	0.203047342D 06	0.307275117D 05	-0.0017	103	
0.70414893D 05	0.242734721D 06	0.704148910D 05	0.0020	110	
0.31398553D 05	0.290118380D 06	0.313985504D 05	0.0026	119	
0.71074008D 05	0.329793839D 06	0.710740097D 05	-0.0017	126	
0.32031826D 05	0.377151663D 06	0.320318340D 05	-0.0080	135	
0.71671088D 05	0.416790919D 06	0.716710903D 05	-0.0023	142	

A0=-0.1907907481D 06 A1= 0.10000000777D 01

SIGMA=0.00565 NO. POINTS= 18

RATIO OF CLOCK TIME TO SYS TIME= 0.99999992226D 00

ORDER FIT 2

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.37240383D 05	0.228031136D 06	0.372403841D 05	-0.0011	9	
0.77053477D 05	0.267844225D 06	0.770534753D 05	0.0017	16	
0.32594290D 05	0.309785034D 06	0.325942863D 05	0.0037	24	
0.72299778D 05	0.349490531D 06	0.722997851D 05	-0.0071	31	
0.33309788D 05	0.396900538D 06	0.333097938D 05	-0.0058	40	
0.73100383D 05	0.436691121D 06	0.731003781D 05	0.0049	47	
0.34100658D 05	0.484091391D 06	0.341006493D 05	0.0087	56	
0.73702350D 05	0.523693097D 06	0.737023561D 05	-0.0061	63	
0.29340467D 05	0.288602850D 05	0.293404567D 05	0.0103	71	
0.74546183D 05	0.740660170D 05	0.745461890D 05	-0.0060	79	
0.30051578D 05	0.115971406D 06	0.300515781D 05	-0.0001	87	
0.69751498D 05	0.155671329D 06	0.697515010D 05	-0.0030	94	
0.30727510D 05	0.203047342D 06	0.307275135D 05	-0.0035	103	
0.70414893D 05	0.242734721D 06	0.704148919D 05	0.0011	110	
0.31398553D 05	0.290118380D 06	0.313985499D 05	0.0031	119	
0.71074008D 05	0.329793839D 06	0.710740078D 05	0.0002	126	
0.32031826D 05	0.377151663D 06	0.320318302D 05	-0.0042	135	
0.71671088D 05	0.416790919D 06	0.716710847D 05	0.0033	142	

A0=-0.1907907686D 06 A1= 0.100000008876D 01

A2=-0.6864429946085D-13

SIGMA=0.00483 NO. POINTS= 18

TABLE 3-2



TABLE 3-3

## J-26 TEMPERATURE SUMMARY

<u>SENSOR</u>	<u>ORBITS ACQUIRED</u>																	
<u>Master Camera</u>	0	9	16	24	31	40	47	56	63	71	79	87	95	103	110	119	126	142
3	64	80	76	81	75	77	76	78	75	77	75	76	70	78	67	70	65	66
4	62	84	81	85	81	82	80	82	79	82	79	79	72	78	71	75	70	68
5	57	84	79	83	79	82	77	81	77	80	77	77	70	74	68	70	66	66
6	62	91	87	91	87	90	86	87	84	86	85	83	77	69	75	76	73	72
7	62	88	86	89	85	88	84	86	83	85	84	82	77	80	73	75	71	71
8	68	92	88	92	87	91	85	90	85	90	85	86	79	83	76	81	75	74
9	62	92	86	92	85	89	84	89	83	88	83	84	77	81	75	78	73	72
10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	65	90	85	90	77	86	81	85	80	78	80	80	71	75	68	72	66	64
12	69	86	81	88	80	84	80	85	80	85	81	82	66	80	73	78	71	71
13	59	87	85	88	81	83	82	82	81	81	81	78	72	74	70	70	67	67
AVG	63	87	83	88	82	85	81	84	81	83	81	81	73	78	72	75	70	69
<u>Slave Camera</u>																		
3	59	86	81	87	80	82	80	82	79	80	78	77	69	73	64	67	62	62
4	65	89	84	89	84	87	83	86	82	86	82	81	75	80	72	75	71	68
5	64	86	87	86	82	86	80	84	81	83	82	81	77	79	72	74	71	70
6	58	81	79	82	79	81	78	79	78	79	79	78	74	78	68	70	66	66
7	61	88	84	88	84	87	82	86	82	85	83	82	78	80	71	73	69	69
8	62	86	83	87	83	85	82	85	82	85	83	82	77	81	74	76	71	70
9	65	88	84	89	83	85	83	87	83	87	85	85	80	84	77	80	75	74
10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	67	79	76	80	78	78	76	79	76	81	78	76	70	74	67	69	66	67
12	59	85	78	85	78	81	77	82	76	81	77	78	70	75	67	71	64	63
13	55	77	75	78	75	74	74	74	73	75	76	71	68	69	64	64	61	60
AVG	62	85	81	85	81	83	80	82	79	82	80	79	74	77	70	72	68	67
<u>Supply Spool</u>																		
1	65	72	72	75	74	74	74	76	74	76	76	74	70	72	67	67	65	65
2	66	79	76	80	77	80	76	80	76	79	77	76	71	74	67	69	65	64

**NOTE:** All data corrected for self-heating, except injection.

TABLE 3-3

## J-26 TEMPERATURE SUMMARY

SENSOR		ORBITS ACQUIRED														
Fair ("A")	Barrel #1 ("B")	0	9	16	24	31	40	47	56	63	71	79	87	95	103	110
	1	*OBH	51	29	51	29	35	25	51	25	48	25	34	78	38	25
	2	OBH	17	0	17	0	7	0	20	0	20	0	79	53	76	51
	3	OBH	-4	-8	0	-8	-8	-8	-4	-4	0	-4	91	85	88	76
	4		217	54	41	54	44	47	41	54	41	51	38	45	42	35
	5	OBH	75	55	72	52	62	48	68	48	65	45	41	31	34	24
	6	231+	76	57	70	50	57	44	67	40	63	40	--	--	--	--
<u>Barrel #2</u>																
	1	-131	55	58	52	52	39	48	48	48	45	42	35	29	32	22
	2	125	57	67	54	67	41	57	48	57	44	51	44	38	38	31
	3	190	83	80	83	83	77	80	83	83	83	83	85	80	83	70
	4	212	75	55	71	58	71	58	78	62	78	65	81	58	81	55
	5	201	63	60	66	60	60	60	66	66	82	73	66	60	76	43
<u>Conic Adapter</u>																
	1	145	58	48	55	45	38	38	51	42	48	38	35	18	32	32
<u>Clock</u>																
	1	90	74	70	74	70	67	70	74	70	72	72	65	55	63	70
	2	92	74	67	72	70	67	65	72	65	72	67	65	52	61	50
<u>Thrust Cone "A" to "B" SRV</u>																
	1	110	46	39	45	38	40	37	42	37	42	37	67	61	64	61
	2	72	63	56	59	54	55	52	55	52	55	50	74	67	69	67
<u>Stellar/Index "A" to "B"</u>																
	1	74	60	54	60	54	51	51	57	54	57	51	64	51	61	51
	2	65	62	59	62	56	56	53	59	53	56	53	64	52	58	52
<u>Recovery Battery "B" SRV</u>																
	1	72	75	75	75	76	70	74	74	74	73	74	81	84	86	84
<u>Master Cassette "A" SRV</u>																
	2	93	74	70	72	70	64	63	64	63	63	63	--	--	--	--

\*Out of Bounds High (OBH)

NOTE: Only Thrust Cone Data corrected for Self-heating.

TOP SECRET

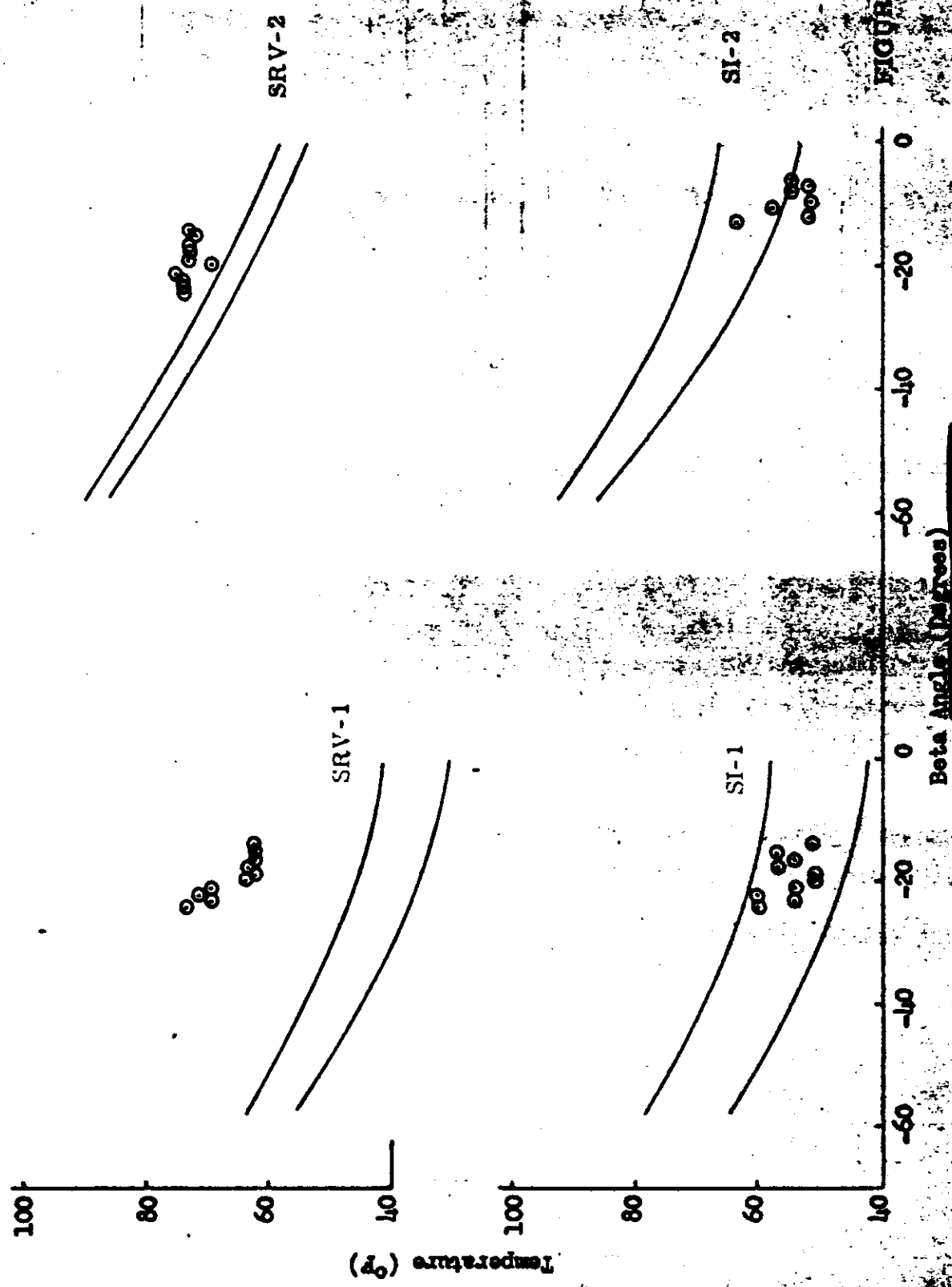


FIGURE 3

TOP SECRET

TOP SECRET

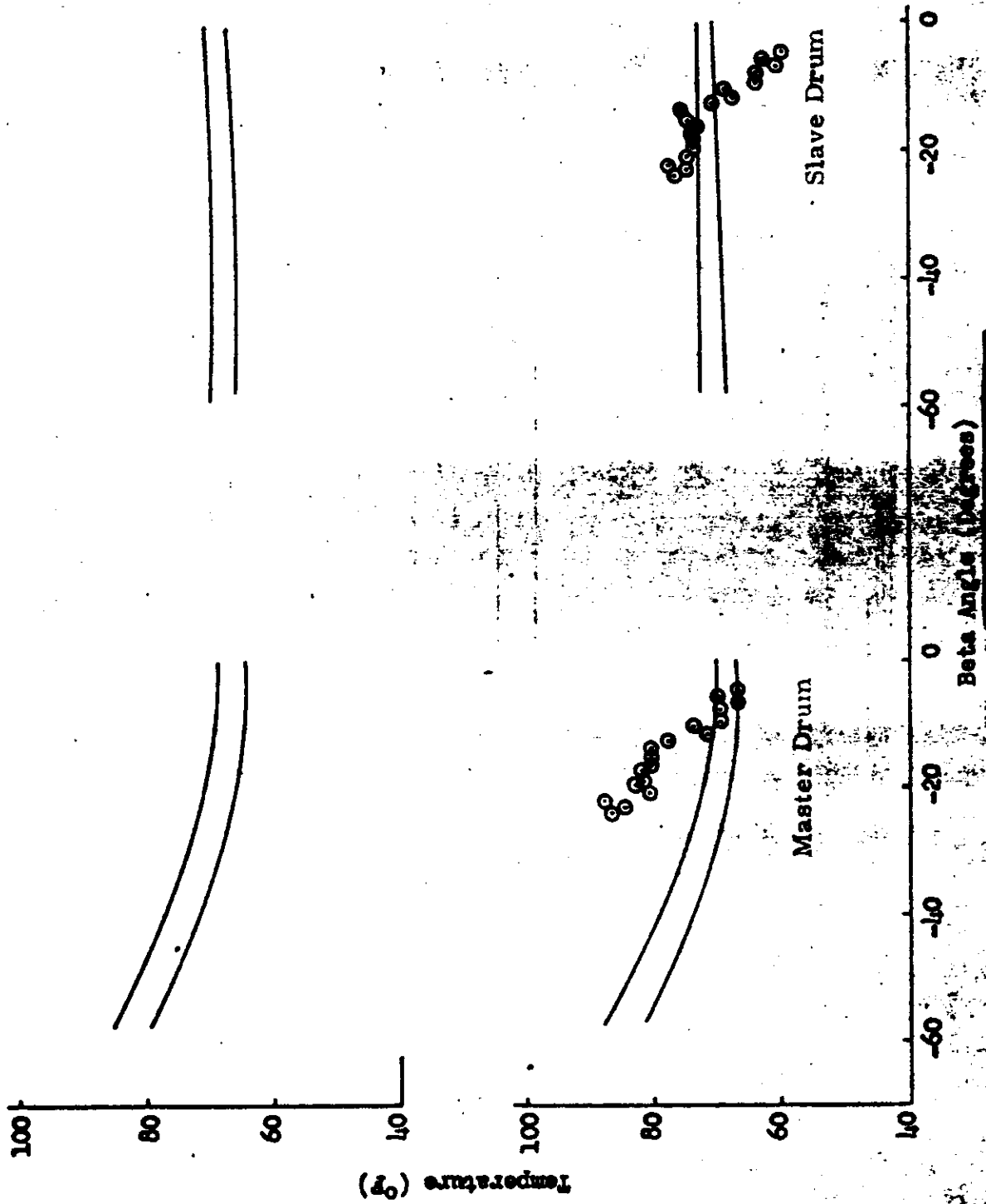
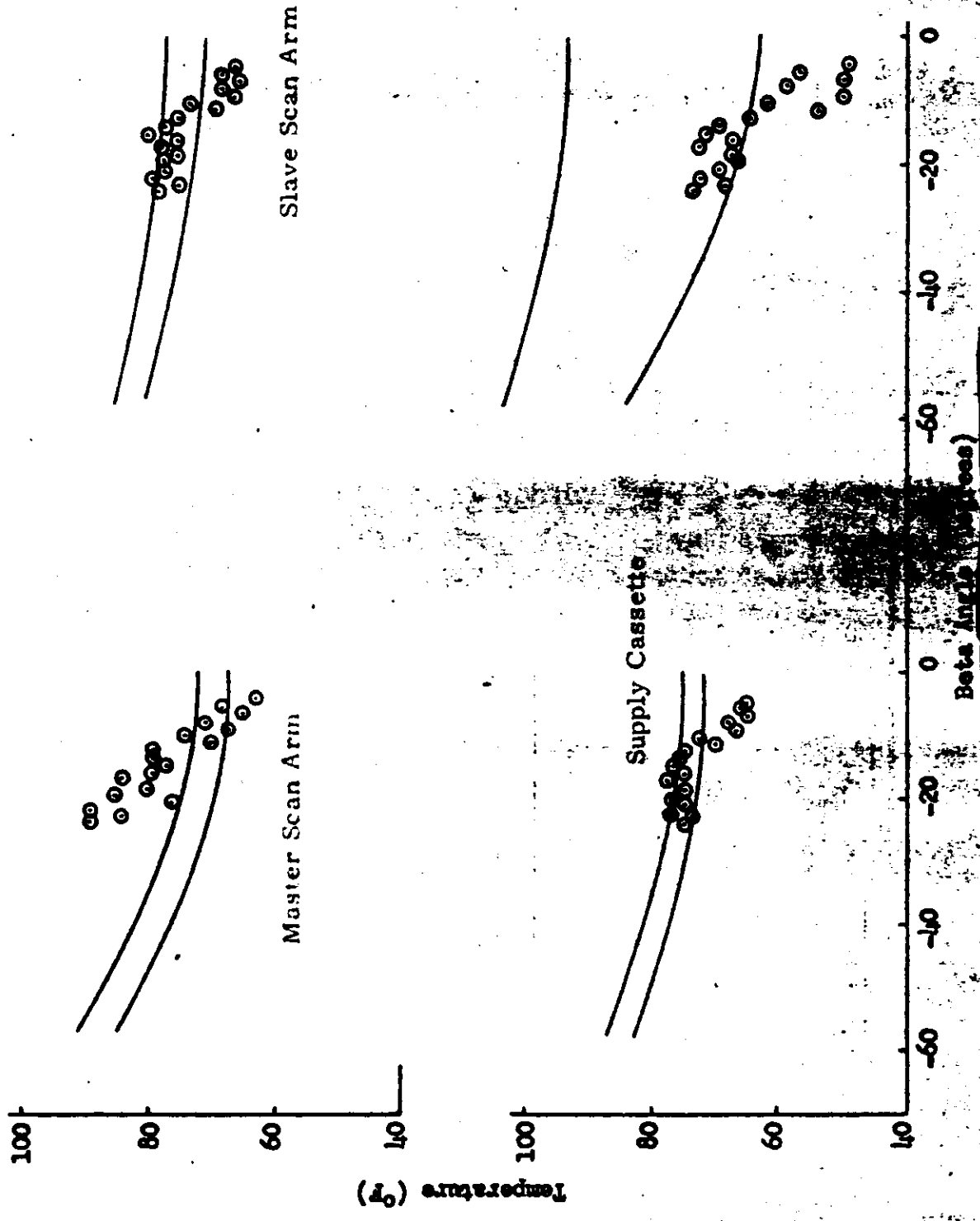


FIGURE 3

TOP SECRET

TOP SECRET



FIGURE

Beta Angle (Degrees)

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SECTION 4

MISSION 1028-1 RECOVERY SYSTEM

SRV #703 was received at A/P on 24 May 1965. The receiving inspection weight was 146.6 pounds. After modifications and incorporation of outstanding Engineering Orders, the unit was delivered to Systems Test for installation into the J-26 system.

The Recovery System was shipped to VAFB on 2 December 1965.

A successful air catch was made during Orbit 81 on 29 December 1965 at 1615 PST. The impact point was within predicted tolerances.

Predicted Impact  $23^{\circ} - 59.6' N$   $169^{\circ} - 34.6' W$

Actual Impact  $23^{\circ} - 58' N$   $169^{\circ} - 42' W$

All recovery event times were within the required tolerances. Table 4-1 shows the time sequence of recovery events.

The condition of the recovered capsule was normal.

~~TOP SECRET~~

MISSION 1028-1

RE-ENTRY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>
* Arm	N/A	77.0 <u>±</u> 1.0
** Transfer	N/A	2.0 <u>±</u> 0.25
Electrical Disconnect	N/A	0.90 <u>±</u> 0.43 - 0.40
Separation	--	--
** Spin	N/A	3.40 <u>±</u> 0.30
Retro	N/A	7.55 <u>±</u> 0.45
Despin	10.62	10.75 <u>±</u> 0.59
T/C Separation	1.51	1.5 <u>±</u> 0.15
*** "G" Switch Open	478.4	490.2 - 512.4
Parachute Cover Off	33.94	34.0 <u>±</u> 1.5
Drogue Chute Deployed	0.63	0.63 <u>±</u> 0.08
Main Chute Bag Separate	9.79	10.25 <u>±</u> 1.5
Main Chute Deployed	0.55	0.52 <u>±</u> 0.13
Main Chute Disreef	4.68	4.5 <u>±</u> 0.8
* From Separation		
** From Electrical Disconnect		
*** From Retro		
Spin Rates (RPM)	N/A	
Despin Rates (RPM)	N/A	
Retro Velocity (Ft./Sec.)	968	

TABLE 4-1

SECTION 5

MISSION 1028-2 RECOVERY SYSTEM

SRV #704 was received at A/P on 24 May 1965. The receiving inspection weight was 150.8 pounds. After modifications and incorporation of outstanding Engineering Orders, the unit was delivered to Systems Test for installation into the J-26 System.

The Recovery System was shipped to VAFB on 2 December 1965.

A successful air catch was made during Orbit 144 on 2 January 1966 at 1552 PST. The impact point was within predicted tolerances.

Predicted Impact	22° - 52' N	167° - 18.4' W
Actual Impact	22° - 54' N	167° - 25' W

All recovery event times were within the required tolerances. Table 5-1 shows the time sequence of recovery events.

The condition of the recovered capsule was normal.



MISSION 1028-2

RE-ENTRY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>
*Arm	76.77	77.0 <u>+ 1.0</u>
*Transfer	2.04	2.0 <u>+ 0.25</u>
Electrical Disconnect	0.84	0.90 <u>+ 0.43</u> - 0.40
Separation	--	--
**Spin	3.45	3.4 <u>+ 0.30</u>
Retro	7.60	7.55 <u>+ 0.45</u>
Despin	10.68	10.75 <u>+ 0.59</u>
T/C Separation	1.52	1.5 <u>+ 0.15</u>
***"G" Switch Open	511.0	490.2 - 512.4
Parachute Cover Off	33.80	34.0 <u>+ 1.5</u>
Drogue Chute Deployed	0.60	0.63 <u>+ 0.08</u>
Main Chute Bag Separate	9.71	10.25 <u>+ 1.5</u>
Main Chute Deployed	0.55	0.52 <u>+ 0.13</u>
Main Chute Disreef	4.10	4.50 <u>+ 0.80</u>
* From Separation		
** From Electrical Disconnect		
*** From Retro		
Spin Rates (RPM)	6.40	
Despin Rates (RPM)	12.75	
Retro Velocity (Ft. /Sec.)	944	

TABLE 5-1

SECTION 6

MASTER PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	176
Main Camera Lens	1772435
Supply Horizon Camera	278-G4
Supply Horizon Camera Lens	E12830
Take-up Horizon Camera	274-G1
Take-up Horizon Camera Lens	816635
Supply Cassette	SC-5

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.250"
Filter Type	Wratten 25
Film Type	Eastman Type 3404

Supply (Port) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/6.3
Exposure Time	1/100 second
Filter Type	Wratten 25

**Take-up (Starboard) Horizon Camera:**

Lens	55 mm f/6.8
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

**C. POST FLIGHT PERFORMANCE EVALUATION**

The image quality produced on this mission was considered by both the PEIR team and PI groups to be the best obtained in recent months. The PI group described the coverage as having a crispness not obtained since last winter. A high contrast resolution target displayed a ground resolution of 7.5 feet along track and 11.5 feet cross track. As has been noted on most missions the Aft camera imagery is slightly better than the Forward looking camera. The MIP rating for the -1 and -2 mission was 85 and the selected frames were from the Aft camera.

The 200 cycle timing light operated intermittently and the smear pulse varied in length. The probable cause was a marginal neon bulb.

Minor light leaks were traced to the felt seals and the laminated strips on the instrument drum.

An out of focus condition occurred during passes D130 and D131. A manufacturing splice was located in this area and probably caused abnormal film tension.

SECTION 7

SLAVE PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	177
Main Camera Lens	1752435
Supply Horizon Camera	279-G4
Supply Horizon Camera Lens	E12865
Take-up Horizon Camera	275-G1
Take-up Horizon Camera Lens	816637
Supply Cassette	SC-8

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.175"
Filter Type	Wratten 21
Film Type	Eastman Type 3404

Supply (Starboard) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

**Take-up (Port) Horizon Camera:**

Lens	55 mm f/6.8
Aperture Setting	f/6.8
Exposure Time	1/100 second
Filter Type	Wratten 25

**C. POST FLIGHT PERFORMANCE EVALUATION**

The photographic quality and information content of the imagery produced by the Slave camera was excellent. The photography was degraded by the minor effects of the usual light leaks and the following anomalies.

The horizon imagery on the starboard side (supply) was veiled from the start of the mission through pass D68. This veiling did not interfere with the data reduction.

A region of soft imagery was present throughout the mission. It was located along the time track edge of the format and up to one-half inch wide. This condition is possibly due to irregularity in tracking tension.

SECTION 8

PANORAMIC CAMERA EXPOSURE

The Master camera used a 0.250 inch slit and a Wratten 25 filter while the Slave instrument was fitted with a 0.175 inch slit and a Wratten 21 filter. The resulting nominal exposure calls for processing between intermediate and full development of EK type 3404 film.

The frequency distribution of the solar elevations and solar azimuths encountered during the photographic operations are shown in Figures 8-1 to 8-4.

The nominal exposure times are shown as a function of latitude for passes D-8, D-72, and D-136 in Figure 8-5 to 8-10. The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by

[REDACTED]

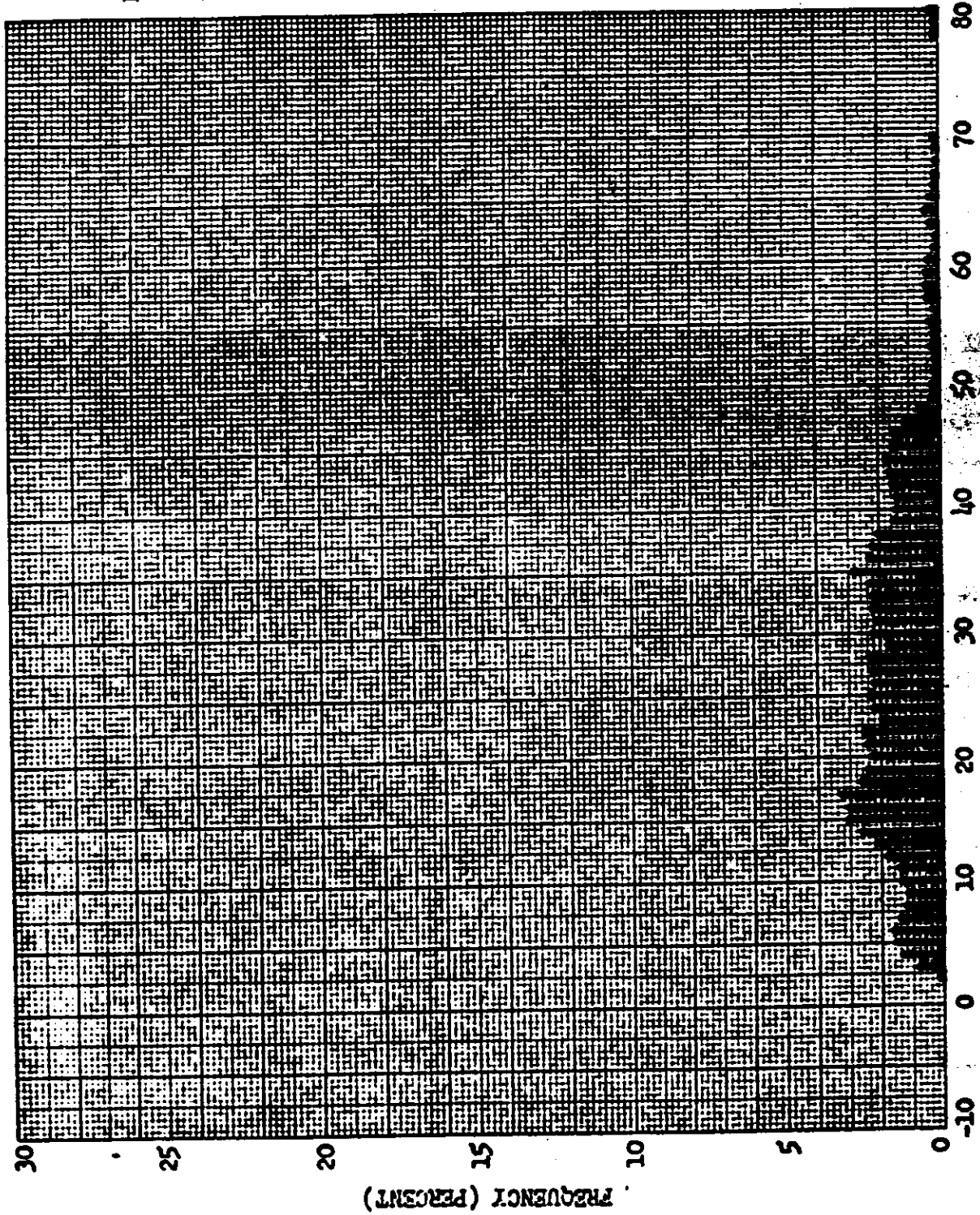
<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1028-1	FWD	Predicted	0	4	96
		Reported	0	4	96
1028-1	AFT	Predicted	0	5	95
		Reported	0	16	84
1028-2	FWD	Predicted	0	3	97
		Reported	1	9	90
1028-2	AFT	Predicted	0	10	90
		Reported	0	6	94

The measured density values (D-Min., D-Max.) were lower than the average values for past missions. The camera exposure settings are selected by weighing the predicted density versus image degradations resulting from image motion. The mission used exposure times, which in combination with solar altitudes produces low density values even with full processing development. It would be an aid in selecting exposure settings to have data describing the mission's operational target brightnesses.

[REDACTED]

~~TOP SECRET~~

SOLAR ELEVATION FREQUENCY DISTRIBUTION



Mission No: 1022-2

Payload No: J-26

Camera No: 176

Launch Date: 12/21/62

Launch Time: 2106 J

Inclination: 60°

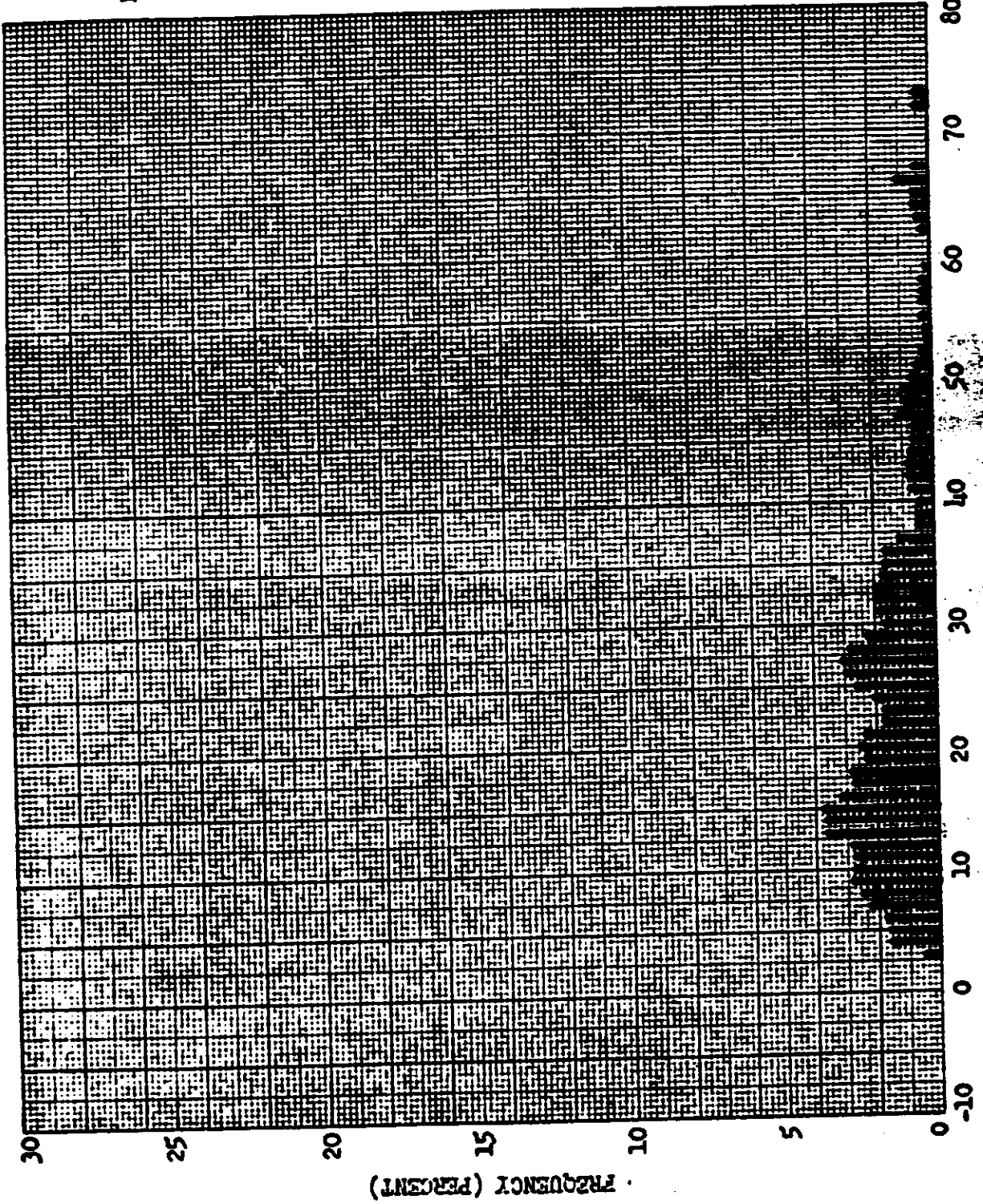
FIGURE 8-1

~~TOP SECRET~~

~~TOP SECRET~~

~~TOP SECRET~~

SOLAR ELEVATION FREQUENCY DISTRIBUTION



Mission No: 1028-1

Payload No: J-26

Camera No: 176

Launch Date: 12/24/65

Launch Time: 2106 Z

Inclination: 80°

FIGURE 8-2

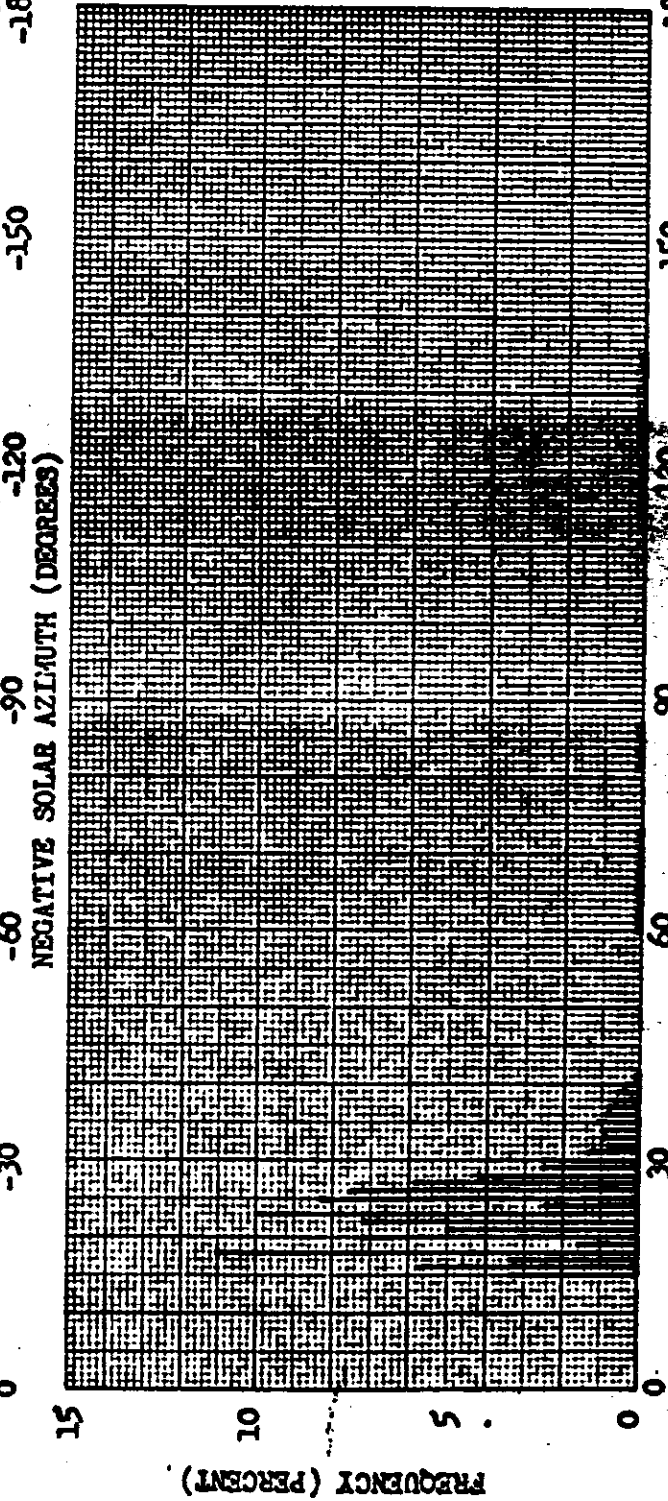
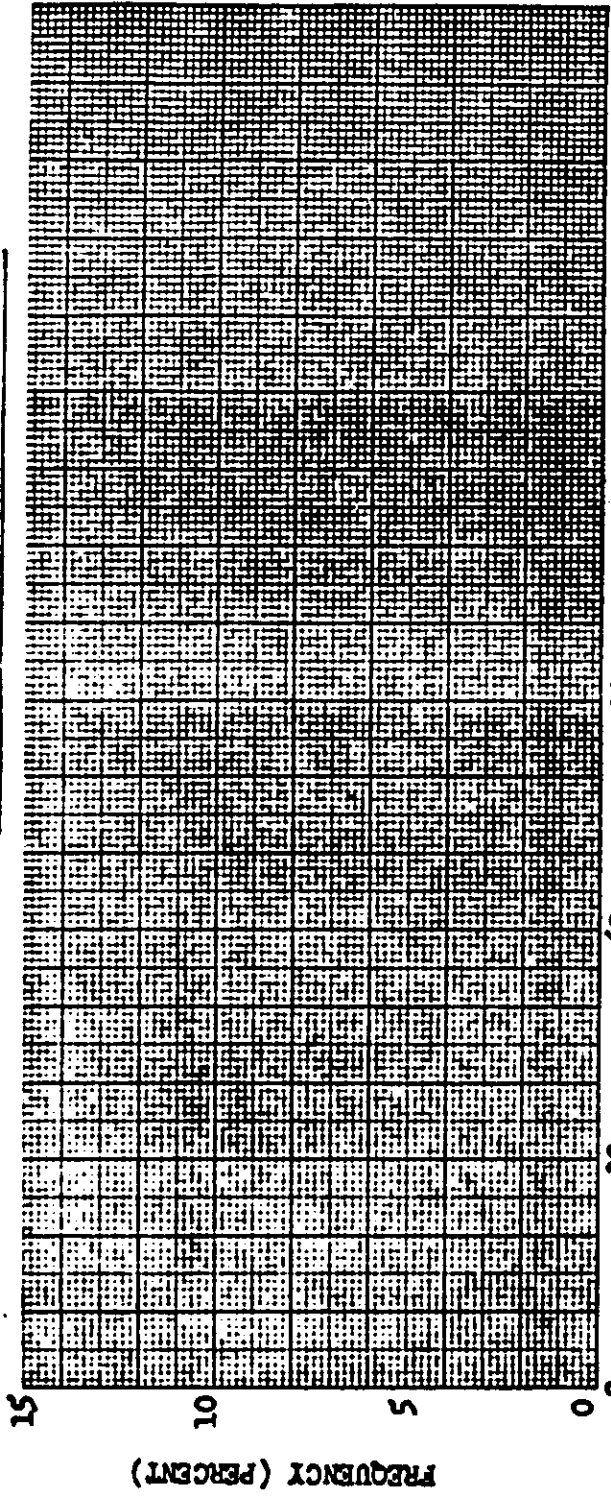
SOLAR ELEVATION (DEGREES)

~~TOP SECRET~~



TOP SECRET

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1028-1

Payload No: J-26

Camera No: 176

Launch Date: 12/24/65

Launch Time: 2106 Z

Inclination: 80°

SIGN NOTATION

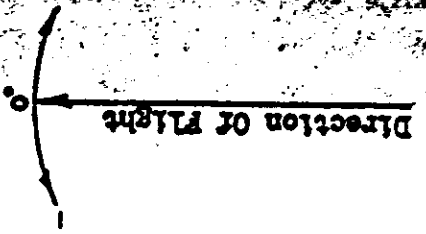
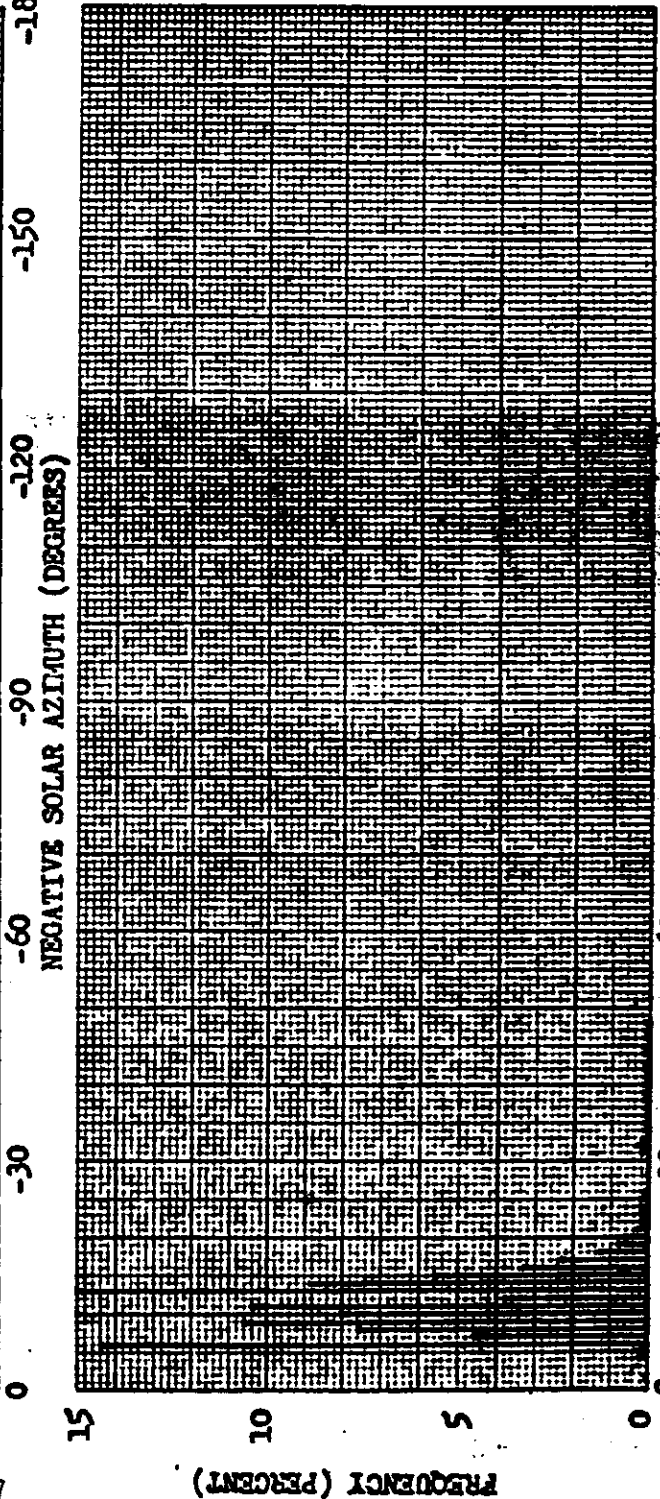
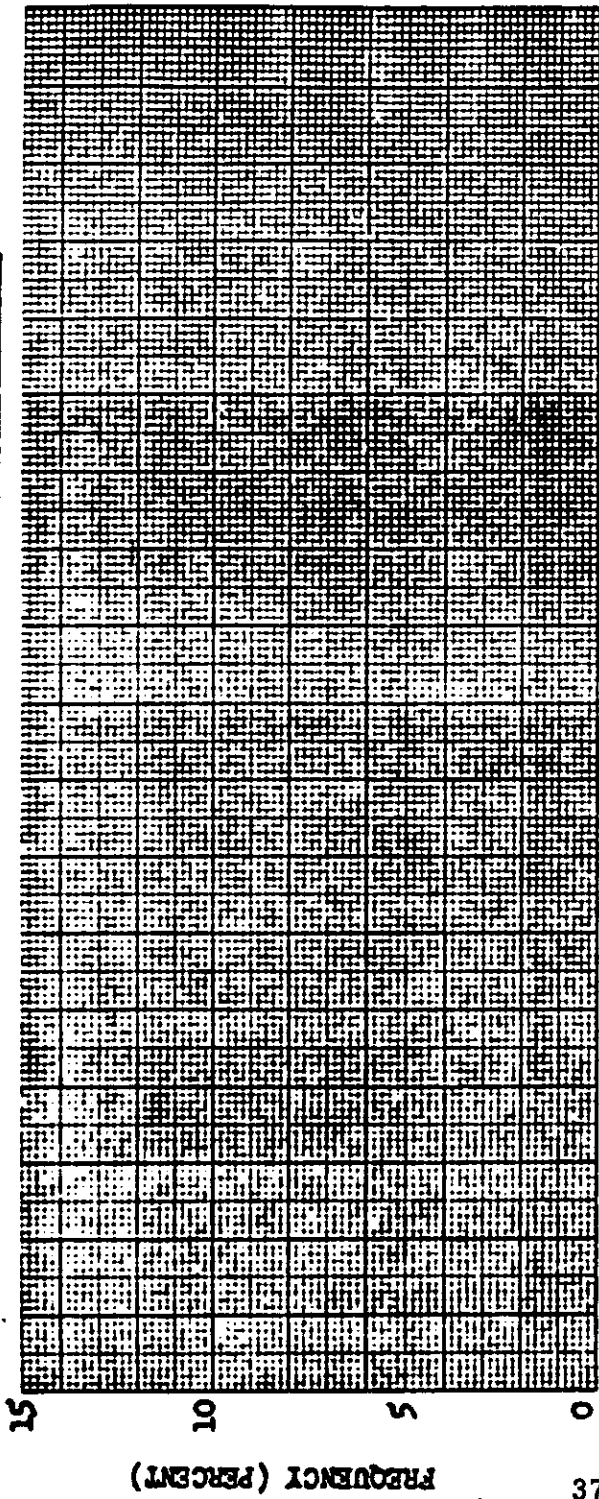


FIGURE 8-3

TOP SECRET

~~TOP SECRET~~

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1080-2

Payload No: J-26

Camera No: 176

Launch Date: 12/24/65

Launch Time: 2106 Z

Inclination: 60°

SIGN NOTATION

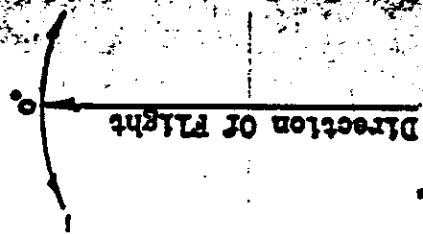
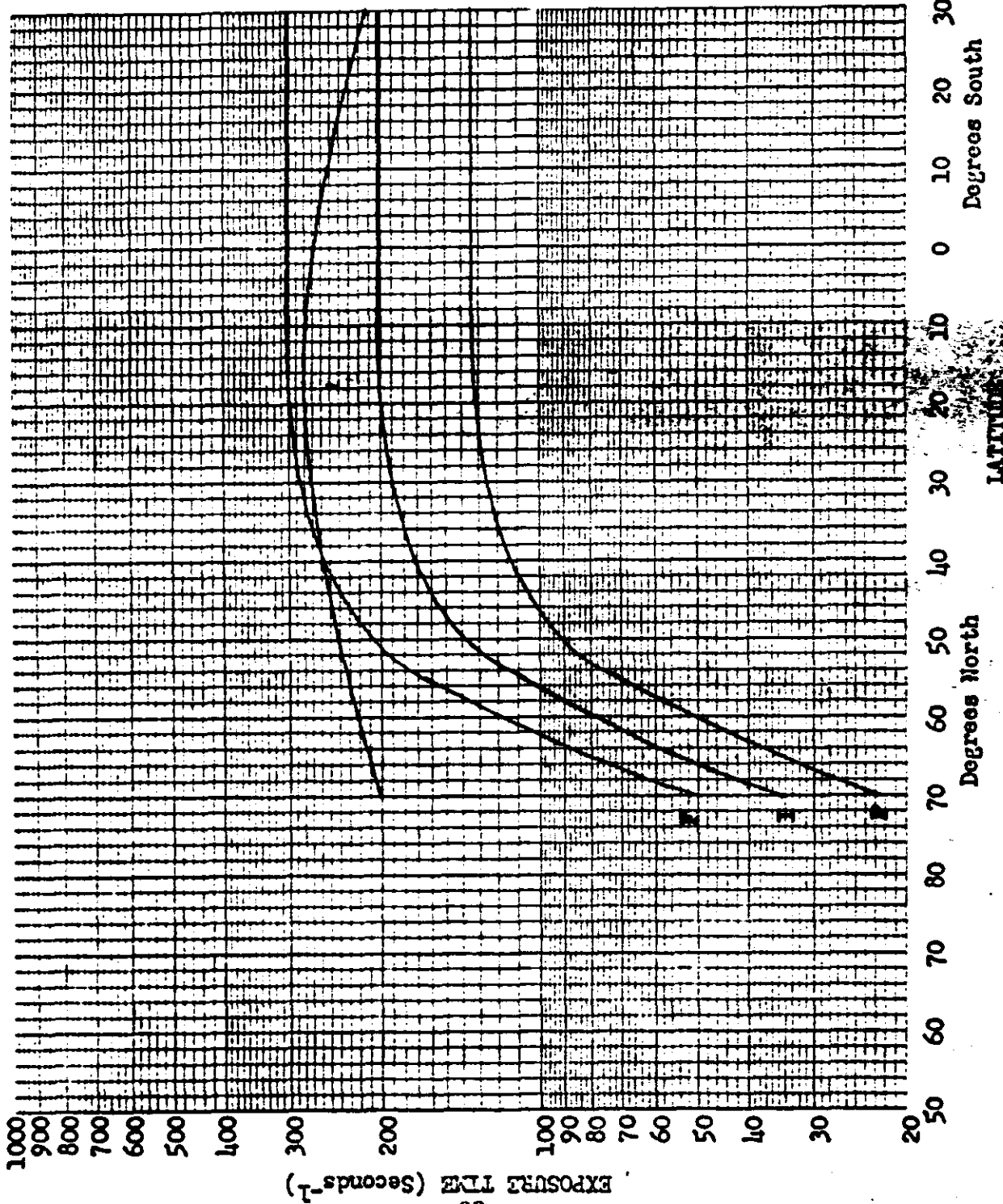


FIGURE 8-4

EXPOSURE POINTS



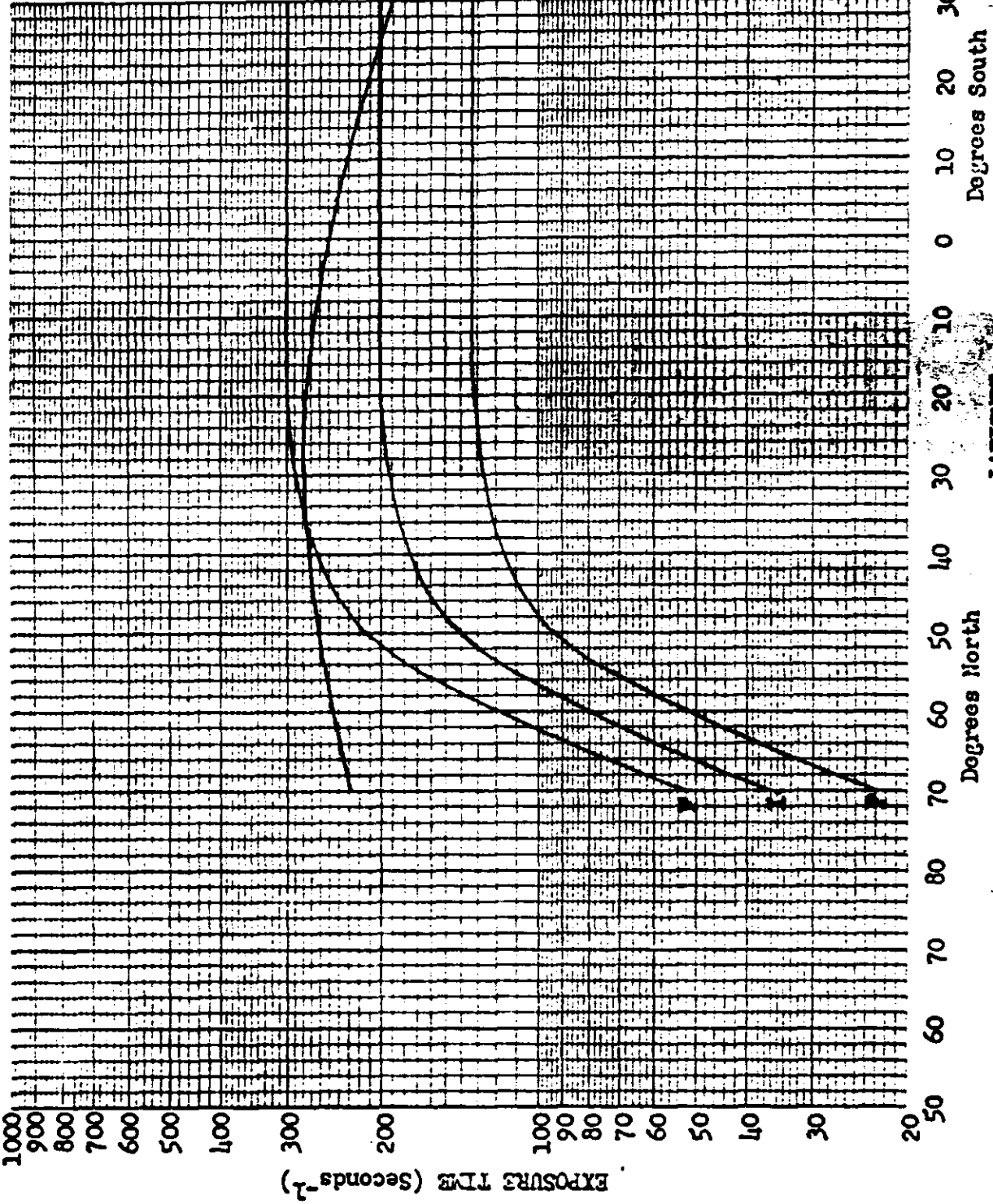
Mission No: 1028  
Payload No: J-26  
Camera No: 176  
Pass No: 6  
Launch Date: 12/21/65  
Launch Time: 2106 L  
Slit Width: .250  
Filter Type: Wavelength 25  
Film Type: 3404

FIGURE 8-5

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EXPOSURE POINTS



Mission No: 1028  
 Payload No: J-26  
 Camera No: 176  
 Pass No: 72  
 Launch Date: 12/21/65  
 Launch Time: 2106 Z  
 Slit Width: .250  
 Filter Type: Wattson 5  
 Film Type: 3104

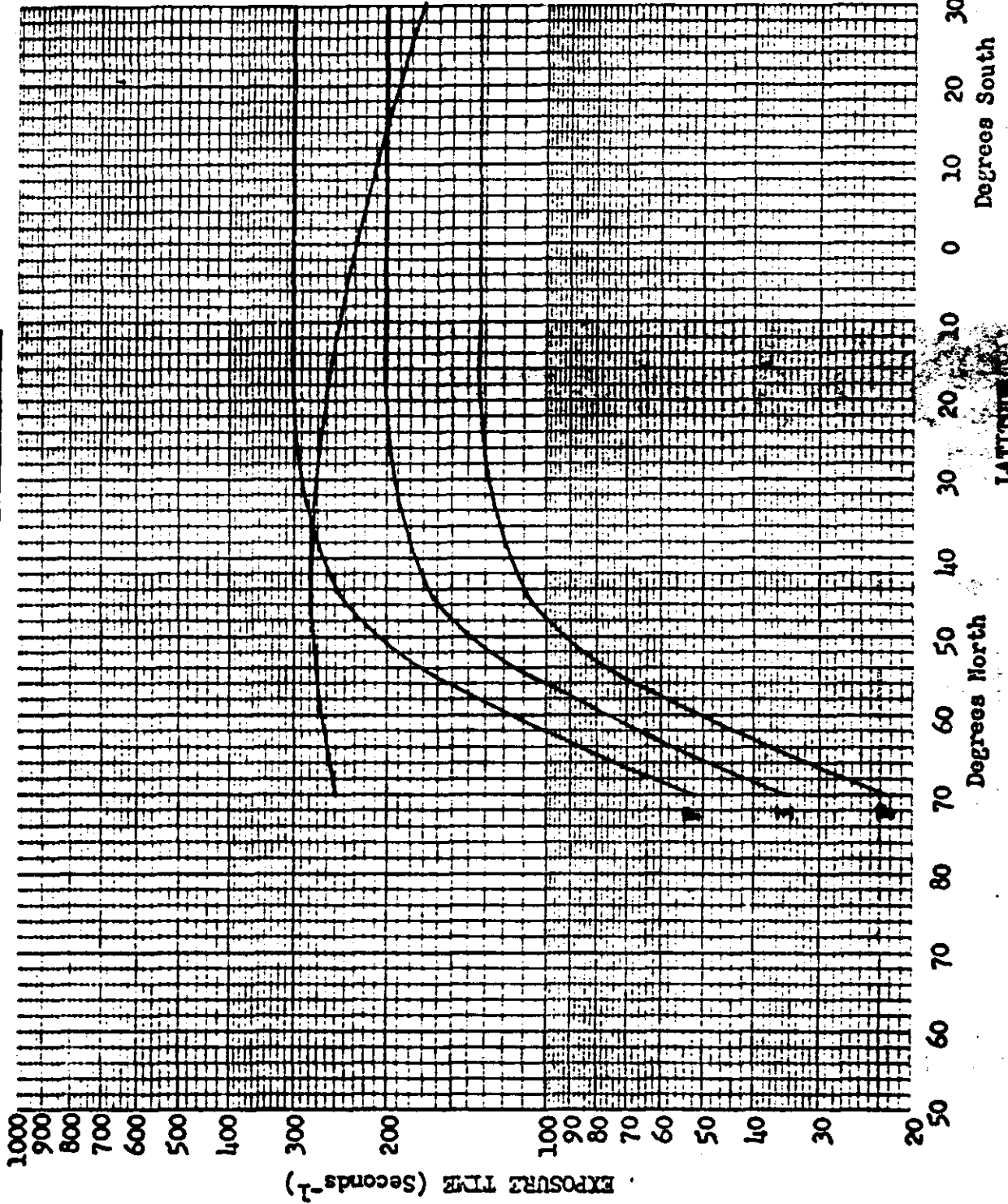
FIGURE 8-6

LATITUDE  
Degrees North  
Degrees South

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EXPOSURE POINTS



Mission No: 1028

Payload No: J-26

Camera No: 176

Pass No: 136

Launch Date: 12/24/65

Launch Time: 2106 Z

Slit Width: .250

Filter Type: Wratten 25

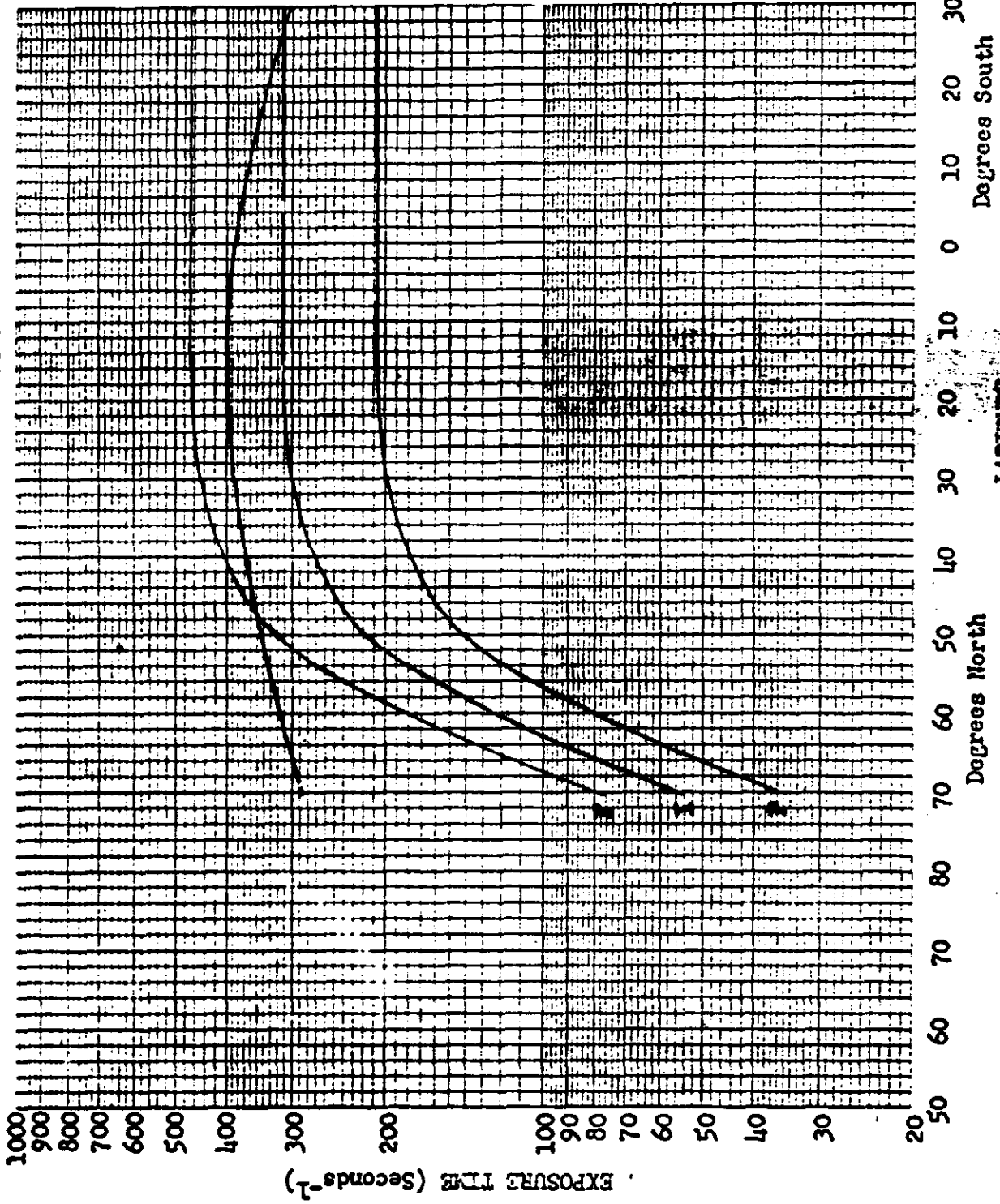
Film Type: 3104

FIGURE 8-7

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EXPOSURE POINTS

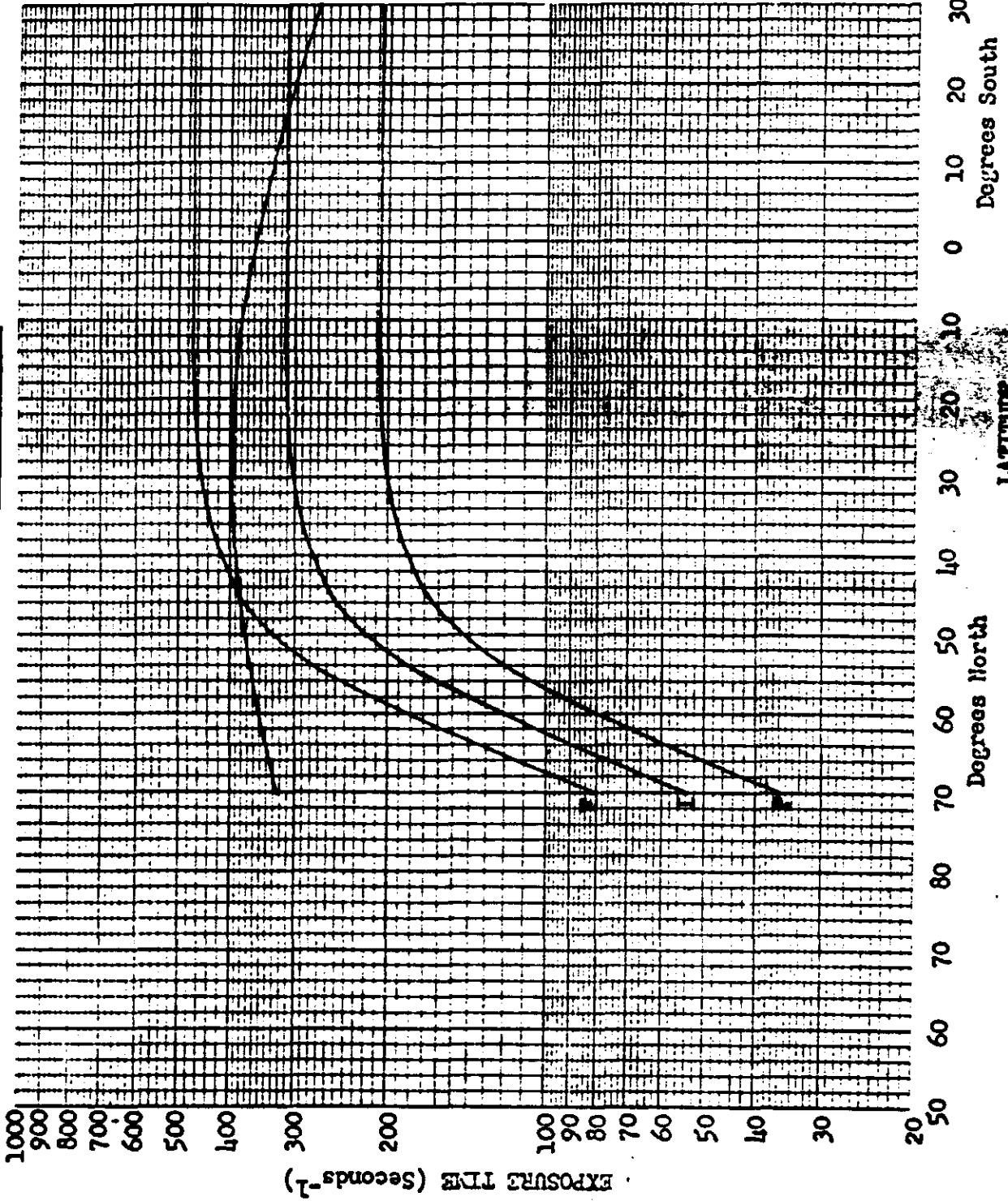


Mission No: 1028  
 Payload No: J-26  
 Camera No: 177  
 Pass No: 8  
 Launch Date: 12/24/65  
 Launch Time: 2106 Z  
 Slit Width: .175  
 Filter Type: Wratten 21  
 Film Type: 3104

FIGURE 8-8

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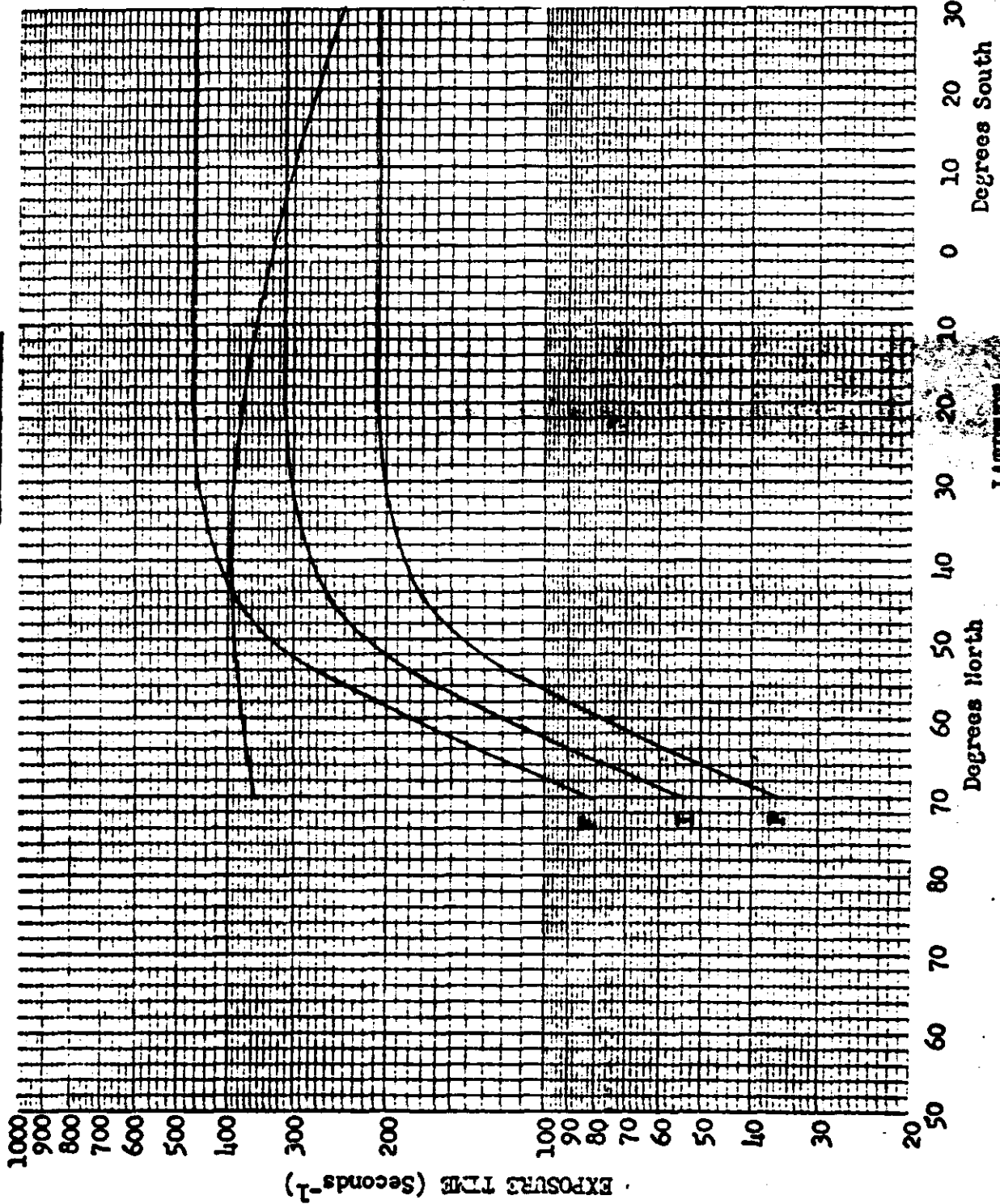
EXPOSURE POINTS



Mission No: 1028  
Payload No: J-26  
Camera No: 177  
Pass No: 72  
Launch Date: 12/24/65  
Launch Time: 2106 Z  
Slit Width: .175  
Filter Type: Wratten 21  
Film Type: 304

FIGURE 8-9

EXPOSURE POINTS



Mission No: 1028

Payload No: J-26

Camera No: 177

Pass No: 136

Launch Date: 12/21/65

Launch Time: 2106 Z

Slit Width: .275

Filter Type: Wratten 21

Film Type: 2404

FIGURE 8-10

LATITUDE

Degrees North

Degrees South



SECTION 9

DIFFUSE DENSITY MEASUREMENTS

The diffuse density measurements made by AFSPPF were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base plus fog density values where measurements up to 0.09 density are considered as having received Primary processing, 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1028-1	FWD	Predicted	0	4	96
		Reported	0	4	96
		Computed	0	11	89
1028-1	AFT	Predicted	0	5	95
		Reported	0	16	84
		Computed	0	11	89
1028-2	FWD	Predicted	0	3	97
		Reported	1	9	90
		Computed	0	15	85
1028-2	AFT	Predicted	0	10	90
		Reported	0	6	94
		Computed	0	6	94

The tabulations of density frequency distributions for Missions 1028-1 and 1028-2 are included in Appendix A, Table A-1 through A-4. The graphical presentation of the density distribution are computer plotted in Appendix A, Figure A-1 through A-37.

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A summary of the processing and exposure analysis is shown in Table 9-1. The terrain D-Min. criteria (range) for proper exposure and processing is 0.40 to 0.90 density units.

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MISSION 1028-1 INSTR - FRWD 2-11-66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDEK EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	C	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	29	0 PC	55 PC	38 PC	7 PC	0 PC
FULL	224	73 PC	0 PC	27 PC	0 PC	0 PC
ALL LEVELS	258	65 PC	6 PC	28 PC	1 PC	0 PC

MISSION 1028-1 INSTR - AFT 2-11-66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDEK EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	30	3 PC	43 PC	53 PC	0 PC	0 PC
FULL	237	63 PC	0 PC	35 PC	2 PC	0 PC
ALL LEVELS	267	56 PC	5 PC	37 PC	1 PC	0 PC

MISSION 1028-2 INSTR - FRWD 2-11-66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDEK EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	36	0 PC	19 PC	81 PC	0 PC	0 PC
FULL	206	69 PC	0 PC	30 PC	1 PC	0 PC
ALL LEVELS	242	59 PC	3 PC	37 PC	1 PC	0 PC

MISSION 1028-2 INSTR - AFT 2-11-66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDEK EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	15	0 PC	13 PC	40 PC	33 PC	13 PC
FULL	234	50 PC	0 PC	44 PC	6 PC	0 PC
ALL LEVELS	249	47 PC	1 PC	44 PC	7 PC	1 PC

MISSION 1028-2 INSTR - AFT 2-11-66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	BASE + FOG	UNDEK EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-C.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP
INTERMEDIATE	0.10-C.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

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TABLE 8

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SECTION 10

PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1028-1 and 1028-2 received a MIP rating of 85. A summary is tabulated below of the MTF/AIM resolution values measured by AFSPPF and [REDACTED]. The microdensimeter slit used by AFSPPF and [REDACTED] was one micron by 80 microns.

<u>Mission</u>	<u>Camera</u>	<u>AFSPPF</u>	[REDACTED]
1028-1	FWD	81	89
1028-1	AFT	92	93
1028-2	FWD	88	87
1028-2	AFT	77	84

The details of the measurement and computing techniques, targets measured and target locations are fully reported in the evaluation report published by AFSPPF and are not normally included in this report.

SECTION 11

OBSERVED DATA

Mission 1028 panoramic camera system produced some of the best photography seen to date on the Corona Program. This conclusion was reached without the aid of CORN Resolution Targets by using other objects of known dimensions. The mobile target at Jefferson City Airport, Missouri was degraded by haze to the extent that approximately 16 feet was the limit of ground resolution. The fixed targets at Edwards AFB, California, were not activated for this mission and were probably reduced in contrast due to dust and sand. No other CORN Targets were photographed.

The MIP frame for mission segment 1028-2 is from the aft camera on pass 126D. In the center of the format is the San Fernando Valley of California. 1 1/2 inches apart are the Lockheed Air Terminal at Burbank and Van Nuys Airport. The standard threshold markers on the Lockheed All-weather Runway are oriented in the photo suitable for along-track resolution evaluation. The same type markings on the Van Nuys Runway are approximately 90° to the other and thus suitable for cross-track evaluation. These markers consist of 2 sets of 4 parallel stripes 12 feet wide, 50 feet long and a space of 3 feet between stripes, using 40x magnification these 3 foot spaces were resolved their entire length by both fore and aft cameras in the along-track direction and by the aft in the cross-track direction. Results were not quite as good for the forward camera cross-track. This suggests a ground resolution capability of approximately 6 feet or 115 L/mm. This corresponds very closely with the results of pre-flight lo-contrast resolution test results.

By comparing other objects in this MIP frame with similar objects in the MIP frame for missions segment 1028-1 and its associated stereo frame, as well as other frames where clear air prevailed, nearly uniform performance was found throughout the mission.

SECTION 12

MISSION 1028-1 STELLAR-INDEX CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-77
Index Reseau	91
Stellar Reseau	97

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

C. POST FLIGHT EVALUATION

Stellar Camera

The camera was operational throughout the mission and provided acceptable imagery for attitude determinations. There were at least 20 images per frame, however they were double imaged. The first 152 frames had images of foreign particles, which are assumed to be jettisoned fuel particles.

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### Index Camera

The camera was operational throughout the mission and provided good terrain photography.

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SECTION 13

MISSION 1028-2 STELLAR-INDEX CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-74
Index Reseau	76
Stellar Reseau	95

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

C. POST FLIGHT EVALUATION

Stellar Camera

The camera was operational throughout the mission. The film was partially fogged from head to tail due to the Index camera shutter malfunction. The fog was degrading for 3 frames at each camera off period. Most images were double and/or smeared, but adequate for attitude determination.



**Index Camera**

The shutter remained open throughout the mission and all terrain imagery was lost.

SECTION 14

VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1028-1 and 1028-2 were derived from the reduction of the stellar camera photography. This attitude data is supplied to A/P by NPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 14-1 through 14-6 show these distributions for Mission 1028-1 and Figures 14-7 through 14-10 for Mission 1028-2.

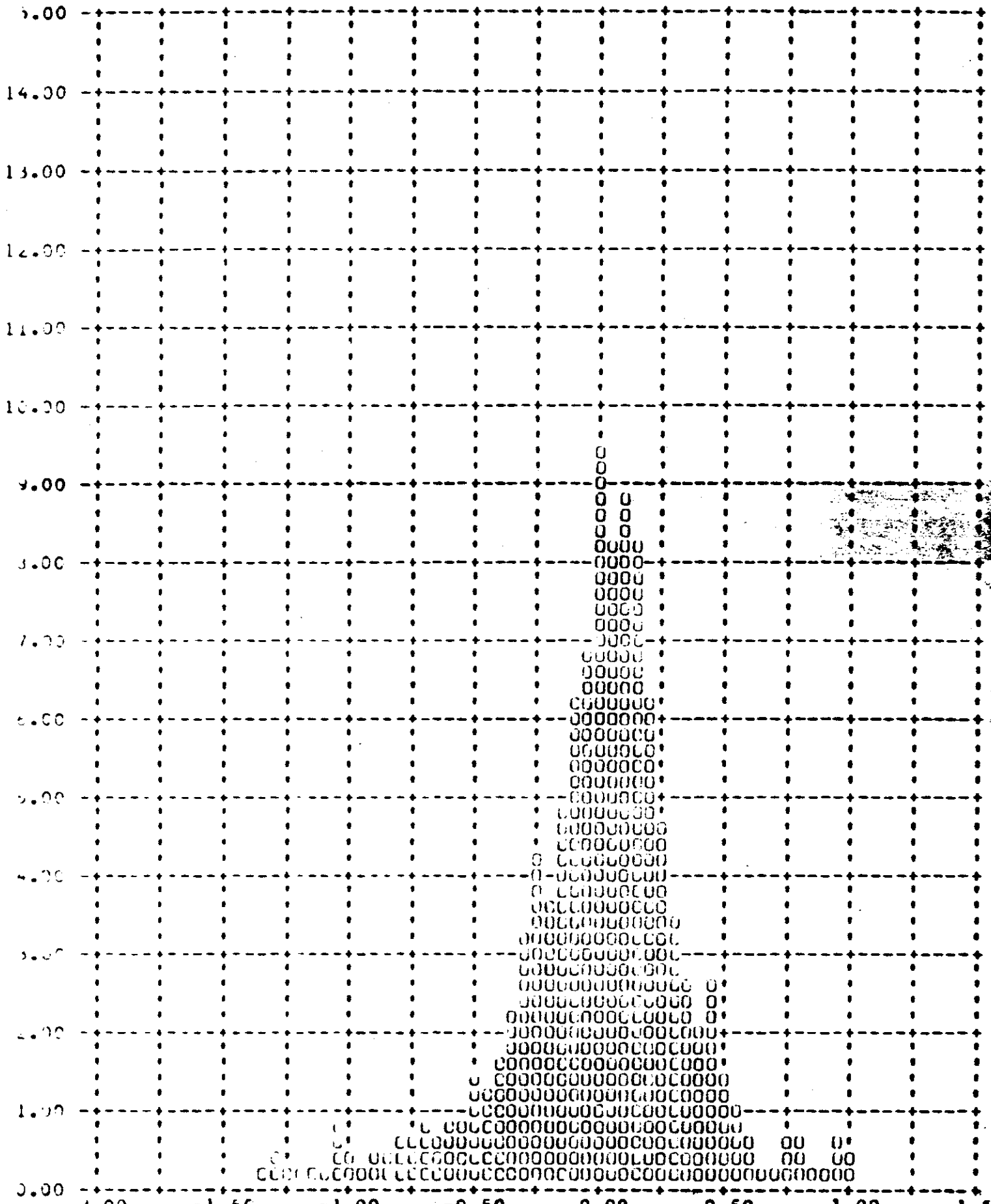
The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the Fwd photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

<u>Value</u>	<u>Mission 1028-1</u>		<u>Mission 1028-2</u>	
	<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
Pitch Error ( $^{\circ}$ )	0.52	-1.35 to +1.00	0.76	-1.70 to +0.60
Roll Error ( $^{\circ}$ )	0.37	-0.40 to +0.90	0.52	-0.50 to +0.85
Yaw Error ( $^{\circ}$ )	0.50	-1.00 to +1.10	--	--
Pitch Rate ( $^{\circ}$ /hr.)	36.62	-70 to +100	42.7	-85 to +100
Roll Rate ( $^{\circ}$ /hr.)	28.02	-80 to +90	25.7	-90 to +85
Yaw Rate ( $^{\circ}$ /hr.)	30.47	-52 to +64	--	--

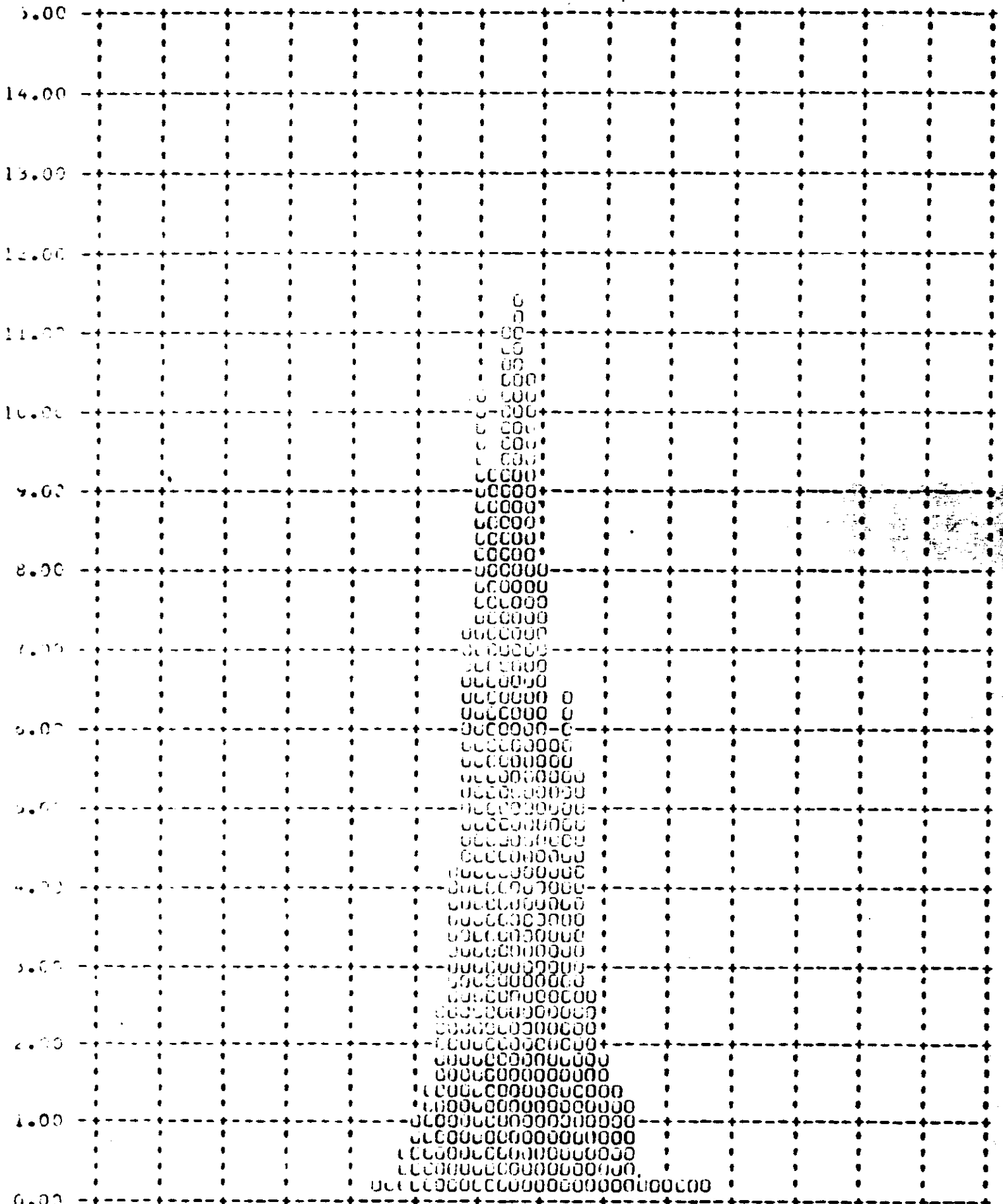
The performance of the attitude control system is comparable to the control systems used on recent missions. The panoramic photography was not degraded by the attitude control system.

-26 A-BUCKET FORWARD INSTRUMENT FRAMES 1-6 OF EACH OF OMITTED 90 PERCENT ± 0.52

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



-26 A-BUCKET FORWARD INSTRUMENT FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT - 0.50

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

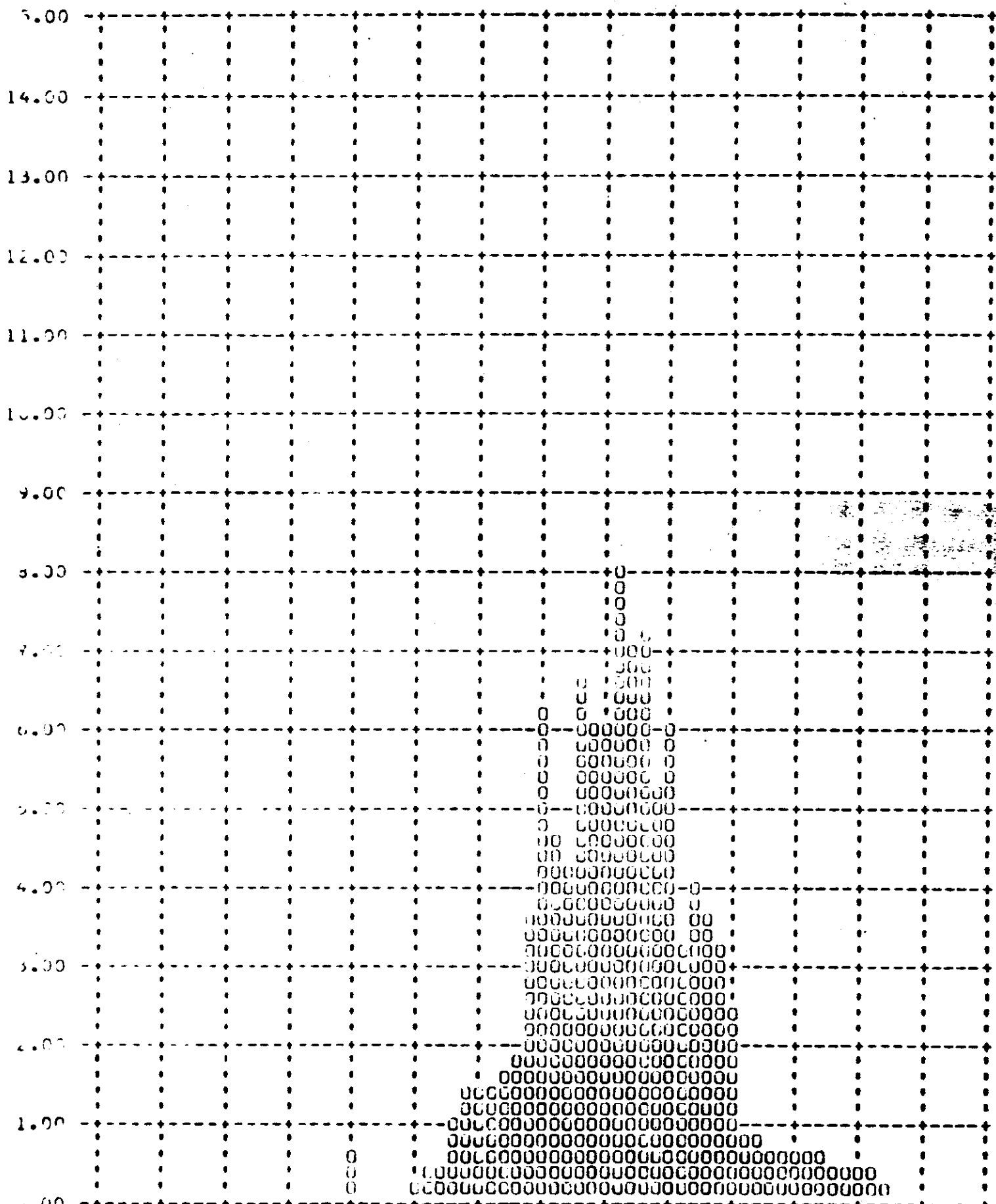
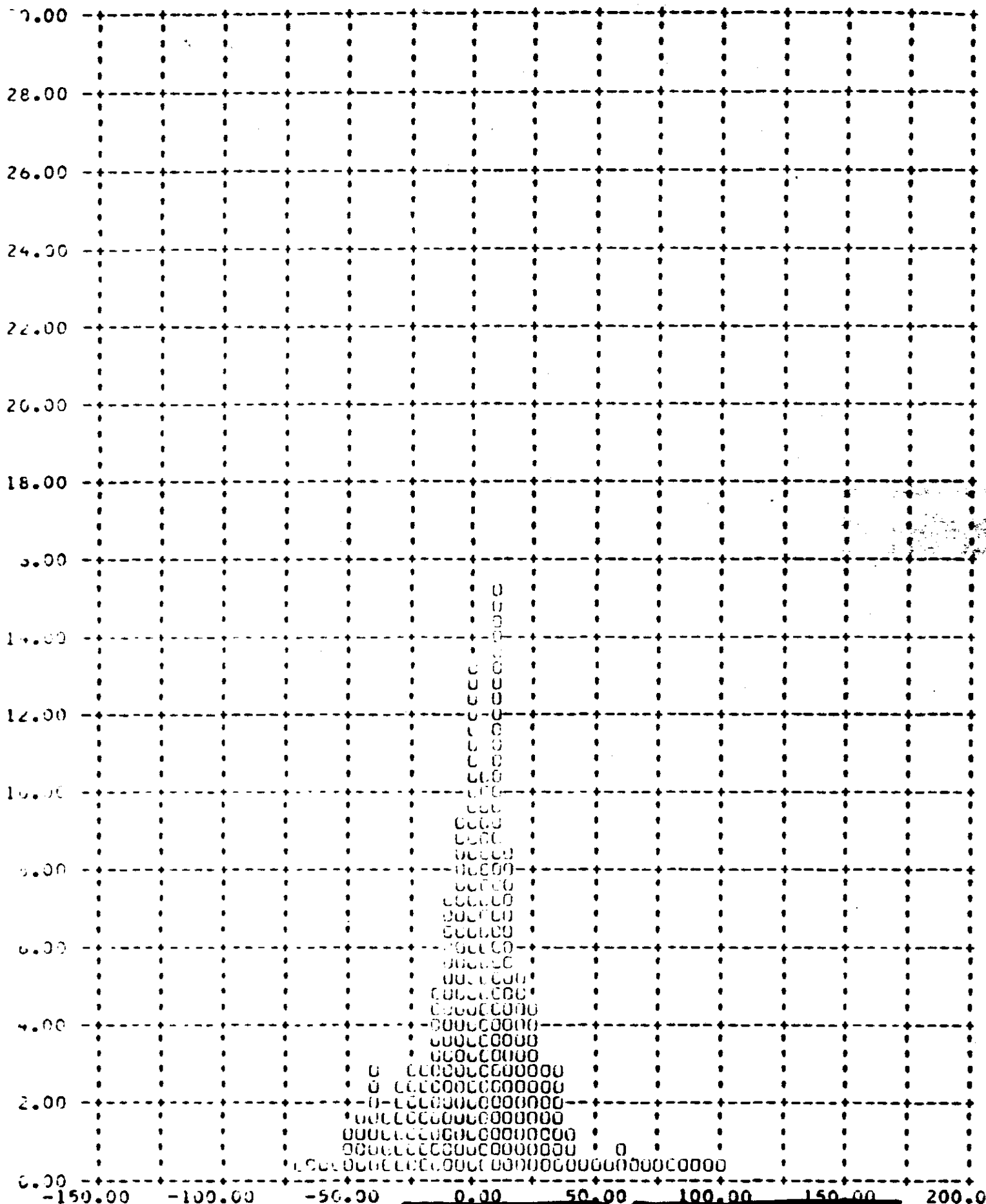


FIGURE 11-2

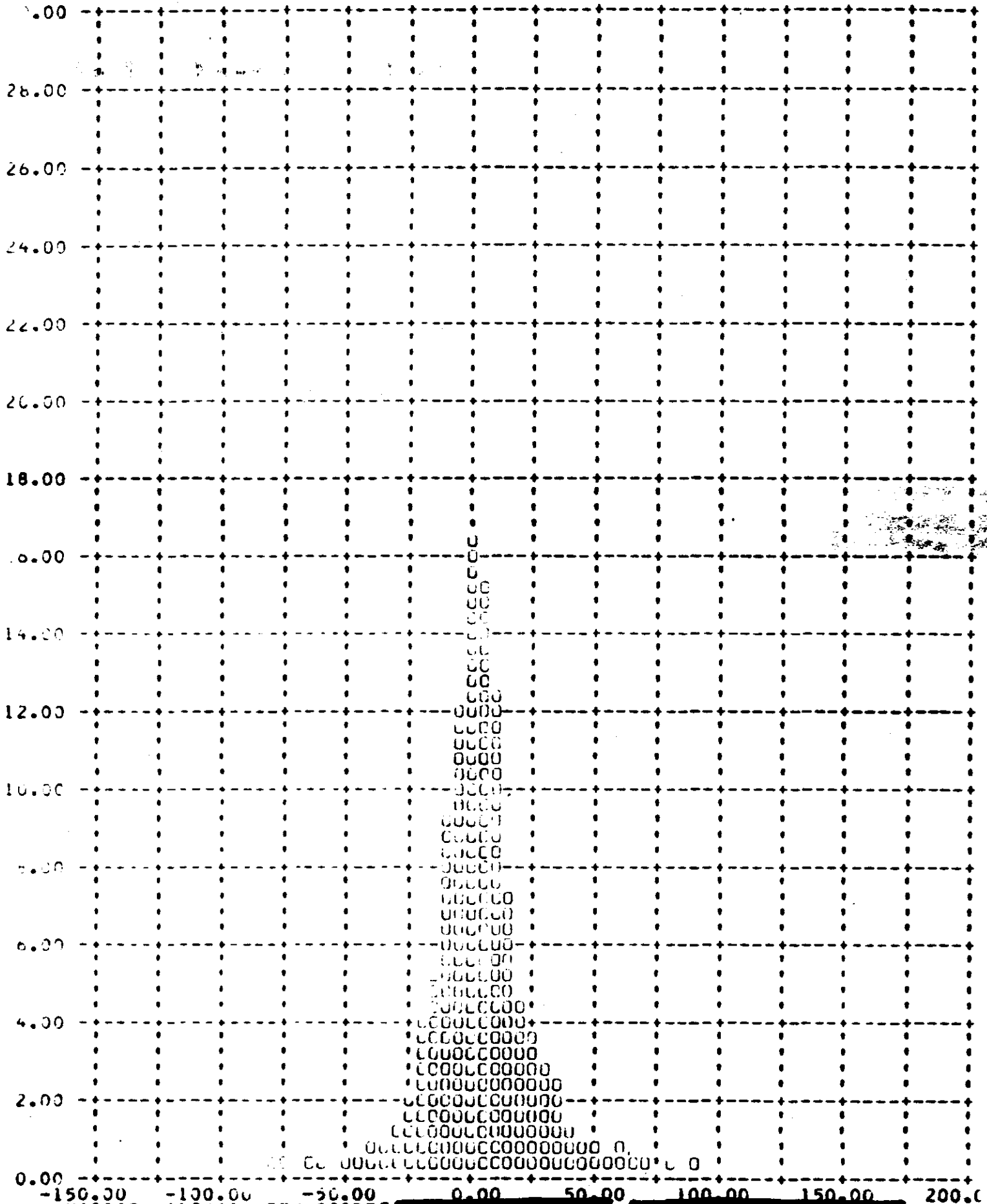
-26 A-BUCKET FORWARD INSTRUMENT FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 36.62

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



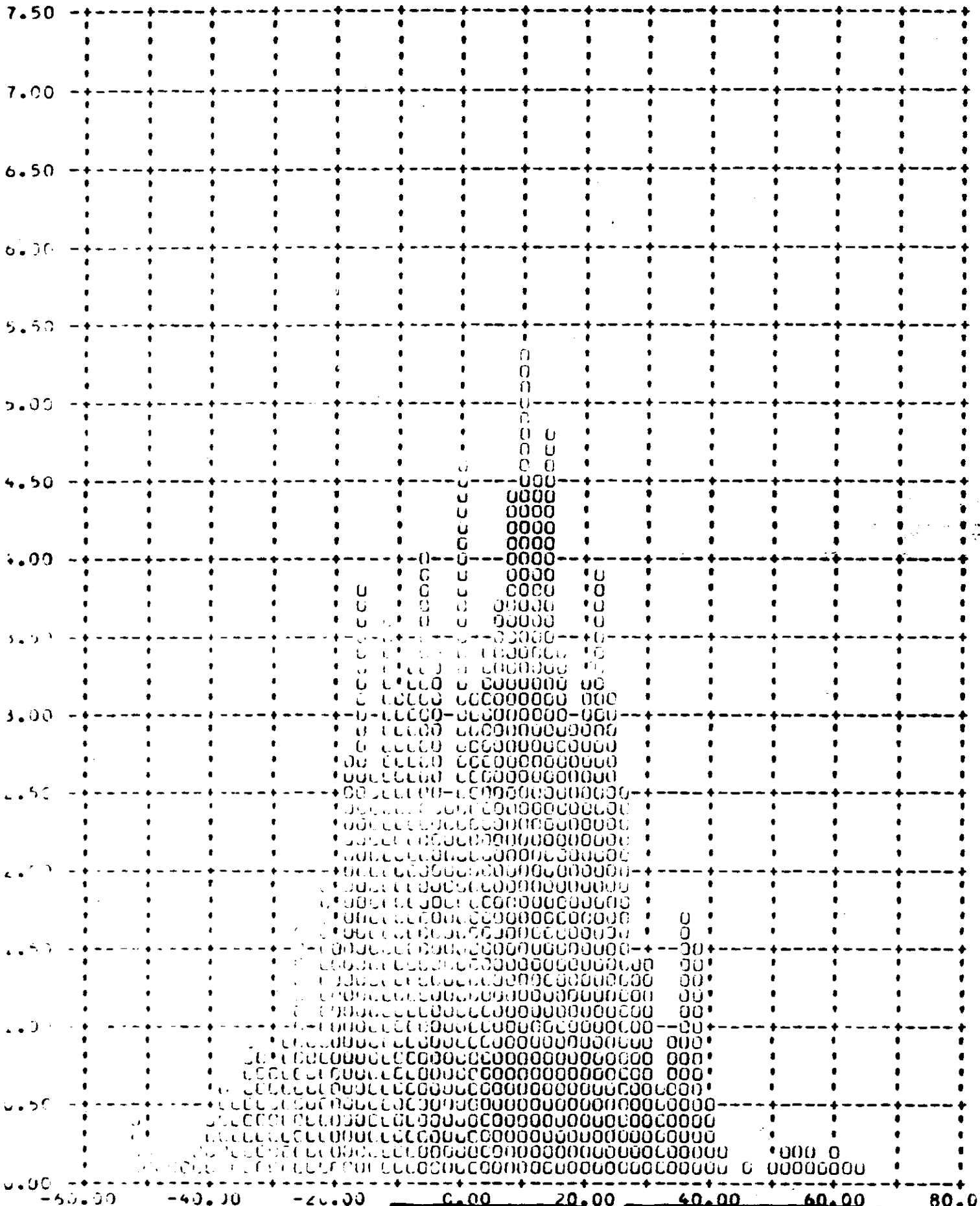
-26 A-BUCKET FORWARD INSTRUMENT FRAMES 1-6 OF EACH OP LIMITED 90 PERCENT = 28.02

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



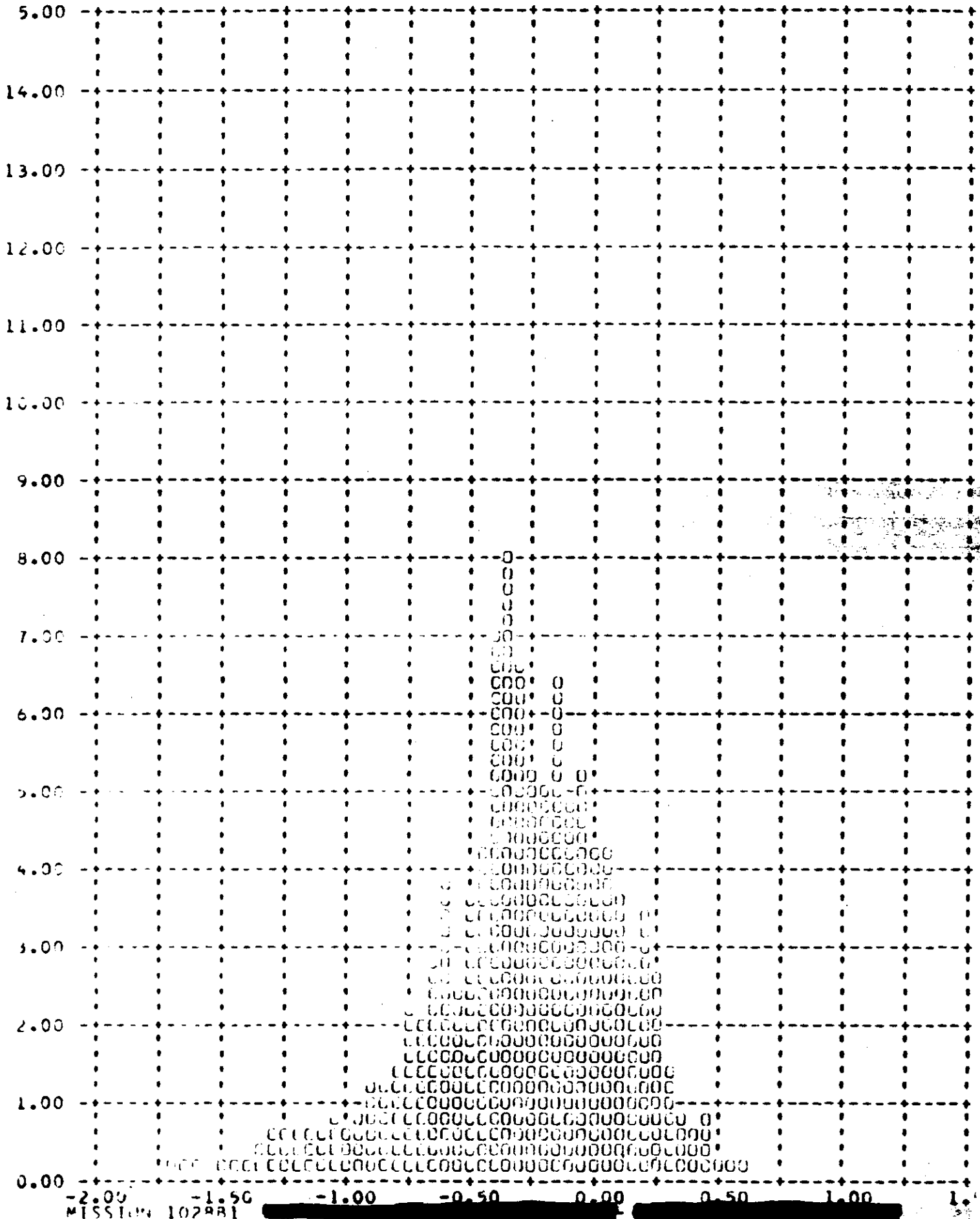
1-26 A-BUCKET FORWARD INSTRUMENT FRAMES 1-6 OF EACH OP OMITTED - 90 PERCENT = 30.47

YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

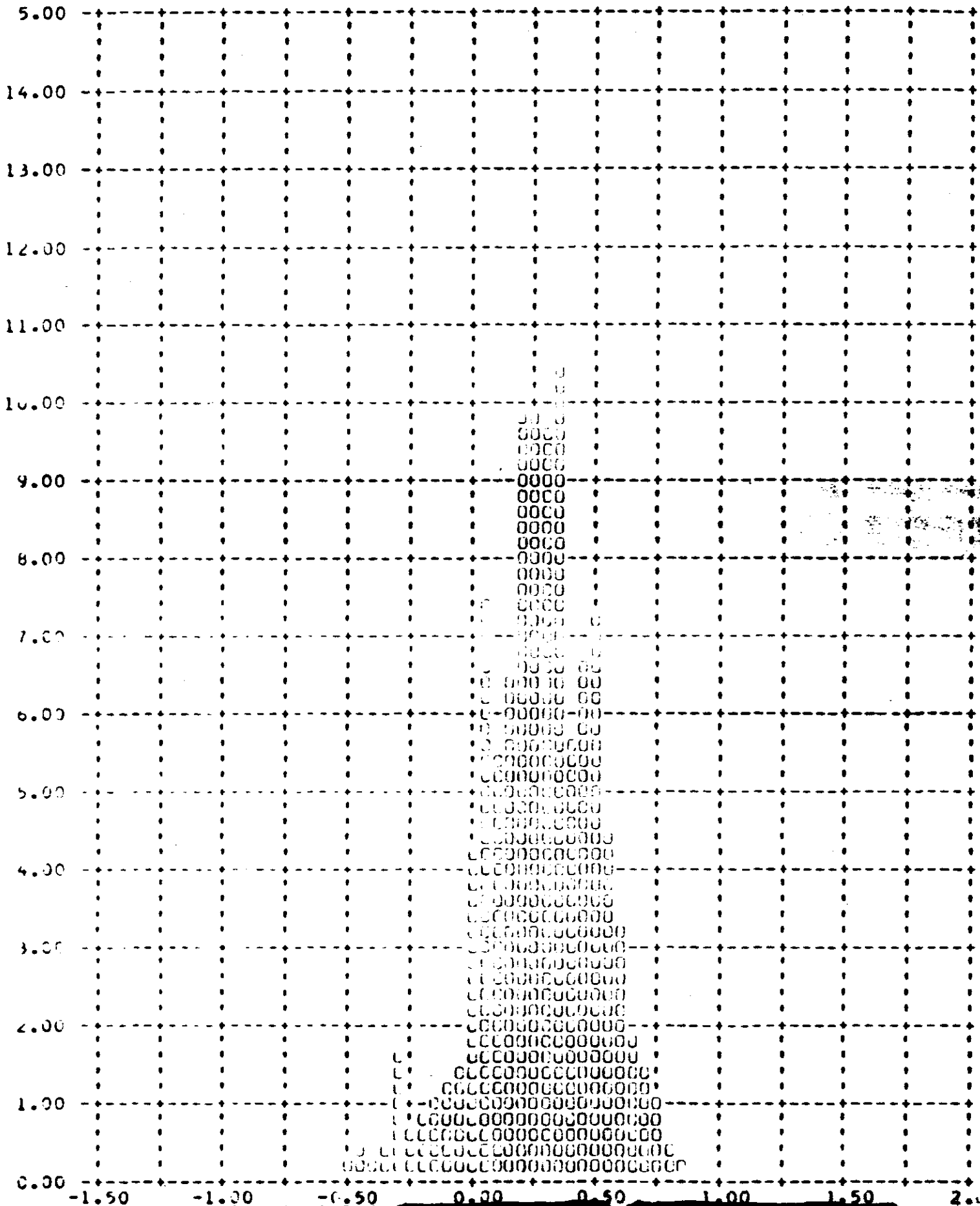




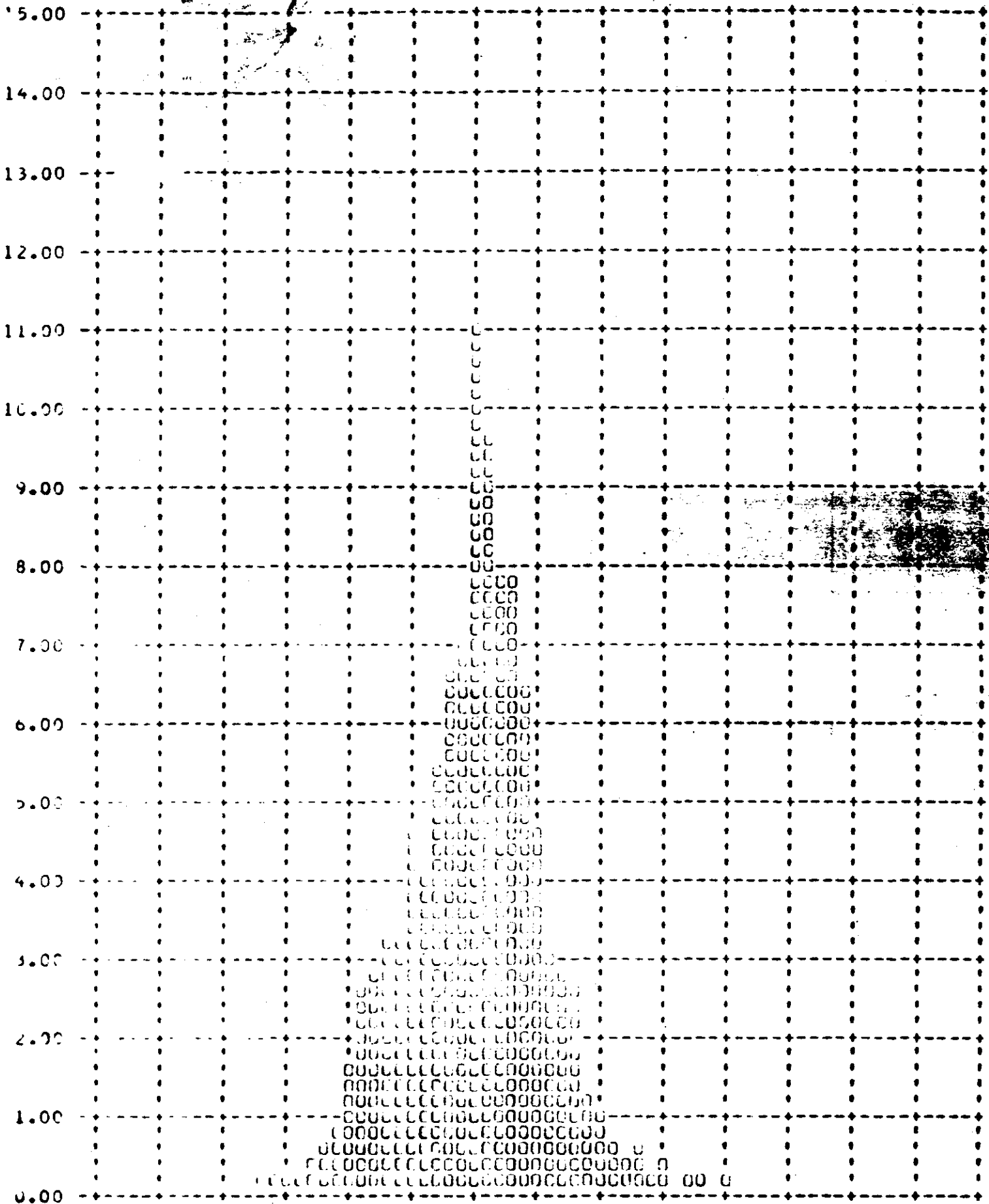
Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



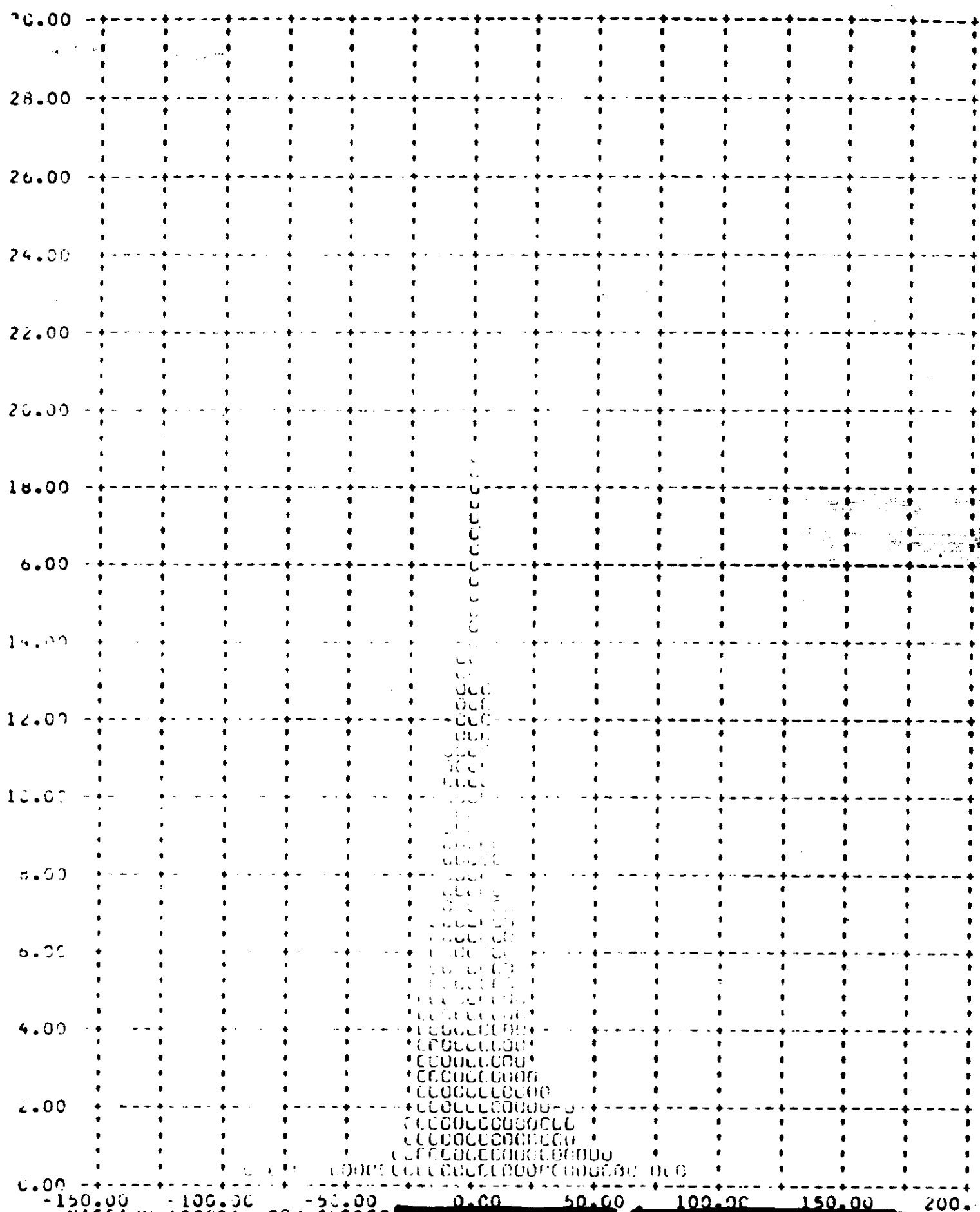
Y PITCH RATE ERROR DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



-150.00 -100.00 -50.00 0.00 50.00 100.00 150.00 200.00

J-26

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



-150.00 -100.00 -50.00 0.00 50.00 100.00 150.00 200.00

SECTION 15

IMAGE SMEAR ANALYSIS

The frame correlation tape supplied to A/P by NPIC contains the binary time word of each frame of photography. A computer program has been assembled at A/P which calculates the exposure time of each frame and compares the camera cycle rate with the ephemeris to calculate the V/h mismatch. This data is combined with the vehicle attitude error and rate values of each frame and the crab error caused by earth rotation at the latitude of each frame. The program outputs the total along track and cross track IMC error and the limit of ground resolution that can be acquired by a camera regardless of focal length and system capabilities.

The computer rejects the first six frames of all operations as the large V/h error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/h errors and resolution limits are computer plotted and are shown in Figures 15-1 through 15-10.

The summary table 15-1 presents the maximum V/h ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

SECTION 15

IMAGE SMEAR ANALYSIS

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The computer rejects the first six frames of all operations as the large V/h error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/h errors and resolution limits are computer plotted and are shown in Figures 15-1 through 15-10.

The summary table 15-1 presents the maximum V/h ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

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MISSION 1028

V/h RATIO AND RESOLUTION LIMITS

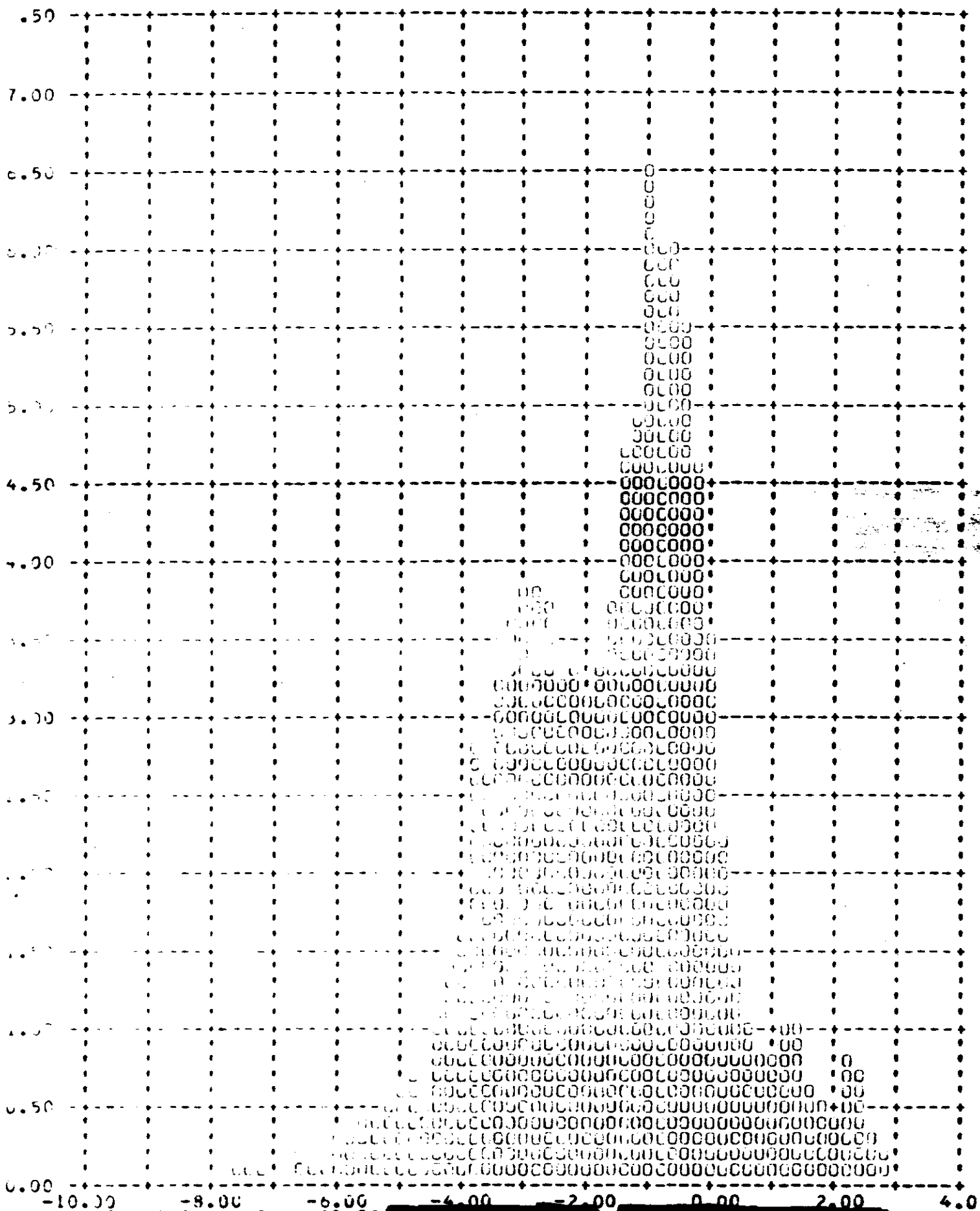
<u>Value</u>	<u>Units</u>	<u>Camera</u>	<u>Mission 1028-1</u>		<u>Mission 1028-2</u>	
			<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
V/h Ratio Error	%	FWD	3.86	-7.6 to +2.8	3.18	-6.0 to +2.18
		AFT	3.10	-8.2 to +3.4	2.85	-6.0 to +3.6
Along Track Resolution Limit	Feet	FWD	4.82	0.2 to 10.6	4.21	0.2 to 8.4
		AFT	3.96	0.2 to 8.2	3.34	0.2 to 6.6
Cross Track Resolution Limit	Feet	FWD	8.04	2.2 to 10.4	No Yaw Data	No Yaw Data
		AFT	5.61	1.6 to 7.2	No Yaw Data	No Yaw Data

TABLE 15-1

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-26 A-BUCKET FORWARD INSTRUMENT FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 3.86

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

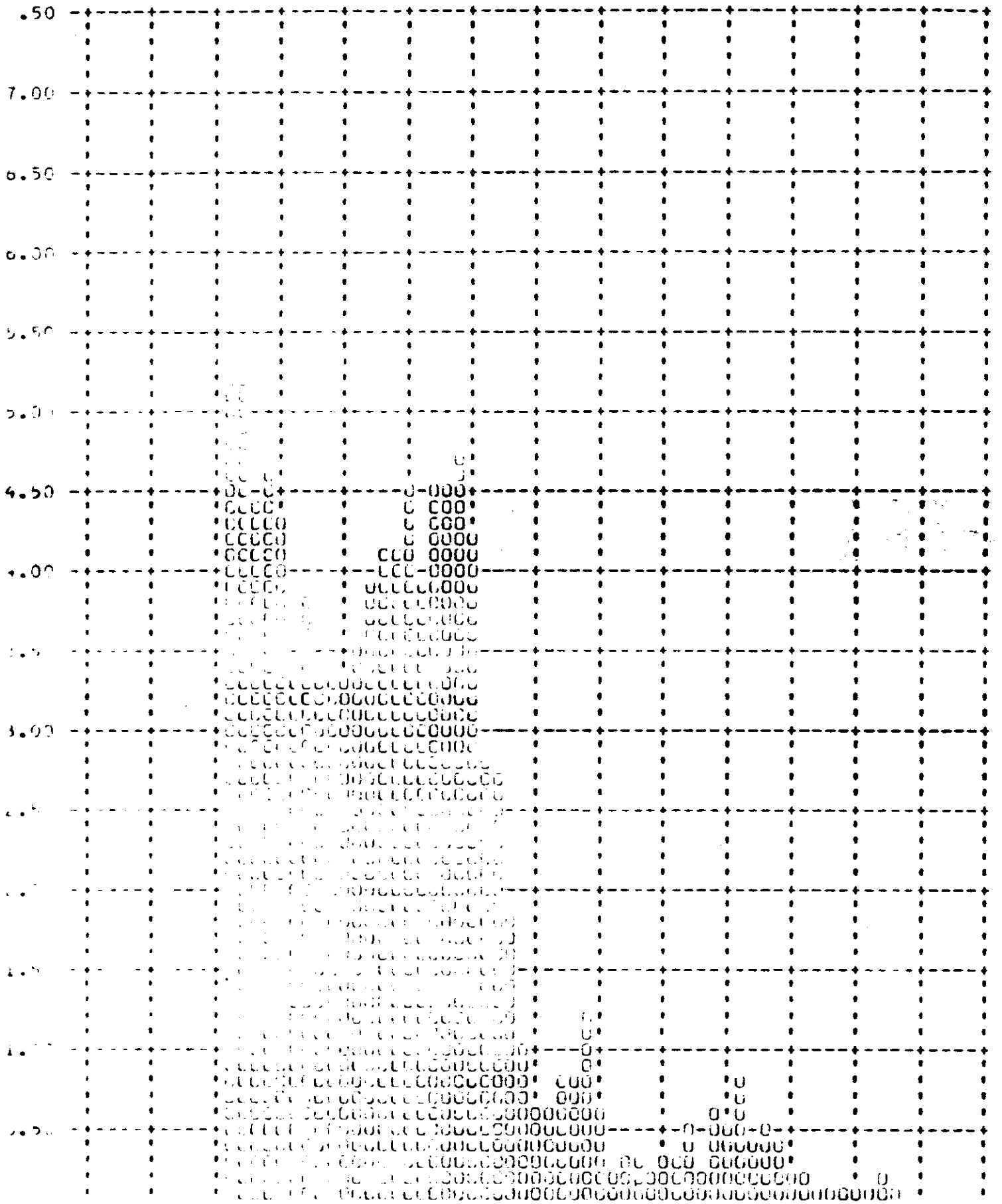


-10.00 -8.00 -6.00 -4.00 -2.00 0.00 2.00 4.00



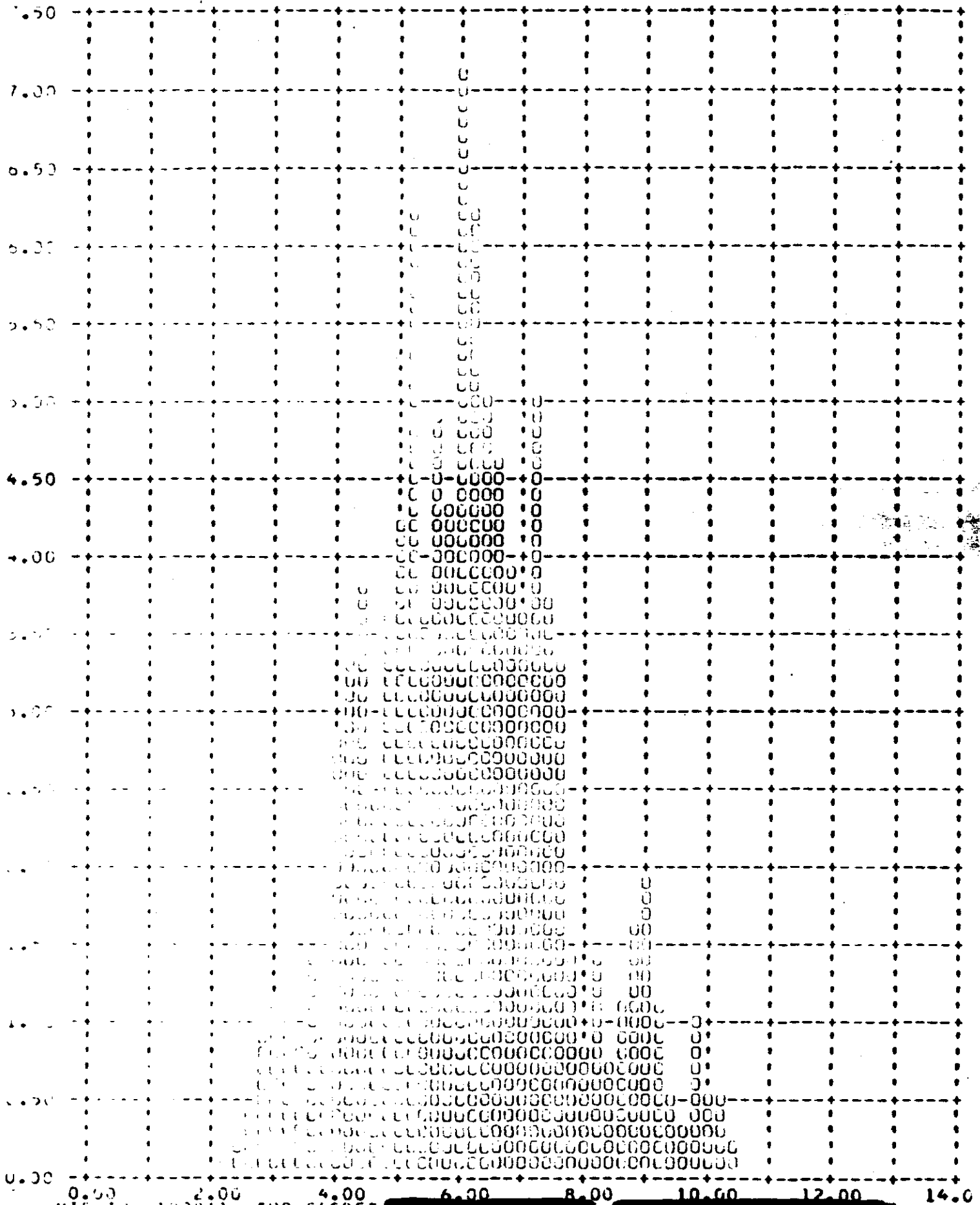
-26 A-BUCKET FORWARD INSTRUMENT FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 4.82

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



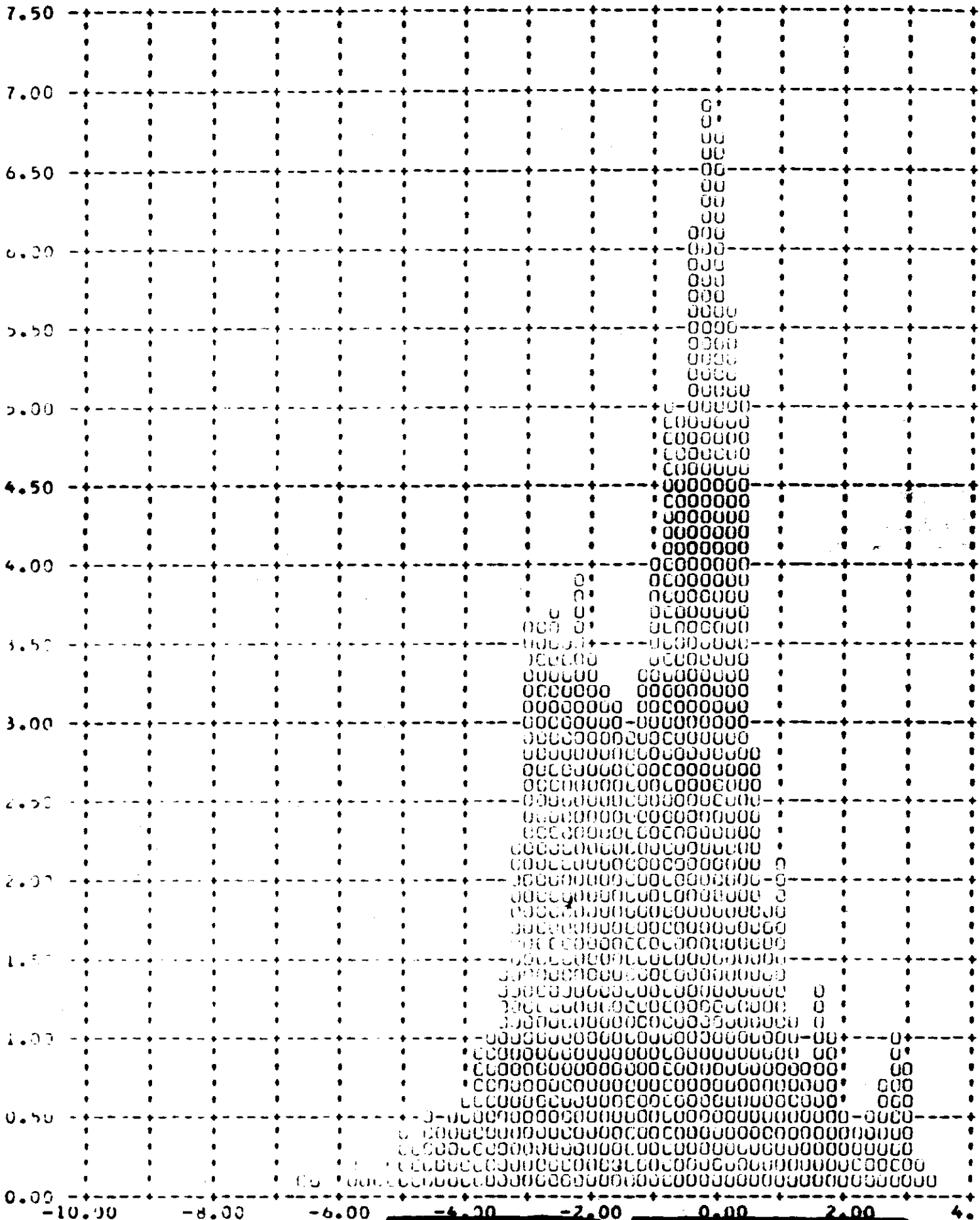
-26 A-BUCKET FORWARD INSTRUME FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 8.04

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



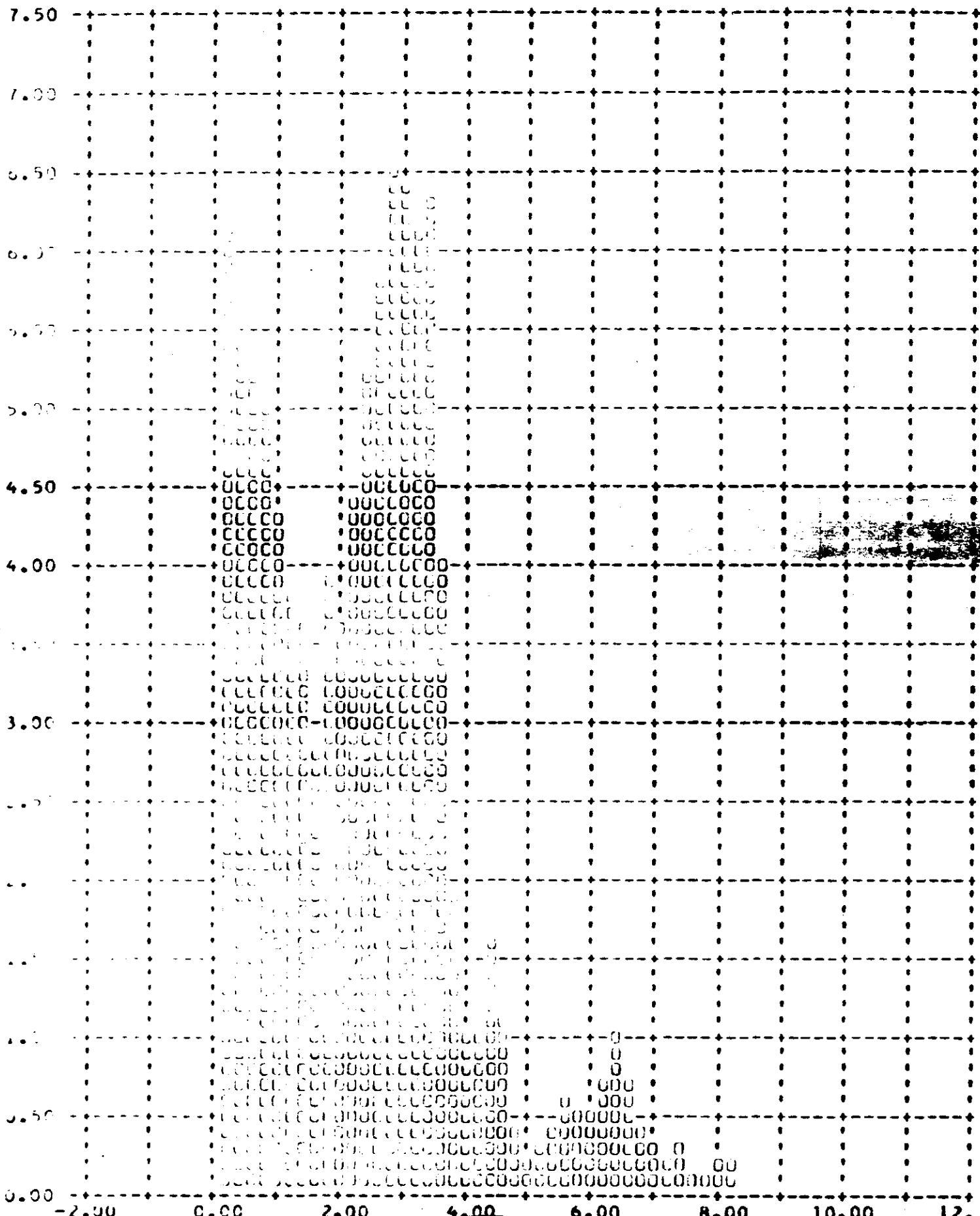
J-26 A-BUCKET AFT INSTRUMENT FRAMES 1-6 OF EACH OP. OMITTED 90 PERCENT = 3.10

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



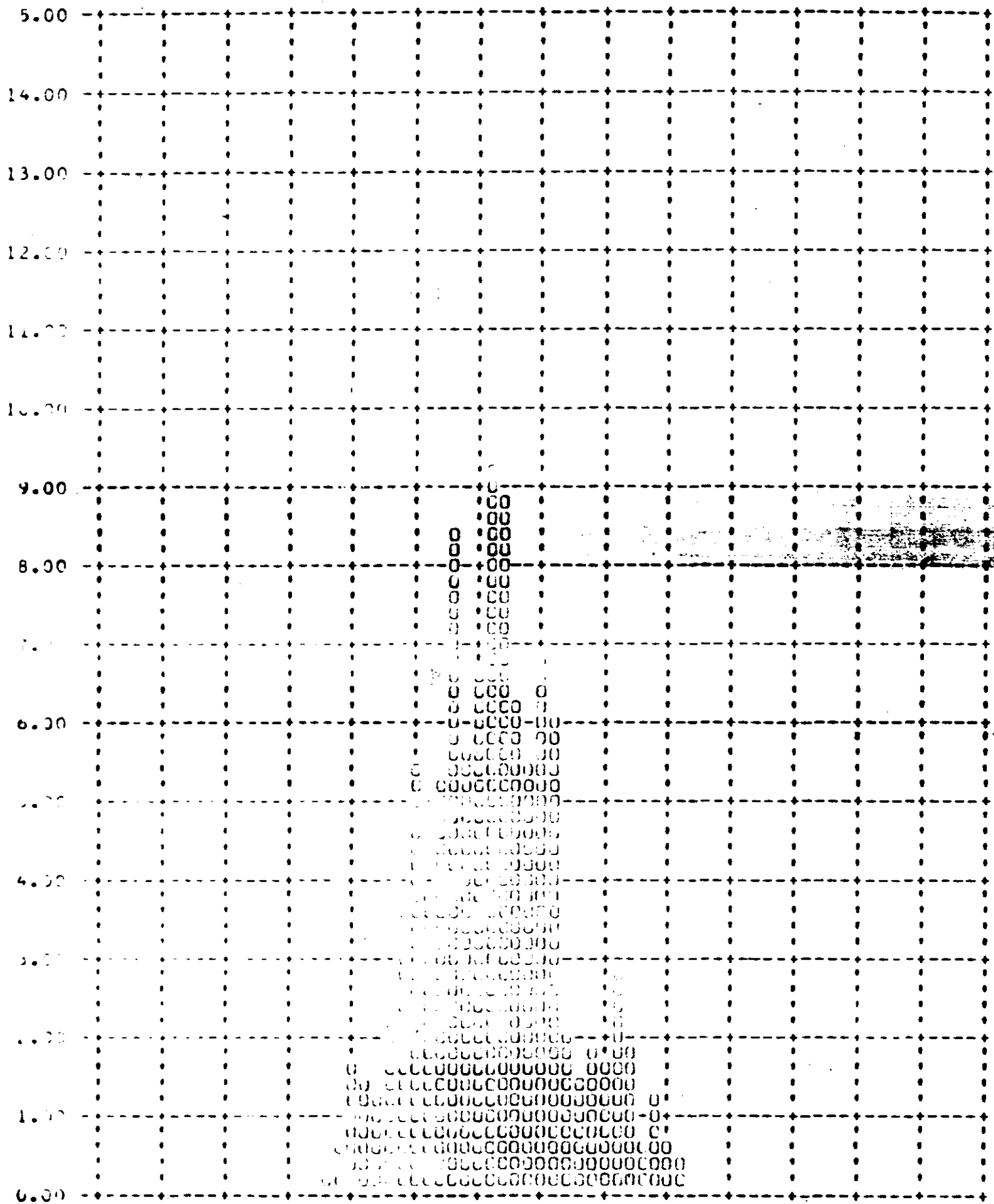
I-26 A-BUCKET AFT INSTRUMENT FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 3.96

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

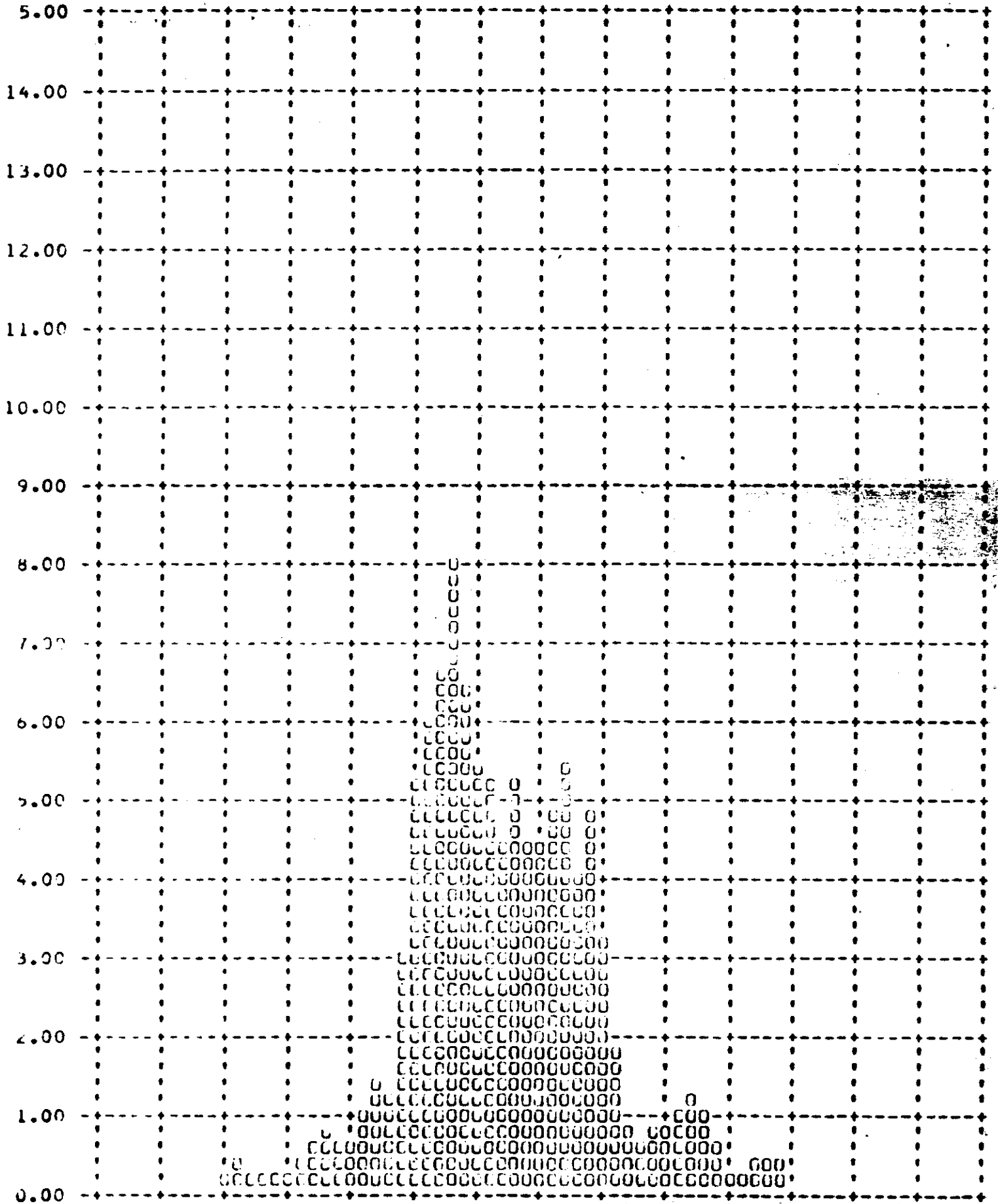


1-26 A-BUCKET AFT INSTRUMENT FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 5.61

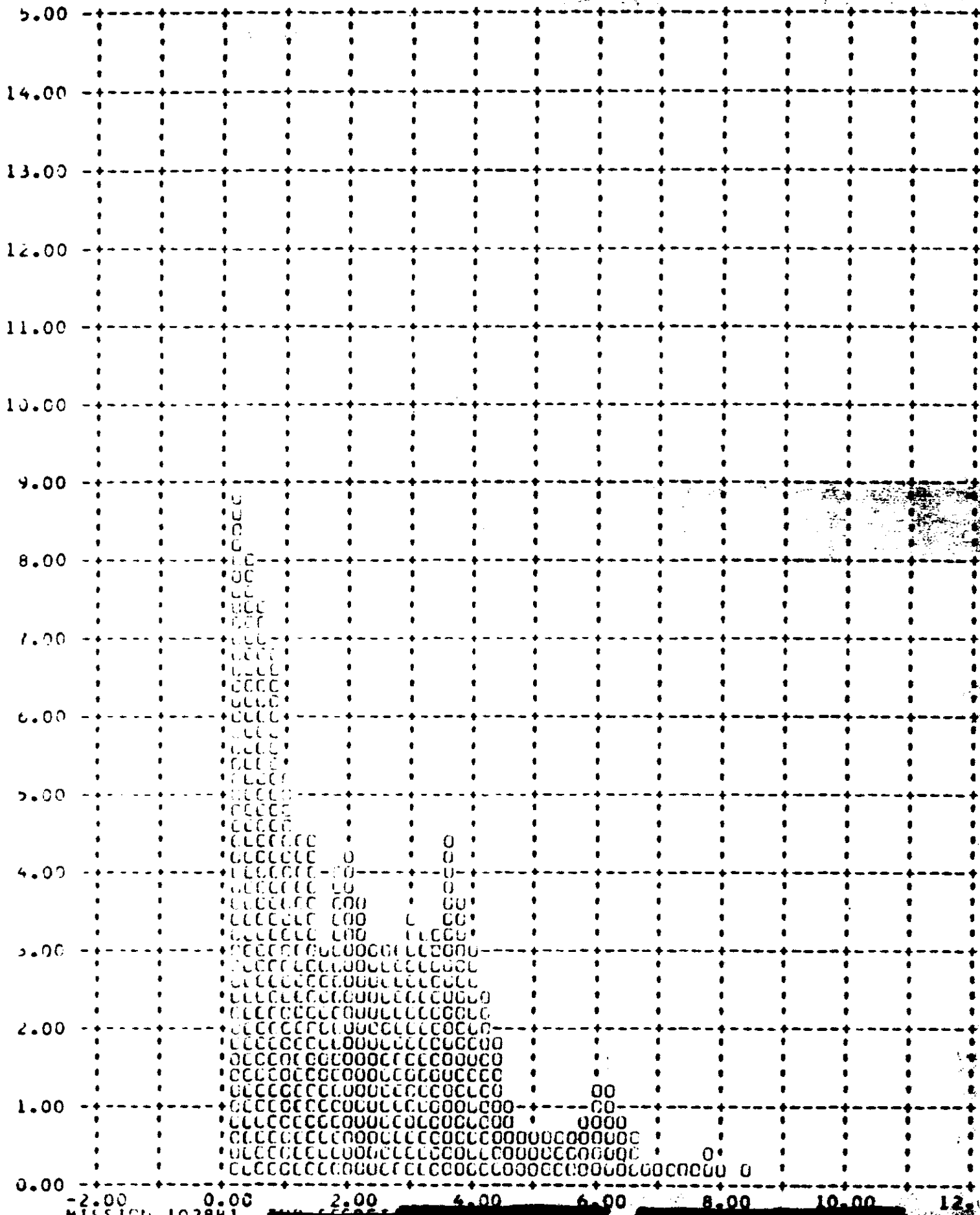
Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



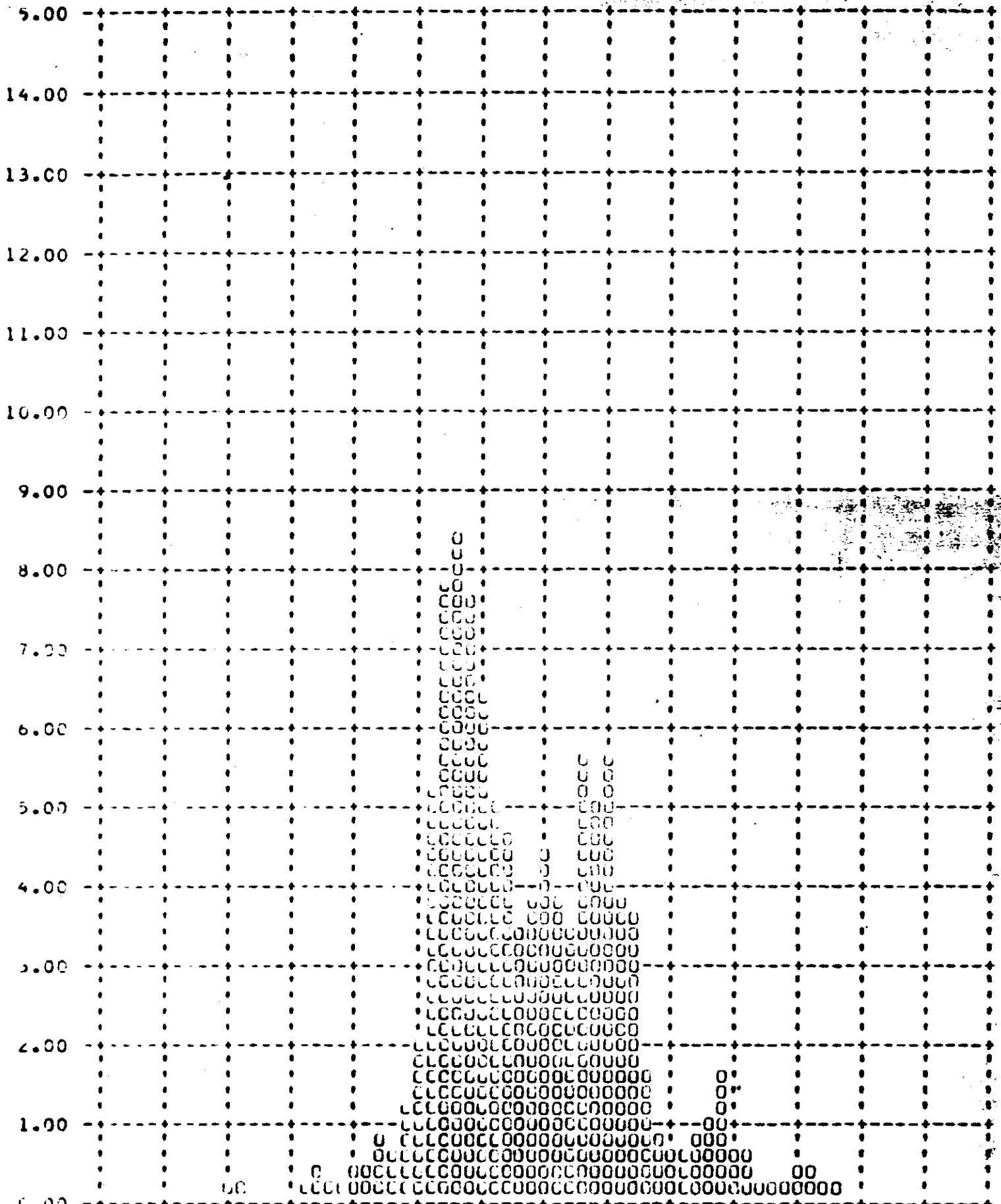
Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

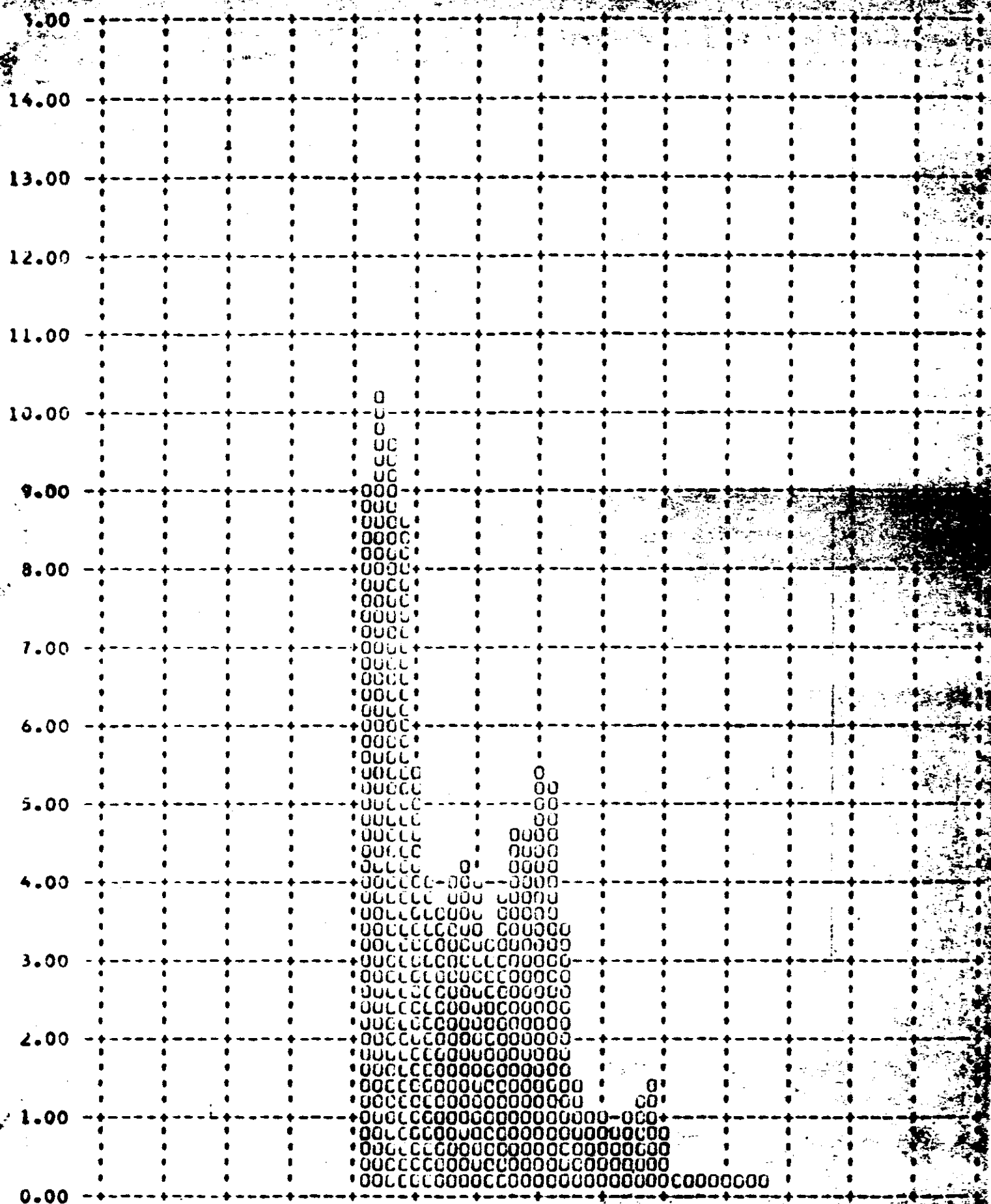


Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)





Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



SECTION 16

RADIATION DOSAGE

Each recovery system flown on a Corona mission contains a sealed packet of Eastman Type 3401 and Royal X Pan emulsions to determine the total radiation received at the take-up cassette. Both film types have been irradiated by LMSC at various levels and the base plus fog densities recorded after controlled processing.

Following recovery the film dosimeter packets are removed at A/P and processed with a pre-flight sample of the same film type and sensitometric control film. The resulting base plus fog density measurement of the dosimeter strips is used to ascertain the total radiation level. The table below presents the base plus fog readings for the dosimeter strips and the radiation level equivalents.

<u>Emulsion</u>	<u>Mission 1028-1</u>		<u>Mission 1028-2</u>	
	<u>B + F Density</u>	<u>Radiation</u>	<u>B + F Density</u>	<u>Radiation</u>
Type 3401	0.16	0.5 R	0.18	0.6 R
Royal X Pan	0.24	0.4 R	0.29	0.6 R

The mean total radiation seen by the take-up cassettes during both missions was approximately 0.5 roentgens. This level is below the level that will degrade the panoramic photography.

**Panoramic Camera Reliability**

Sample Size - 132 opportunities to operate.  
One failure - S/I Programmer on System J-19  
Assume - 3000 cycles per camera per mission.  
Estimated Reliability = 98.7% at 50% confidence level.

**Main Camera Door Reliability**

Sample Size - 46 vehicles x 2 doors = 92 opportunities to operate.  
Estimated Reliability = 99.2%

**Payload Command and Control**

Sample Size - 6960 hours operation in sample  
2 Failures  
Estimated Reliability = 96.4% at 50% confidence level.

**Payload Clock Reliability**

Sample Size - 6960 hours operation in sample.  
No Failures  
Estimated Reliability = 99.0% at 50% confidence level.

Estimated Reliability of Payload Functioning on Orbit = 96.7% at  
50% confidence level.

**Recovery System Reliability**

57 opportunities to recover  
1 Failure - improper separation due to water seal - cutter failure.  
Estimated Reliability = 97.1% at 50% confidence level.

**Stellar-Index Camera Reliability**

Sample begins with J5  
Sample Size = 16,015 cycles  
3 Failures  
Estimated Reliability = 90.7% at 50% confidence level.

### Horizon Camera Reliability

Sample begins with J5A

Sample Size - 67,500

Estimated Reliability of Single Camera - 98.5% at 50% confidence level.

Estimated Reliability of Four Horizon Cameras at a Parallel

Redundant System = 99.9% at 50% confidence level.

# ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS						ON-ORBIT FUNCTIONS	RECOVERY SYSTEM		SECONDARY FUNCTIONS	
	PANORAMIC CAMERA	PANORAMIC CAMERA DOORS	COMMAND & CONTROL SYSTEM	PAYLOAD CLOCK	ON-ORBIT FUNCTIONS	RECOVERY SYSTEM		STELLAR - INDEX CAMERAS	HORIZON CAMERAS		
	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	
9038 TO 1000	60 1 97.3	52 0 99.6	3124 0 98.0	3124 0 98.0	98.1	18 1 90.7	3400 3 83.1	12,000 0 91.7			
1009	64 1 97.4	3216 0 98.7	3216 0 98.0	3216 0 98.0	98.2	20 1 91.5	4280 3 69.3	18,000 0 93.4			
1010	68 1 97.6	3432 0 98.8	3432 0 98.1	3432 0 98.1	98.4	22 1 92.8	9100 3 73.7	18,000 0 94.4			
1011	72 1 97.7	3600 0 98.9	3600 0 98.1	3600 0 98.1	98.8	24 1 93.0	9325 0 94.7	21,000 0 98.2			
1012	76 1 97.8	3780 0 98.9	3780 0 98.2	3780 0 98.2	98.9	26 1 93.9	9825 0 94.7	24,000 0 98.9			
1013	78 1 97.8	3940 0 99.0	3940 1 98.9	3940 0 98.9	98.0	28 1 94.0	9960 0 96.1	28,500 0 98.3			
1014	82 1 97.9	4006 0 99.0	4006 1 98.1	4006 0 98.3	98.1	30 1 94.4	4373 1 89.8	28,800 0 98.0			
1015	86 1 98.0	4380 0 99.0	4380 1 98.3	4380 0 98.4	98.1	32 1 94.8	7225 1 90.4	31,800 0 98.9			
1016	90 1 98.1	4660 0 99.0	4660 1 98.5	4660 0 98.5	98.4	34 1 96.2	7650 1 91.0	34,800 0 97.8			
1017	94 1 98.3	4780 0 99.0	4780 1 98.7	4780 0 98.8	97.6	36 1 96.4	9985 1 92.3	37,800 0 97.3			
1018	98 1 98.3	4920 0 99.1	4920 1 98.8	4920 0 98.7	98.7	38 1 96.6	9960 1 92.3	40,800 0 97.8			
1019	102 1 98.4	5126 0 99.1	5126 1 98.9	5126 0 98.7	98.8	39 1 98.8	9075 1 91.8	43,800 0 97.8			

0 DENIES PER MONTHS SYSTEMS FAILING OPERATIONS

Table 17-1

17. AND UNDER SET OF RECORDS

# ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS				SECONDARY FUNCTIONS			
	PANORAMIC CAMERA	PANORAMIC CAMERA DOORS	COMMAND & CONTROL SYSTEM	PAYLOAD GLOCK	OR - ORBIT FUNCTIONS	RECOVERY SYSTEM	STELLAR - INDEX CAMERAS	HORIZON CAMERAS
	SAMPLES RELIABILITY	SAMPLES FAILURES RELIABILITY	SAMPLES FAILURES RELIABILITY	SAMPLES FAILURES RELIABILITY	RELIABILITY	SAMPLES FAILURES RELIABILITY	SAMPLES FAILURES RELIABILITY	SAMPLES FAILURES RELIABILITY
1020	108 98.5	78 0 99.1	5944 1 97.1	5344 0 98.9	98.9	43 1 96.1	10,680 2 99.9	48,000 0 97.9
1021	104 98.5	76 0 99.1	5376 1 97.0	5376 0 98.8	98.9	41 1 96.0	9930 2 99.1	46,800 0 97.8
1022	112 98.5	80 0 99.2	5784 1 97.3	5784 0 98.9	98.9	45 1 94.3	11,550 2 90.7	51,000 0 98.0
1023	114 98.6	82 0 99.2	6000 2 95.2	6000 0 98.9	98.2	47 1 96.5	12,190 2 91.1	54,000 0 98.1
1024	118 98.6	84 0 99.2	6240 2 96.0	6240 0 98.9	98.3	49 1 96.6	13,040 2 91.6	57,000 0 98.2
1025	122 98.6	86 0 99.2	6480 2 96.1	6480 0 99.0	98.4	51 1 98.7	13,990 2 92.1	60,000 0 98.3
1026	126 98.7	88 0 99.2	6720 2 96.3	6720 0 99.0	98.5	53 1 96.8	14,740 2 92.6	63,000 0 98.4
1027	128 98.7	90 0 99.2	6744 2 96.3	6744 0 99.0	98.5	55 1 97.0	15,198 3 90.0	64,800 0 98.4
1028	132 98.7	92 0 99.2	6960 2 96.4	6960 0 99.0	98.7	57 1 97.1	16,018 3 90.7	67,800 0 98.6

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SECTION 18

SUMMARY DATA

The comparison of the operating parameters and the performance achieved by previous missions has been difficult due to the large volume of data that results from each mission. Some of the pertinent characteristics from prior missions have been summarized in Tables 18-1 through 18-3.

The summary data was started with Mission 1004 as the J-05 camera system was the first to incorporate the major modifications of the titanium drum and scan arm, four roller scan head and Corona J capabilities. Only those missions that culminated in the recovery of some photography have been listed, therefore Mission 1003 and 1005 are deleted.

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# MISSION SUMMARY

MISSION NUMBER	PAYLOAD NUMBER	VEHICLE NUMBER	LAUNCH DATE	LAUNCH TIME	ORBIT INCLINATION (°)	PERIGEE		RECOVERY PASS	MASTER CAMERA		SLAVE CAMERA		STELLAR-INDEX CAMERA NUMBER				
						ALTITUDE (NM)	LOCATION (°N)		CAMERA NUMBER	SLIT (")	FILTER TYPE	CAMERA NUMBER		SLIT (")	FILTER TYPE		
1004	J-09	1174	2/19/64	2138 Z	74.9	99.9	29.0	49	112	124	0.250	W-21	129	0.250	W-21	D59/89/89	942/46/87
1006	J-09	1176	6/4/64	2258 Z	79.9	84.0	63.2	98	128	148	0.200	W-21	149	0.200	W-21	D45/47/46	049/33/42
1007	J-07	1609	6/19/64	2318 Z	85.0	99.2	41.8	85	128	144	0.250	W-25	145	0.200	W-21	D43/43/43	054/56/91
1008	J-10	1177	7/10/64	2314 Z	85.0	99.4	40.8	49	112	150	0.200	W-21	151	0.200	W-21	D48/48/48	033/28/33
1009	J-12	1608	8/8/64	2316 Z	80.1	99.6	39.5	49	128	154	0.200	W-21	156	0.200	W-21	D36/84/86	028/28/24
1010	J-11	1178	9/14/64	2254 Z	84.9	97.4	42.3	65	144	152	0.175	W-21	153	0.175	W-21	D41/41/41	044/36/44
1011	J-3K	1170	10/9/64	2150 Z	79.9	99.3	20.9	65	—	160	0.175	W-21	161	0.175	W-21	D30/30/30	087/87/87
1012	J-13	1179	10/17/64	2202 Z	75.0	96.2	32.4	49	81	156	0.200	W-21	157	0.200	W-21	D31/31/47	046/28/23
1013	J-18	1173	11/2/64	2130 Z	80.0	100.0	25.0	85	81	158	0.225	W-21	159	0.225	W-21	D82/49/86	047/68/74
1014	J-18	1180	11/8/64	2036 Z	70.0	103.2	65.6	81	145	162	0.250	W-25	159	0.175	W-21	D53/59/49	047/68/74
1016	J-17	1607	12/18/64	2110 Z	74.9	96.7	21.6	81	128	136	0.250	W-25	141	0.175	W-21	D61/61/61	060/44/46
1016	J-18	1608	1/18/66	2101 Z	74.9	99.4	30.2	81	159	132	0.250	W-25	133	0.175	W-21	D55/58/50	039/28/28
1017	J-19	1611	2/25/66	2144 Z	75.0	97.2	25.9	91	145	140	0.250	W-25	165	0.175	W-21	D81/81/81	060/44/46
1018	J-19	1612	3/23/66	2111 Z	96.0	100.2	40.3	66	99	122	0.250	W-25	123	0.175	W-21	D50/50/50	062/28/28
1019	J-04	1614	4/29/66	2144 Z	85.0	99.1	27.1	80	—	118	0.250	W-25	119	0.175	W-21	D38/38/38	062/28/28
1020	J-20	1613	6/9/66	2158 Z	75.1	97.1	40.6	97	118	136	0.250	W-25	137	0.175	W-21	D47/69/69	048/28/48
1021	J-21	1615	5/18/65	1903 Z	75.0	109.2	24.5	81	161	166	0.175	W-21	167	0.250	W-25	D63/69/69	063/69/69
1022	J-22	1617	7/19/65	2201 Z	85.0	99.7	30.3	86	144	168	0.250	W-25	169	0.175	W-21	D48/77/77	063/69/69
1023	J-23	1618	8/17/65	2100 Z	70.0	97.8	29.0	81	144	170	0.225	W-25	171	0.150	W-21	D17/19/82	068/28/72
1024	J-24	1619	9/22/65	2131 Z	80.0	96.9	18.4	81	161	172	0.225	W-25	173	0.150	W-21	D49/72/64	068/28/72
1025	J-25	1616	10/9/65	1746 Z	75.0	115.9	44.3	81	161	142	0.175	W-21	127	0.175	W-21	D73/78/88	068/28/72
1026	J-26	1620	12/28/65	2117 Z	75.0	95.0	17.0	81	161	174	0.225	W-25	175	0.150	W-21	D75/82/83	070/28/28
1027	J-27	1621	12/19/65	2110 Z	80.0	97.4	17.3	81	161	164	0.250	W-25	163	0.175	W-21	D71/87/87	070/28/28
1028	J-28	1610	12/24/65	2106 Z	90.0	97.6	26.4	81	145	176	0.250	W-25	177	0.175	W-21	D77/94/97	070/28/28

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TABLE 18-1



# PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA	SERIAL NUMBER	M I P VALUE	VISUAL RES	MTF/AM		SLIT AVERAGE (μ)	SLIT AVERAGE (μ)	90% ATTITUDE ERROR (°)			90% ATTITUDE RATES (7HR)			90% V/H ERROR (°)	90% RESOLUTION (MT)	
					AVERAGE (μ)	SLIT (μ)			PITCH	ROLL	YAW	PITCH	ROLL	YAW		ALONG TRACK	CROSS TRACK
1004-1	FWD APT	124	85	78	97	109	350	115	0.45	0.42	1.08	30.0	25.0	21.0	8.1	7.7	9.1
1004-2	FWD APT	128	85	73	88	113	320	117	0.74	0.50	0.91	44.0	30.0	29.0	4.9	6.6	6.6
1006-1	FWD APT	148	90	78	83	108	350	84	0.41	0.42	1.14	26.6	28.5	27.6	15.4	13.6	8.7
1006-2	FWD APT	149	90	83	84	101	350	84	0.49	0.40	1.08	31.1	27.9	30.0	11.6	10.1	7.0
1007-1	FWD APT	144	85	80	80	107	350	82	0.58	0.46	1.43	37.6	23.9	29.9	3.6	3.1	3.4
1007-2	FWD APT	148	88	81	81	101	350	88	0.64	0.47	—	43.0	25.8	—	4.6	2.1	7.6
1008-1	FWD APT	150	85	80	80	107	350	81	0.59	0.39	0.94	43.8	23.9	29.6	2.9	4.9	9.9
1008-2	FWD APT	151	85	82	84	106	350	85	0.63	0.36	0.71	42.9	24.0	32.5	2.8	4.2	8.4
1009-1	FWD APT	154	88	92	80	95	350	75	0.65	0.65	0.71	29.2	22.7	27.6	3.3	5.3	9.8
1009-2	FWD APT	158	85	87	85	91	350	72	0.48	0.65	0.59	33.6	23.9	27.2	2.6	4.9	9.8
1010-1	FWD APT	152	85	86	80	98	350	87	0.93	0.30	0.87	39.1	23.6	30.8	4.9	2.3	4.4
1010-2	FWD APT	153	85	80	82	92	350	82	0.59	0.70	1.21	45.4	23.6	30.7	4.6	7.8	9.8
1011-1	FWD APT	160	90	84	78	98	350	83	0.77	0.39	0.97	43.1	28.9	31.1	2.3	9.3	9.9
1012-1	FWD APT	166	85	92	81	91	350	84	0.65	0.51	—	47.1	33.2	—	1.8	4.8	—
1012-2	FWD APT	157	85	89	85	94	350	85	0.97	0.77	0.51	45.2	30.7	20.4	5.9	3.3	9.9
1013-1	FWD APT	159	85	89	89	94	350	81	0.84	0.32	1.34	38.9	29.0	32.3	3.7	7.8	9.3
1014-1	FWD APT	162	80	87	78	88	350	74	0.82	0.41	1.48	35.0	36.1	38.5	2.2	6.2	9.9
1014-2	FWD APT	139	80	83	80	85	350	70	1.06	0.66	—	34.8	36.0	36.3	3.3	2.8	6.3
1016-1	FWD APT	138	85	87	76	80	350	80	1.08	0.89	—	38.1	36.0	—	3.2	2.2	—
1016-2	FWD APT	141	85	83	73	75	350	97	0.84	0.39	0.53	47.0	29.4	39.2	5.0	6.8	7.8
1016-1	FWD APT	132	88	85	72	72	350	89	0.50	0.61	0.64	39.1	27.0	34.3	3.3	4.6	7.1
1016-2	FWD APT	123	85	91	72	72	350	90	0.50	0.61	0.64	39.1	27.0	34.3	3.3	4.6	7.1
1017-1	FWD APT	140	85	78	87	80	350	81	0.72	0.83	2.01	48.9	30.2	40.4	2.0	5.9	10.9
1017-2	FWD APT	169	85	88	70	70	350	94	0.72	0.83	2.01	48.4	30.1	40.4	2.0	5.9	10.9
1018-1	FWD APT	182	85	79	82	82	350	82	0.83	0.93	2.19	42.2	27.3	39.9	1.5	3.3	9.1
1018-2	FWD APT	183	88	88	77	71	350	82	0.91	0.48	—	47.4	36.7	—	3.4	9.4	—

# PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA	SERIAL NUMBER	M I P VALUE	VISUAL RES	AFSPF		WTF/AIM	SLY		RELEASES		90% ATTITUDE ERROR (°)			90% V/H ERROR (M)			90% RESOLUTION ALONG TRACK		CROSS TRACK
					AVERAGE	SLY		ALL	HIGH	PITCH	ROLL	YAW	PITCH	ROLL	YAW	90% V/H	ALONG TRACK			
1019-1	FWD AFT	118 119	88	81 86	—	—	80	75 63	80 87	88 87	104 101	0.43 0.37	0.89 0.96	31.8 34.7	34.7 33.0	3.3 3.3	9.3 5.0	—	—	—
1020-1	FWD AFT	136	80	88	—	—	80	82	80	78	90	0.46	0.85	37.4	31.8	3.4	9.8	—	—	—
1020-2	FWD AFT	137	—	89	—	—	—	82	—	94	105	0.46 0.41	0.78 1.06	37.4 42.6	31.8 42.5	3.3 3.5	6.4 4.5	—	—	—
1021-1	FWD AFT	166	88	88	—	—	80	77	80	86	99	0.55	0.81	34.9	32.6	2.7	8.8	—	—	—
1021-2	FWD AFT	167	88	88 74	—	—	80	74 82	80	96 88	109 112	0.38 0.89	0.81	34.8 44.7	33.0 50.6	3.1	8.6 9.2	—	—	—
1022-1	FWD AFT	166	88	88	—	—	80	88	80	78	81	0.47	0.89	28.3	27.1	3.9	9.8	—	—	—
1022-2	FWD AFT	169	88	81 80 82	—	—	80	83 88 82	80	101 74 99	111 84 110	0.47 0.40	0.90 0.90	27.9 29.4	26.6 27.3	3.0 2.6	6.2 4.9	—	—	—
1023-1	FWD AFT	170	88	—	—	—	80	84	80	97	110	0.49	0.90	33.0	28.7	3.4	4.0	—	—	—
1023-2	FWD AFT	171	88	—	—	—	80	71 88	80	83 76	101 87	0.48 0.42	0.90 0.93	28.7 29.6	26.6 21.3	3.5 2.9	2.7 2.7	—	—	—
1024-1	FWD AFT	172	88	—	—	—	80	79	80	90	102	0.42	0.82	32.2	24.9	2.6	9.9	—	—	—
1024-2	FWD AFT	173	88	—	—	—	80	95 86 95	80	94 89 100	105 101 114	0.42 0.36 0.36	0.82 0.93 0.93	30.4 30.4 30.6	24.9 24.5 23.6	2.1 5.5	3.8 4.7 3.3	—	—	—
1025-1	FWD AFT	148	85	—	—	—	80	87	80	80	97	0.90	0.41	28.1	28.7	2.0	3.9	—	—	—
1025-2	FWD AFT	187	88	—	—	—	80	85	80	101 96	114 107	0.91 0.92	0.42 0.44	28.6 28.0	29.7 26.1	3.2 1.7	2.8 4.7	—	—	—
1026-1	FWD AFT	174	88	—	—	—	80	76	80	80	92	0.69	0.70	37.9	33.2	6.1	13.8	—	—	—
1026-2	FWD AFT	175	88	—	—	—	80	88 85 93	80	98 92 90	113 104 103	0.65 0.58 0.59	0.70 0.87 0.88	37.9 41.1 43.3	33.2 46.5 50.0	6.1 6.1 6.7	13.8 13.1 13.3	—	—	—
1027-1	FWD AFT	164 163	88	—	—	—	80	89	80	80	80	0.51	0.74	47.3	25.5	4.7	19.3	—	—	—
1028-1	FWD AFT	176	88	—	—	—	80	81	80	89	92	0.82	0.90	47.3	25.2	3.8	19.3	—	—	—
1028-2	FWD AFT	177	88	—	—	—	80	82 88 77	80	95 87 84	95 87 84	0.82 0.78 0.78	0.90 0.90 0.90	36.6 36.6 42.5	28.0 28.0 25.6	3.9 3.1 3.2	4.8 4.8 4.2	—	—	—

# EXPOSURE - PROCESSING SUMMARY

WILSON NUMBER	CAMERA	SOLAR ELEVATION RANGE (°)		SOLAR AZIMUTH RANGE (°)		PREDICTED PROCESSING			REPORTED PROCESSING			COMPUTED PROCESSING			TERRAIN D. MIN.			TERRAIN D. MAX.			CLOUD D. MAX.			UNDER EXPOSED (%)	OVER PROCESSED (%)	NOMINAL EXP. & PRO	OVER EXPOSED (%)	CLOUD COVER (%)
		LOW	HIGH	LOW	HIGH	P	F	T	P	F	T	P	F	T	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN					
1004-1	PWO	-3	61	88	124	5	76	19	4	79	17	0	78	21	0	28	189	0.83	0.78	0.81	0.43	2.43	2.04	2.08	0	31	80	38
1004-2	AFT	-3	81	28	124	6	74	21	4	79	17	0	80	20	0	22	156	0.78	0.70	0.83	0.93	2.43	1.98	2.03	0	26	87	38
1004-3	PWO	-4	68	10	131	7	76	17	37	90	13	4	77	19	4	29	180	0.83	0.78	0.83	0.36	2.50	1.87	1.93	0	27	59	38
1004-4	AFT	-4	68	10	131	7	76	17	37	90	13	4	77	19	4	29	180	0.83	0.78	0.83	0.36	2.50	1.87	1.93	0	20	87	38
1005-1	PWO	36	88	32	140	1	99	0	1	99	0	51	49	0	51	49	0.88	0.80	0.71	0.80	2.40	2.20	2.24	0	21	72	60	60
1005-2	AFT	32	84	36	147	2	98	0	30	41	29	11	59	30	0	21	114	0.53	0.50	0.50	0.36	2.33	2.11	2.16	2	4	56	48
1007-1	PWO	12	49	90	103	0	95	1	20	79	0	25	77	0	25	77	0.47	0.47	0.47	0.62	2.17	2.21	2.21	20	3	67	60	60
1007-2	AFT	32	87	43	112	0	98	0	10	42	48	6	77	17	0	26	176	0.58	0.55	0.55	0.78	2.31	2.20	2.24	1	13	80	60
1008-1	PWO	30	81	90	102	0	100	0	4	27	69	0	34	66	0	26	132	0.71	0.69	0.71	0.52	2.39	2.20	2.24	1	1	84	48
1008-2	AFT	29	86	42	105	0	100	0	3	31	66	0	27	73	0	27	154	0.78	0.72	0.81	0.52	2.37	2.20	2.25	2	3	75	68
1009-1	PWO	12	49	42	132	0	100	0	1	26	73	0	34	66	0	26	132	0.65	0.62	0.65	0.73	2.10	2.18	2.22	1	4	77	60
1009-2	AFT	23	88	35	138	2	98	0	4	27	49	0	56	4	0	26	147	0.69	0.64	0.69	0.44	2.31	2.34	2.34	4	4	74	68
1010-1	PWO	18	47	45	83	0	21	79	0	13	87	0	9	91	0	28	114	0.52	0.47	0.52	0.43	2.32	2.20	2.20	16	3	75	60
1010-2	AFT	15	52	36	76	0	50	50	0	16	84	0	13	87	0	26	151	0.55	0.50	0.55	0.78	2.42	2.20	2.26	9	4	81	48
1011-1	PWO	2	59	33	66	0	64	36	2	23	75	2	27	63	0	18	99	0.59	0.56	0.59	0.30	2.40	2.18	2.22	13	3	78	60
1011-2	AFT	2	59	33	66	0	64	36	2	23	75	2	27	63	0	18	99	0.59	0.56	0.59	0.30	2.40	2.18	2.22	13	3	78	60
1012-1	PWO	0	48	36	71	0	64	36	7	56	37	0	65	36	0	25	130	0.59	0.53	0.59	0.34	2.39	1.93	2.00	6	17	68	60
1012-2	AFT	0	48	36	71	0	64	36	7	56	37	0	65	36	0	25	130	0.59	0.53	0.59	0.34	2.39	1.93	2.00	6	17	68	60
1013-1	PWO	0	56	28	83	0	64	36	0	42	58	0	55	45	0	20	127	0.68	0.62	0.68	0.48	2.38	1.98	2.02	4	0	72	60
1013-2	AFT	0	56	28	83	0	64	36	0	42	58	0	55	45	0	20	127	0.68	0.62	0.68	0.48	2.38	1.98	2.02	4	0	72	60
1014-1	PWO	0	59	14	69	0	21	79	0	13	87	0	9	91	0	28	114	0.52	0.47	0.52	0.43	2.32	2.20	2.20	16	3	75	60
1014-2	AFT	0	59	14	69	0	21	79	0	13	87	0	9	91	0	28	114	0.52	0.47	0.52	0.43	2.32	2.20	2.20	16	3	75	60
1015-1	PWO	0	68	19	67	0	8	92	2	2	96	0	2	96	0	2	96	0.34	0.36	0.34	0.34	2.29	1.94	2.05	27	33	39	60
1015-2	AFT	0	68	19	67	0	8	92	2	2	96	0	2	96	0	2	96	0.34	0.36	0.34	0.34	2.29	1.94	2.05	27	33	39	60
1016-1	PWO	5	69	13	76	0	7	93	1	41	58	0	59	41	0	13	153	0.51	0.45	0.51	0.46	2.41	1.90	1.90	19	17	66	60
1016-2	AFT	4	69	12	76	0	8	92	0	28	74	0	42	58	0	22	126	0.64	0.58	0.64	0.46	2.46	1.90	1.92	11	9	82	60
1017-1	PWO	-1	50	21	99	0	100	0	13	87	0	82	18	0	82	18	0.65	0.61	0.65	0.44	2.44	1.91	2.00	1	6	77	60	
1017-2	AFT	-1	50	21	99	0	100	0	13	87	0	82	18	0	82	18	0.65	0.61	0.65	0.44	2.44	1.91	2.00	1	6	77	60	
1018-1	PWO	6	77	13	124	0	100	0	9	93	0	83	16	0	83	16	0.56	0.52	0.56	0.44	2.44	1.91	1.96	2	1	71	60	
1018-2	AFT	6	77	13	124	0	100	0	9	93	0	83	16	0	83	16	0.56	0.52	0.56	0.44	2.44	1.91	1.96	2	1	71	60	
1019-1	PWO	6	77	13	124	0	100	0	9	93	0	83	16	0	83	16	0.56	0.52	0.56	0.44	2.44	1.91	1.96	2	1	71	60	
1019-2	AFT	6	77	13	124	0	100	0	9	93	0	83	16	0	83	16	0.56	0.52	0.56	0.44	2.44	1.91	1.96	2	1	71	60	

TABLE 18-3



~~TOP SECRET~~ [REDACTED]

SECTION A

APPENDIX

~~TOP SECRET~~ [REDACTED]

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
0.01	0	0	0	0	0	0	0	0	0	0	0	0
0.02	0	0	0	0	0	0	0	0	0	0	0	0
0.03	0	0	0	0	0	0	0	0	0	0	0	0
0.04	0	0	0	0	0	0	0	0	0	0	0	0
0.05	0	0	0	0	0	0	0	0	0	0	0	0
0.06	0	0	0	0	0	0	0	0	0	0	0	0
0.07	0	0	0	0	0	0	0	0	0	0	0	0
0.08	0	0	0	0	0	0	0	0	0	0	0	0
0.09	0	0	0	0	0	0	0	0	0	0	0	0
0.10	0	0	0	0	0	0	0	0	0	0	0	0
0.11	0	0	0	0	0	0	0	0	0	0	0	0
0.12	0	0	0	0	0	0	0	0	0	0	0	0
0.13	0	0	0	0	0	0	0	0	0	0	0	0
0.14	0	0	0	0	0	0	0	0	0	0	0	0
0.15	0	0	0	0	0	0	0	0	0	0	0	0
0.16	0	0	0	0	0	0	0	0	0	0	0	0
0.17	0	0	0	0	0	0	0	0	0	0	0	0
0.18	0	0	0	0	0	0	0	0	0	0	0	0
0.19	0	0	0	0	0	0	0	0	0	0	0	0
0.20	0	0	0	0	0	0	0	0	0	0	0	0
0.21	0	0	0	0	0	0	0	0	0	0	0	0
0.22	0	0	0	0	0	0	0	0	0	0	0	0
0.23	0	0	0	0	0	0	0	0	0	0	0	0
0.24	0	0	0	0	0	0	0	0	0	0	0	0
0.25	0	0	0	0	0	0	0	0	0	0	0	0
0.26	0	0	0	0	0	0	0	0	0	0	0	0
0.27	0	0	0	0	0	0	0	0	0	0	0	0
0.28	0	0	0	0	0	0	0	0	0	0	0	0
0.29	0	0	0	0	0	0	0	0	0	0	0	0
0.30	0	0	0	0	0	0	0	0	0	0	0	0
0.31	0	0	0	0	0	0	0	0	0	0	0	0
0.32	0	0	0	0	0	0	0	0	0	0	0	0
0.33	0	0	0	0	0	0	0	0	0	0	0	0
0.34	0	0	0	0	0	0	0	0	0	0	0	0
0.35	0	0	0	0	0	0	0	0	0	0	0	0
0.36	0	0	0	0	0	0	0	0	0	0	0	0
0.37	0	0	0	0	0	0	0	0	0	0	0	0
0.38	0	0	0	0	0	0	0	0	0	0	0	0
0.39	0	0	0	0	0	0	0	0	0	0	0	0
0.40	0	0	0	0	0	0	0	0	0	0	0	0
0.41	0	0	0	0	0	0	0	0	0	0	0	0
0.42	0	0	0	0	0	0	0	0	0	0	0	0
0.43	0	0	0	0	0	0	0	0	0	0	0	0
0.44	0	0	0	0	0	0	0	0	0	0	0	0
0.45	0	0	0	0	0	0	0	0	0	0	0	0
0.46	0	0	0	0	0	0	0	0	0	0	0	0
0.47	0	0	0	0	0	0	0	0	0	0	0	0
0.48	0	0	0	0	0	0	0	0	0	0	0	0
0.49	0	0	0	0	0	0	0	0	0	0	0	0
0.50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	2	0	0	2	0	2	2	0	0

~~TOP SECRET~~

TABLE A-1

DENSITY VALUE	PRIMARY		INTERMEDIATE			FULL			ALL LEVELS			
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0.51				1	0	0	3	0	0	4	0	0
0.52				0	0	0	1	0	0	1	0	0
0.53				0	0	0	3	0	0	2	0	0
0.54				0	0	0	2	0	0	1	0	0
0.55				0	0	0	0	0	0	0	0	0
0.56				0	0	0	0	0	0	0	0	0
0.57				0	0	0	0	0	0	0	0	0
0.58				0	0	0	0	0	0	0	0	0
0.59				0	0	0	0	0	0	0	0	0
0.60				0	0	0	0	0	0	0	0	0
0.61				0	0	0	0	0	0	0	0	0
0.62				0	0	0	0	0	0	0	0	0
0.63				0	0	0	0	0	0	0	0	0
0.64				0	0	0	0	0	0	0	0	0
0.65				0	0	0	0	0	0	0	0	0
0.66				0	0	0	0	0	0	0	0	0
0.67				0	0	0	0	0	0	0	0	0
0.68				0	0	0	0	0	0	0	0	0
0.69				0	0	0	0	0	0	0	0	0
0.70				0	0	0	0	0	0	0	0	0
0.71				0	0	0	3	0	0	3	0	0
0.72				0	0	0	0	0	0	0	0	0
0.73				0	0	0	0	0	0	0	0	0
0.74				0	0	0	0	0	0	0	0	0
0.75				0	0	0	0	0	0	0	0	0
0.76				0	0	0	0	0	0	0	0	0
0.77				0	0	0	0	0	0	0	0	0
0.78				0	0	0	0	0	0	0	0	0
0.79				0	0	0	0	0	0	0	0	0
0.80				0	0	0	0	0	0	0	0	0
0.81				0	0	0	0	0	0	0	0	0
0.82				0	0	0	0	0	0	0	0	0
0.83				0	0	0	0	0	0	0	0	0
0.84				0	0	0	0	0	0	0	0	0
0.85				0	0	0	0	0	0	0	0	0
0.86				0	0	0	0	0	0	0	0	0
0.87				0	0	0	0	0	0	0	0	0
0.88				0	0	0	0	0	0	0	0	0
0.89				0	0	0	0	0	0	0	0	0
0.90				0	0	0	0	0	0	0	0	0
0.91				0	0	0	0	0	0	0	0	0
0.92				0	0	0	0	0	0	0	0	0
0.93				0	0	0	0	0	0	0	0	0
0.94				0	0	0	0	0	0	0	0	0
0.95				0	0	0	0	0	0	0	0	0
0.96				0	0	0	0	0	0	0	0	0
0.97				0	0	0	0	0	0	0	0	0
0.98				0	0	0	0	0	0	0	0	0
0.99				0	0	0	0	0	0	0	0	0
1.00				0	0	0	0	0	0	0	0	0
SUBTOTAL				0	0	0	26	4	7	3	4	3

TABLE A-1

DENSITY VALUE	PRIMARY			INTERMEDIATE			ALL LEVELS					
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM			
1.01	0	0	0	0	0	1	0	0	0	0	0	1
1.02	0	0	0	0	0	1	0	0	0	0	0	1
1.03	0	0	0	0	0	1	0	0	0	0	0	1
1.04	0	0	0	0	0	1	0	0	0	0	0	1
1.05	0	0	0	0	0	1	0	0	0	0	0	1
1.06	0	0	0	0	0	1	0	0	0	0	0	1
1.07	0	0	0	0	0	1	0	0	0	0	0	1
1.08	0	0	0	0	0	1	0	0	0	0	0	1
1.09	0	0	0	0	0	1	0	0	0	0	0	1
1.10	0	0	0	0	0	1	0	0	0	0	0	1
1.11	0	0	0	0	0	1	0	0	0	0	0	1
1.12	0	0	0	0	0	1	0	0	0	0	0	1
1.13	0	0	0	0	0	1	0	0	0	0	0	1
1.14	0	0	0	0	0	1	0	0	0	0	0	1
1.15	0	0	0	0	0	1	0	0	0	0	0	1
1.16	0	0	0	0	0	1	0	0	0	0	0	1
1.17	0	0	0	0	0	1	0	0	0	0	0	1
1.18	0	0	0	0	0	1	0	0	0	0	0	1
1.19	0	0	0	0	0	1	0	0	0	0	0	1
1.20	0	0	0	0	0	1	0	0	0	0	0	1
1.21	0	0	0	0	0	1	0	0	0	0	0	1
1.22	0	0	0	0	0	1	0	0	0	0	0	1
1.23	0	0	0	0	0	1	0	0	0	0	0	1
1.24	0	0	0	0	0	1	0	0	0	0	0	1
1.25	0	0	0	0	0	1	0	0	0	0	0	1
1.26	0	0	0	0	0	1	0	0	0	0	0	1
1.27	0	0	0	0	0	1	0	0	0	0	0	1
1.28	0	0	0	0	0	1	0	0	0	0	0	1
1.29	0	0	0	0	0	1	0	0	0	0	0	1
1.30	0	0	0	0	0	1	0	0	0	0	0	1
1.31	0	0	0	0	0	1	0	0	0	0	0	1
1.32	0	0	0	0	0	1	0	0	0	0	0	1
1.33	0	0	0	0	0	1	0	0	0	0	0	1
1.34	0	0	0	0	0	1	0	0	0	0	0	1
1.35	0	0	0	0	0	1	0	0	0	0	0	1
1.36	0	0	0	0	0	1	0	0	0	0	0	1
1.37	0	0	0	0	0	1	0	0	0	0	0	1
1.38	0	0	0	0	0	1	0	0	0	0	0	1
1.39	0	0	0	0	0	1	0	0	0	0	0	1
1.40	0	0	0	0	0	1	0	0	0	0	0	1
1.41	0	0	0	0	0	1	0	0	0	0	0	1
1.42	0	0	0	0	0	1	0	0	0	0	0	1
1.43	0	0	0	0	0	1	0	0	0	0	0	1
1.44	0	0	0	0	0	1	0	0	0	0	0	1
1.45	0	0	0	0	0	1	0	0	0	0	0	1
1.46	0	0	0	0	0	1	0	0	0	0	0	1
1.47	0	0	0	0	0	1	0	0	0	0	0	1
1.48	0	0	0	0	0	1	0	0	0	0	0	1
1.49	0	0	0	0	0	1	0	0	0	0	0	1
1.50	0	0	0	0	0	1	0	0	0	0	0	1
SUBTOTAL						15						8

~~TOP SECRET~~

TABLE A-1



DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.51	0	0	0	0	0	0	0	0	0	0	0	0
1.52	0	0	0	0	0	0	0	0	0	0	0	0
1.53	0	0	0	0	0	0	0	0	0	0	0	0
1.54	0	0	0	0	0	0	0	0	0	0	0	0
1.55	0	0	0	0	0	0	0	0	0	0	0	0
1.56	0	0	0	0	0	0	0	0	0	0	0	0
1.57	0	0	0	0	0	0	0	0	0	0	0	0
1.58	0	0	0	0	0	0	0	0	0	0	0	0
1.59	0	0	0	0	0	0	0	0	0	0	0	0
1.60	0	0	0	0	0	0	0	0	0	0	0	0
1.61	0	0	0	0	0	0	0	0	0	0	0	0
1.62	0	0	0	0	0	0	0	0	0	0	0	0
1.63	0	0	0	0	0	0	0	0	0	0	0	0
1.64	0	0	0	0	0	0	0	0	0	0	0	0
1.65	0	0	0	0	0	0	0	0	0	0	0	0
1.66	0	0	0	0	0	0	0	0	0	0	0	0
1.67	0	0	0	0	0	0	0	0	0	0	0	0
1.68	0	0	0	0	0	0	0	0	0	0	0	0
1.69	0	0	0	0	0	0	0	0	0	0	0	0
1.70	0	0	0	0	0	0	0	0	0	0	0	0
1.71	0	0	0	0	0	0	0	0	0	0	0	0
1.72	0	0	0	0	0	0	0	0	0	0	0	0
1.73	0	0	0	0	0	0	0	0	0	0	0	0
1.74	0	0	0	0	0	0	0	0	0	0	0	0
1.75	0	0	0	0	0	0	0	0	0	0	0	0
1.76	0	0	0	0	0	0	0	0	0	0	0	0
1.77	0	0	0	0	0	0	0	0	0	0	0	0
1.78	0	0	0	0	0	0	0	0	0	0	0	0
1.79	0	0	0	0	0	0	0	0	0	0	0	0
1.80	0	0	0	0	0	0	0	0	0	0	0	0
1.81	0	0	0	0	0	0	0	0	0	0	0	0
1.82	0	0	0	0	0	0	0	0	0	0	0	0
1.83	0	0	0	0	0	0	0	0	0	0	0	0
1.84	0	0	0	0	0	0	0	0	0	0	0	0
1.85	0	0	0	0	0	0	0	0	0	0	0	0
1.86	0	0	0	0	0	0	0	0	0	0	0	0
1.87	0	0	0	0	0	0	0	0	0	0	0	0
1.88	0	0	0	0	0	0	0	0	0	0	0	0
1.89	0	0	0	0	0	0	0	0	0	0	0	0
1.90	0	0	0	0	0	0	0	0	0	0	0	0
1.91	0	0	0	0	0	0	0	0	0	0	0	0
1.92	0	0	0	0	0	0	0	0	0	0	0	0
1.93	0	0	0	0	0	0	0	0	0	0	0	0
1.94	0	0	0	0	0	0	0	0	0	0	0	0
1.95	0	0	0	0	0	0	0	0	0	0	0	0
1.96	0	0	0	0	0	0	0	0	0	0	0	0
1.97	0	0	0	0	0	0	0	0	0	0	0	0
1.98	0	0	0	0	0	0	0	0	0	0	0	0
1.99	0	0	0	0	0	0	0	0	0	0	0	0
2.00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL					17	10		80	81	0	97	91

TABLE A-1

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.01												
2.02												
2.03												
2.04												
2.05												
2.06												
2.07												
2.08												
2.09												
2.10												
2.11												
2.12												
2.13												
2.14												
2.15												
2.16												
2.17												
2.18												
2.19												
2.20												
2.21												
2.22												
2.23												
2.24												
2.25												
2.26												
2.27												
2.28												
2.29												
2.30												
2.31												
2.32												
2.33												
2.34												
2.35												
2.36												
2.37												
2.38												
2.39												
2.40												
2.41												
2.42												
2.43												
2.44												
2.45												
2.46												
2.47												
2.48												
2.49												
2.50												
SUBTOTAL												

TOP SECRET

TABLE A-1

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	29	29	19	229	229	154	258	258	173

MISSION 1028-1 INSTR - FRWD 2-11-66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	29	0 PC	55 PC	38 PC	7 PC	0 PC
FULL	229	73 PC	0 PC	27 PC	0 PC	0 PC
ALL LEVELS	258	65 PC	6 PC	28 PC	1 PC	0 PC

PROCESS LEVEL	BASE + FCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

TABLE A-1

MISSION • 1728-1 • INSTR • FR40 • 2-11-66 PLUT OF 0 MI 1 • TERRAIN • PROCESSING • INTERMEDIATE  
 WITH BEAM • 0.42 • FLIPAV • 0.34 • STD DEV • 0.22 • RANGE • 0.23 TO 1.08 WITH 29 SAMPLES

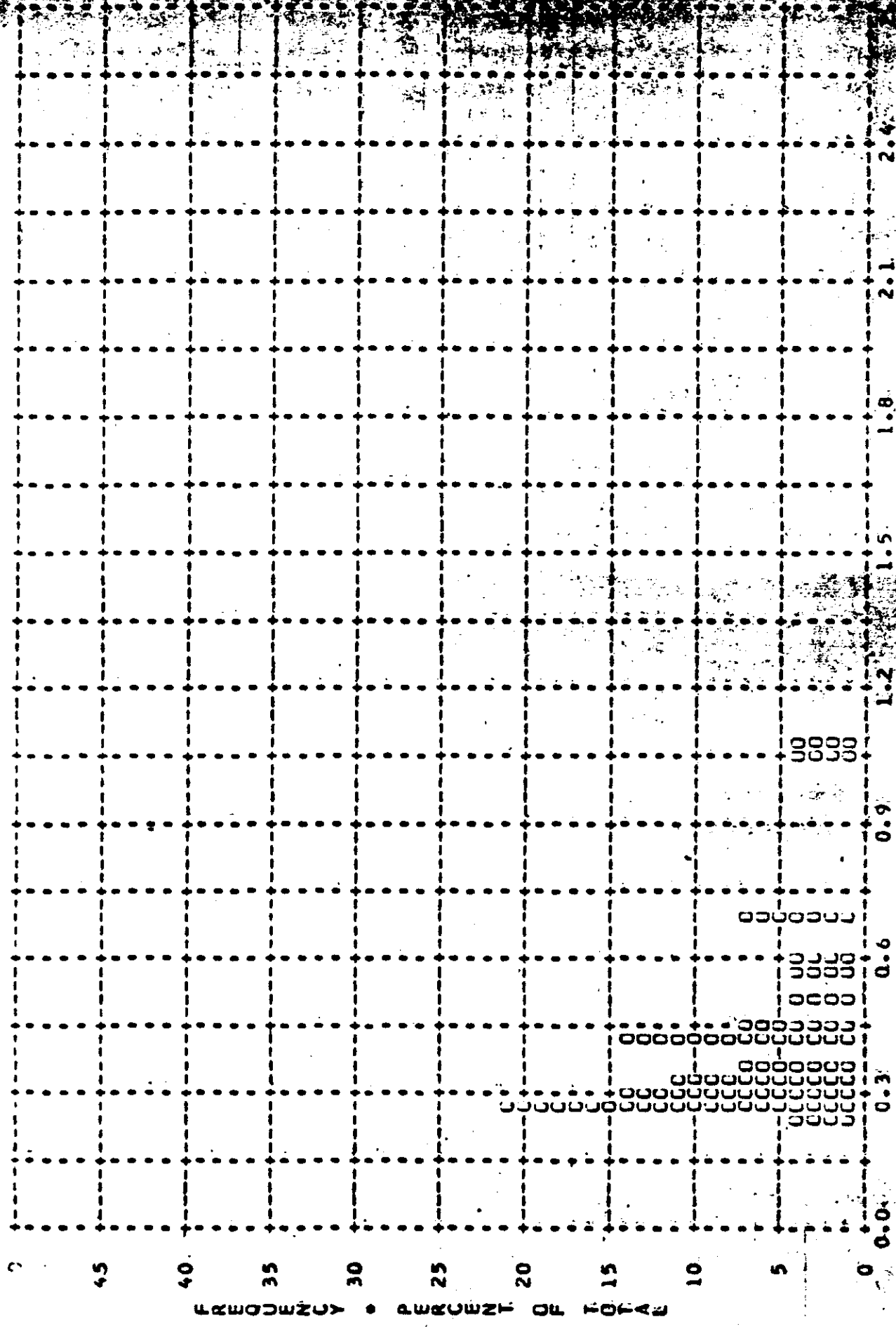
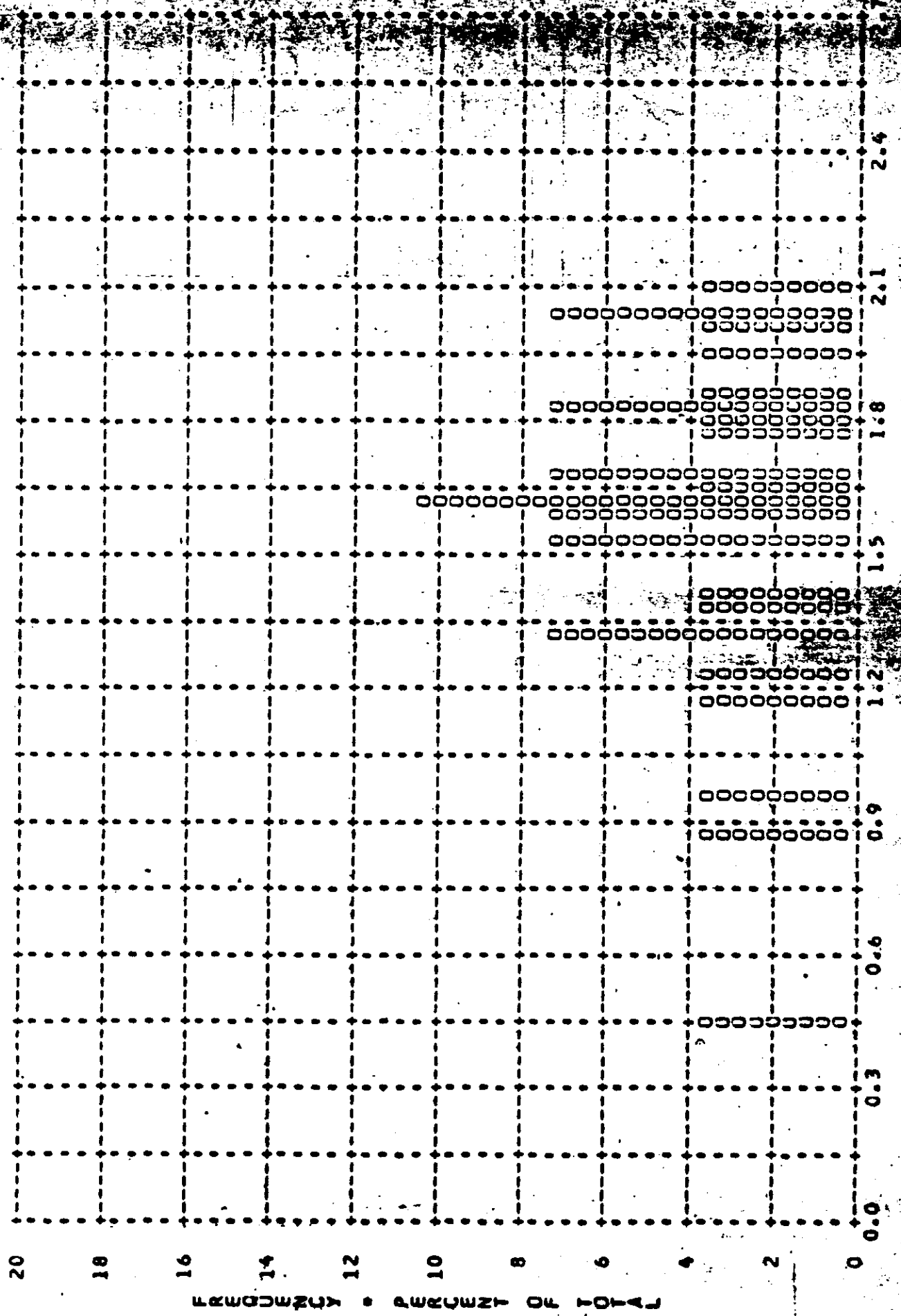


FIGURE A-1

TOP SECRET

~~TOP SECRET~~

MISSION - 1028-1 • INSTR • FRWD • 2-11-66 PLUT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE  
ARITH MEAN • 1.56 • MEDIAN • 1.61 • STD DEV • 0.38 • RANGE • 0.44 TO 2.10 WITH 29 SAMPLES



~~TOP SECRET~~

FIGURE A-2

MISSION • 1028-1 • INSTR • FRWD • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE  
 ARITH MEAN • 1.76 • MEDIAN • 1.91 • STD DEV • C.37 • RANGE • 1.01 TO 2.18 WITH 19 SAMPLES

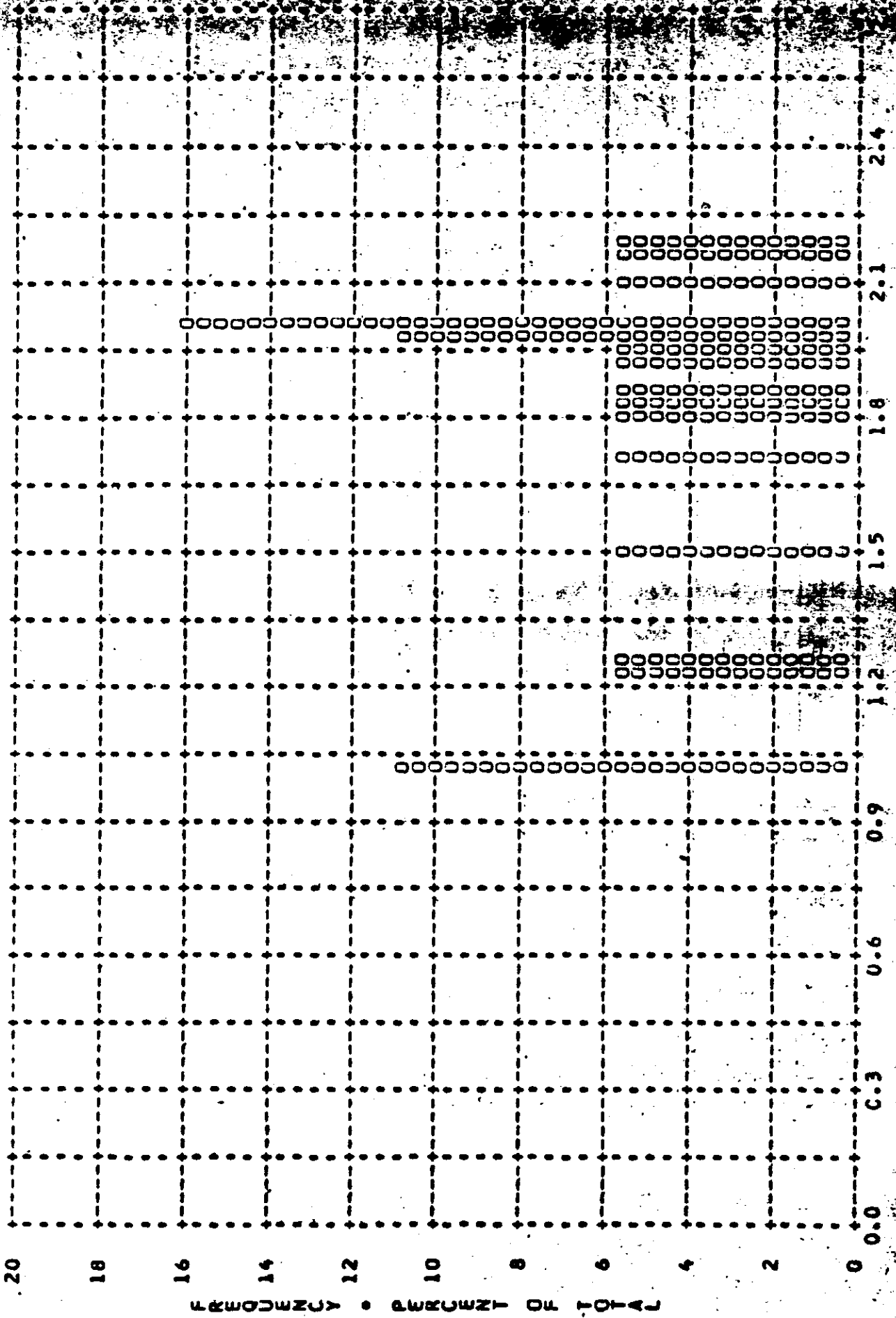
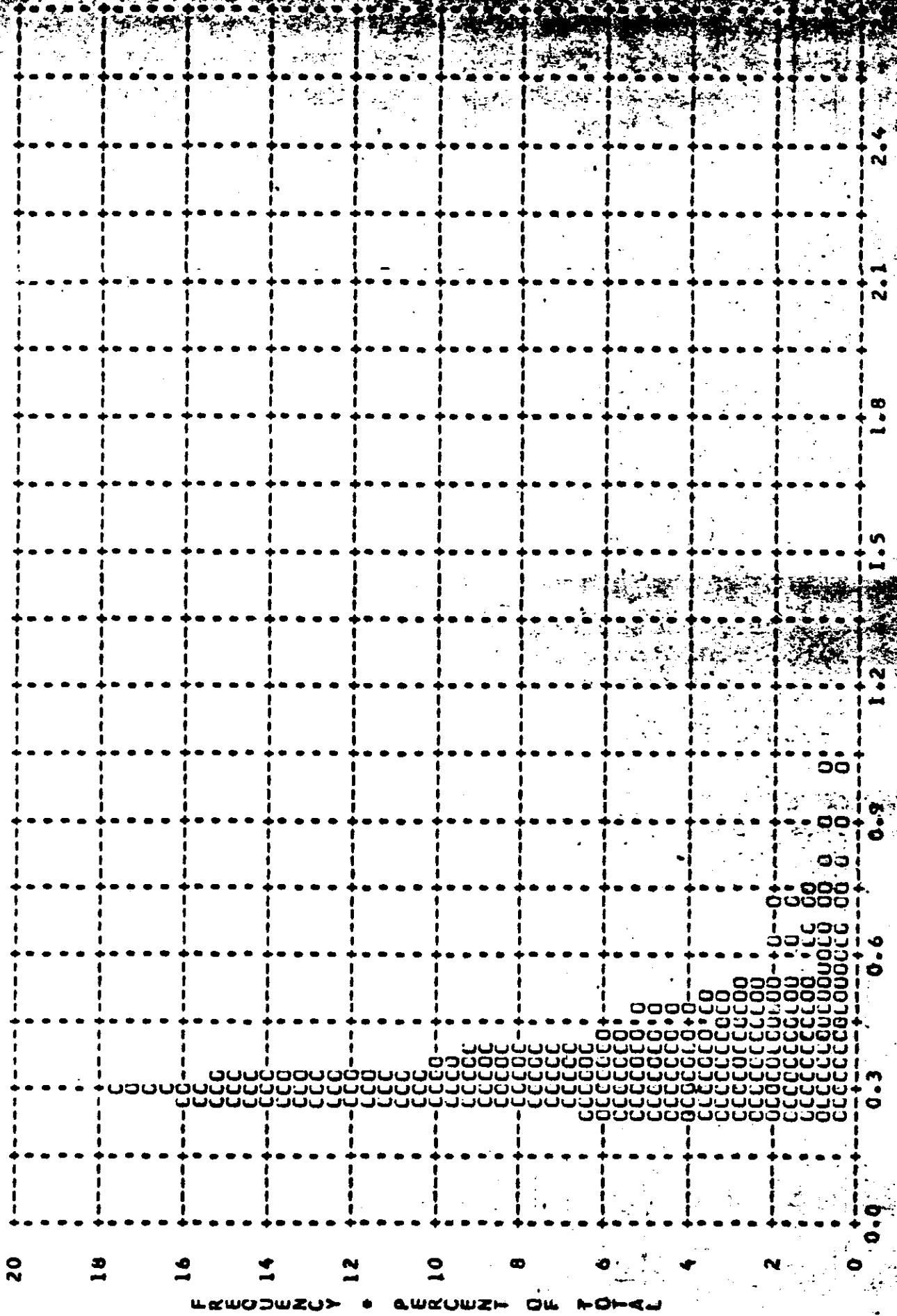


FIGURE A-3

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • FRWD • 2-11-66 PLOT OF 0 MIN • TERRAIN • PRG • ING • FULL  
ARITH MEAN • 0.37 • MEDIAN • 0.32 • STD DEV • 0.12 • RANGE • 0.22 TO 1.00 • 229 SAMPLES

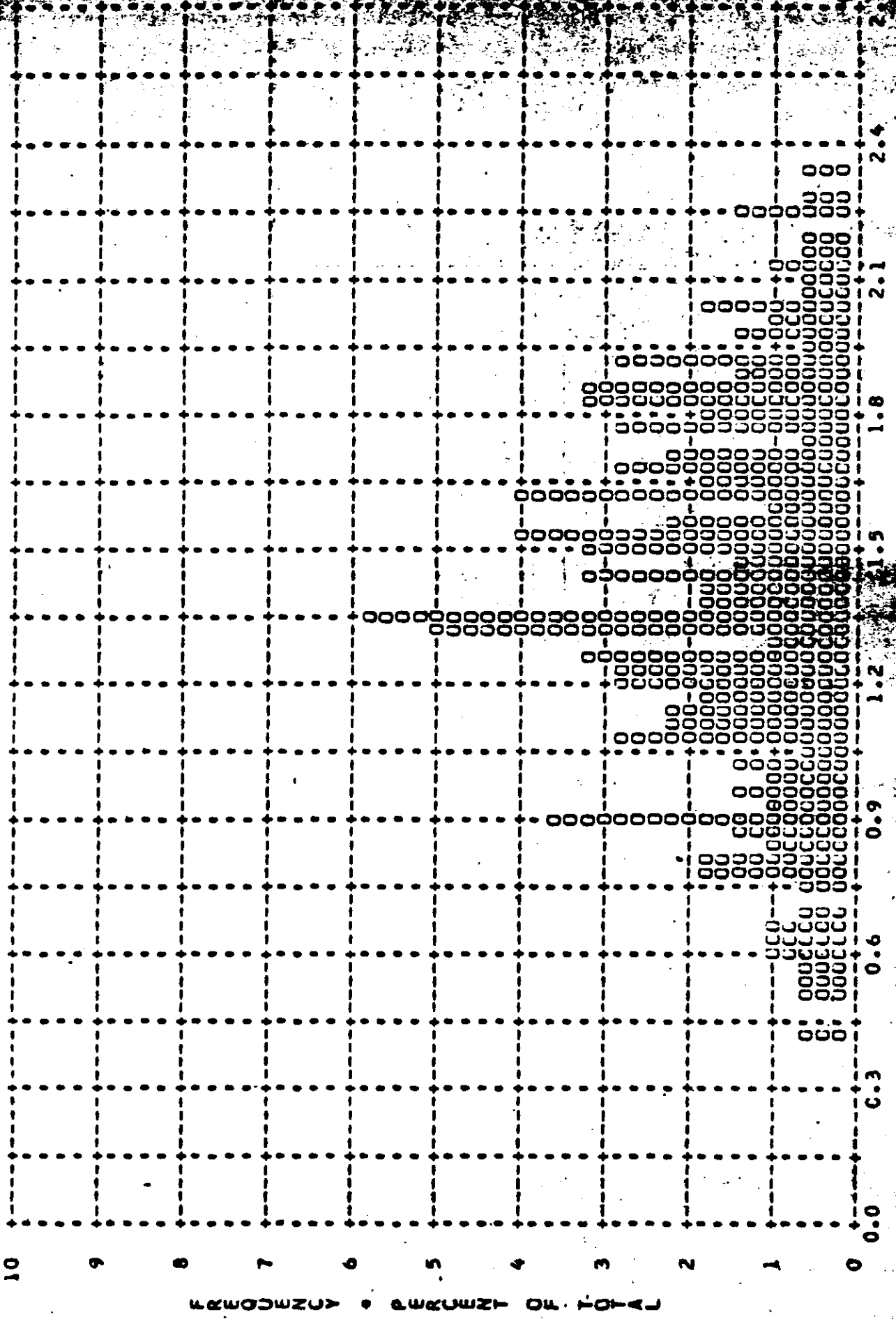


~~TOP SECRET~~

FIGURE A-4

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • FRWD • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • FULL  
ARITH MEAN • 1.40 • MEDIAN • 1.39 • STD DEV • 0.41 • RANGE • 0.40 TO 2.32 WITH 229 SAMPLES



~~TOP SECRET~~

FIGURE A-5



MISSION • 1028-1 • INSTR • FRWD • 2-11-66 PLGT OF D MAX • CLOUD • PROCESSING • FULL  
 ARITH MEAN • 1.77 • MEDIAN • 1.82 • STD DEV • 0.34 • RANGE • 0.62 TO 2.30 WITH 154 SAMPLES

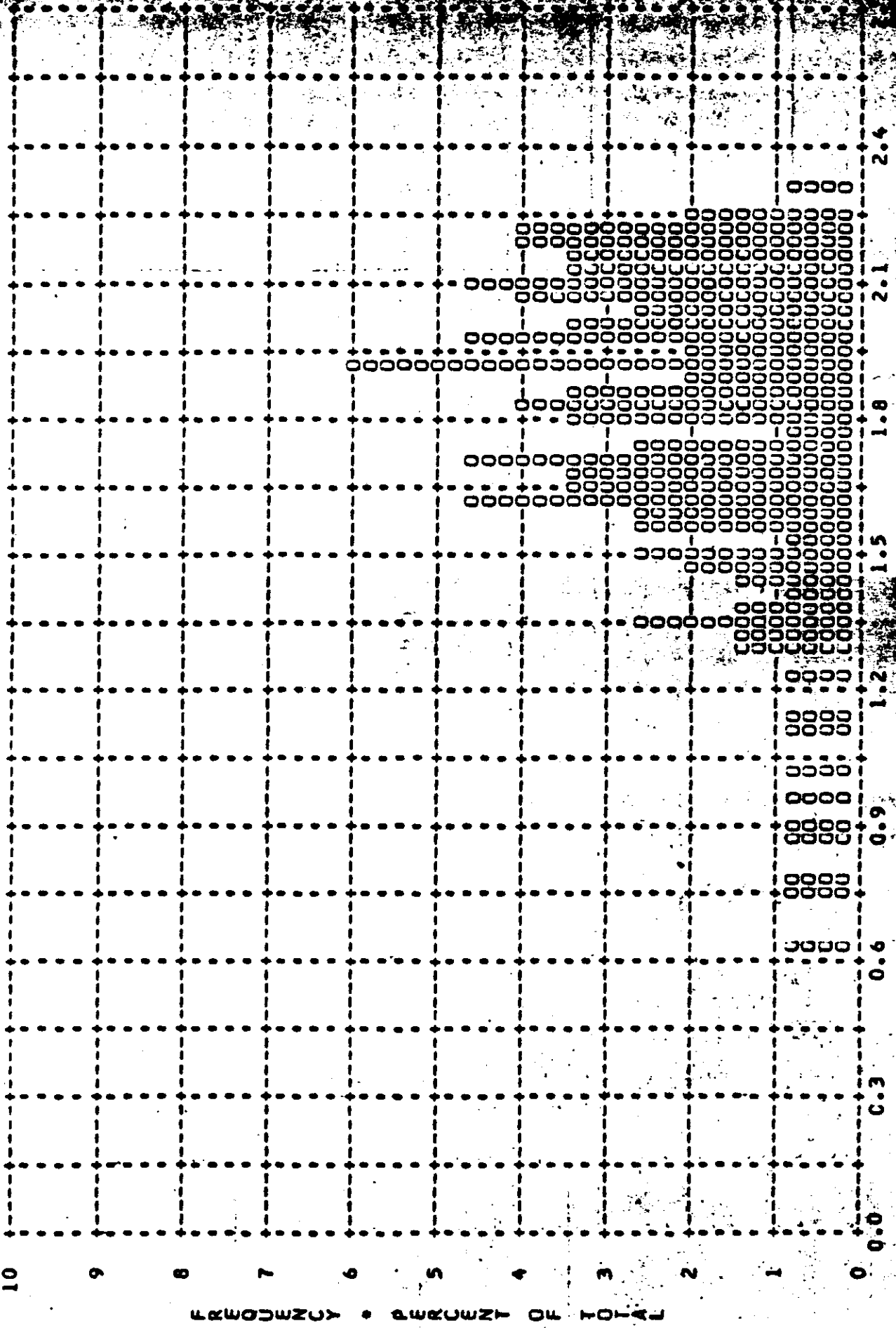
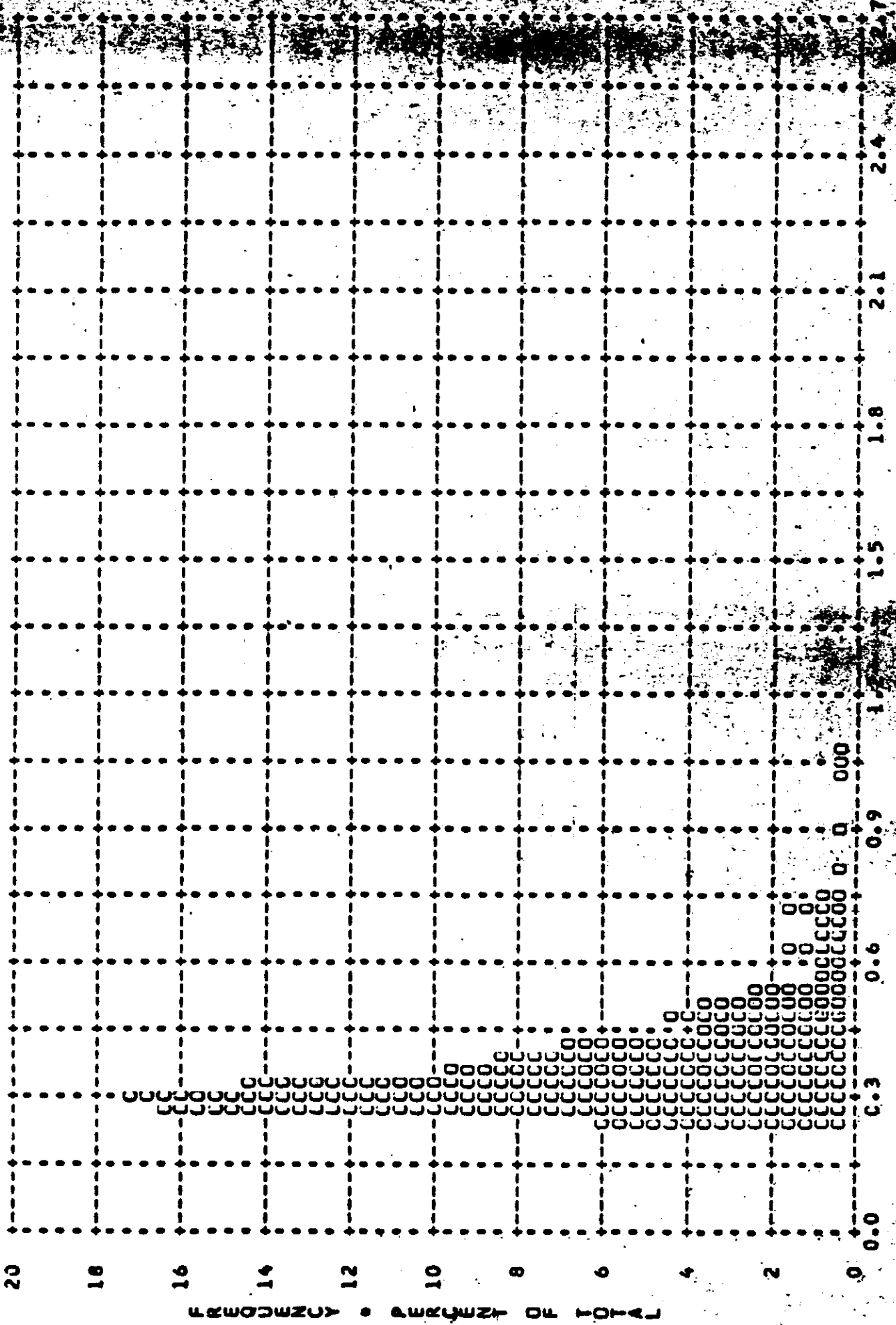


FIGURE A-6

TOP SECRET

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • FRWD • 2-11-66 PLOT OF U MIN • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • C.37 • MEDIAN • C.14 • STD DEV • 0.22 TO 1.08 WITH 258 SAMPLES



• DENSITY •

~~TOP SECRET~~

FIGURE A-7

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • FRWD • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.42 • MEDIAN • 1.42 • STD DEV • 0.40 • RANGE • 0.40 TO 2.32 WITH 258 SAMPLES

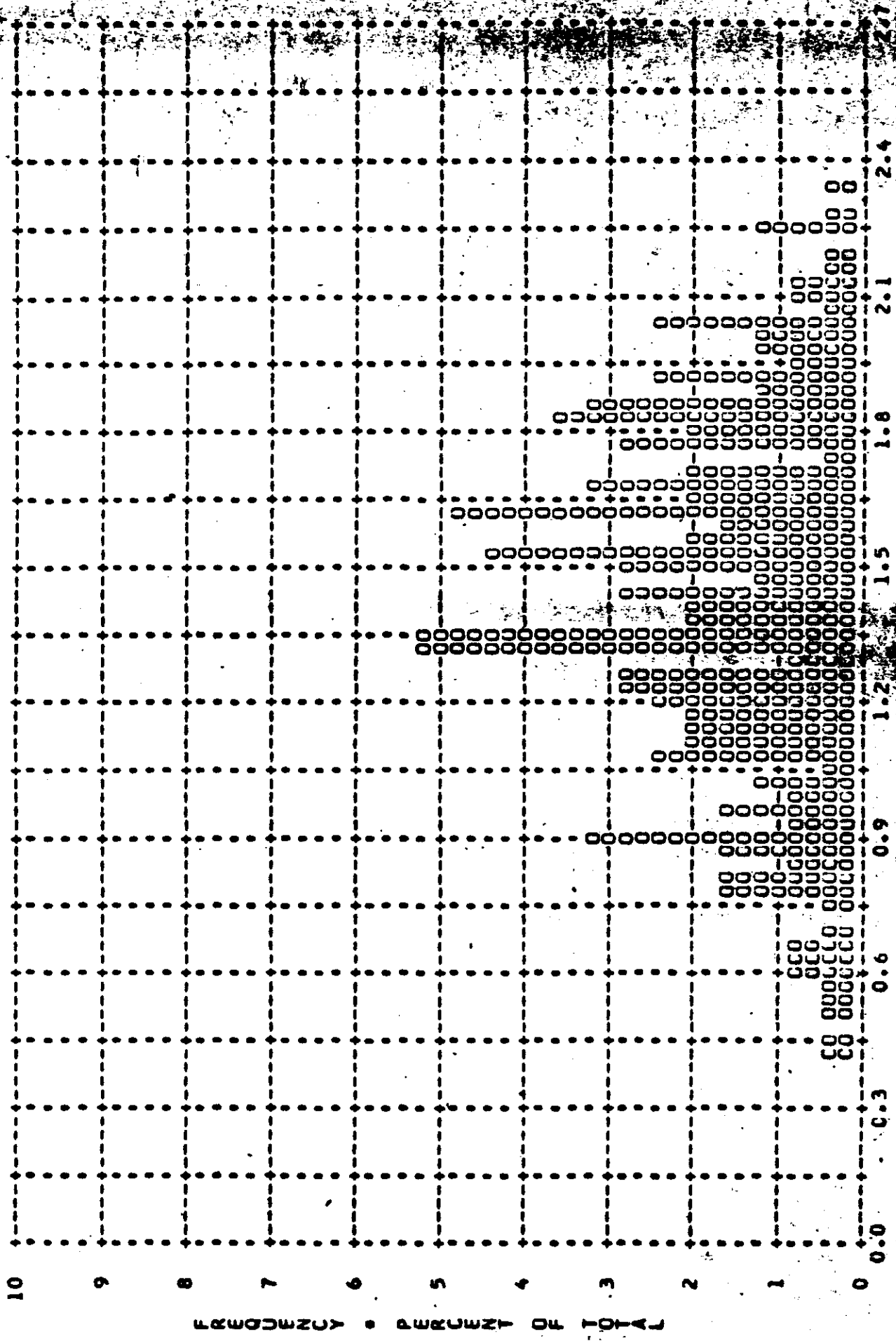
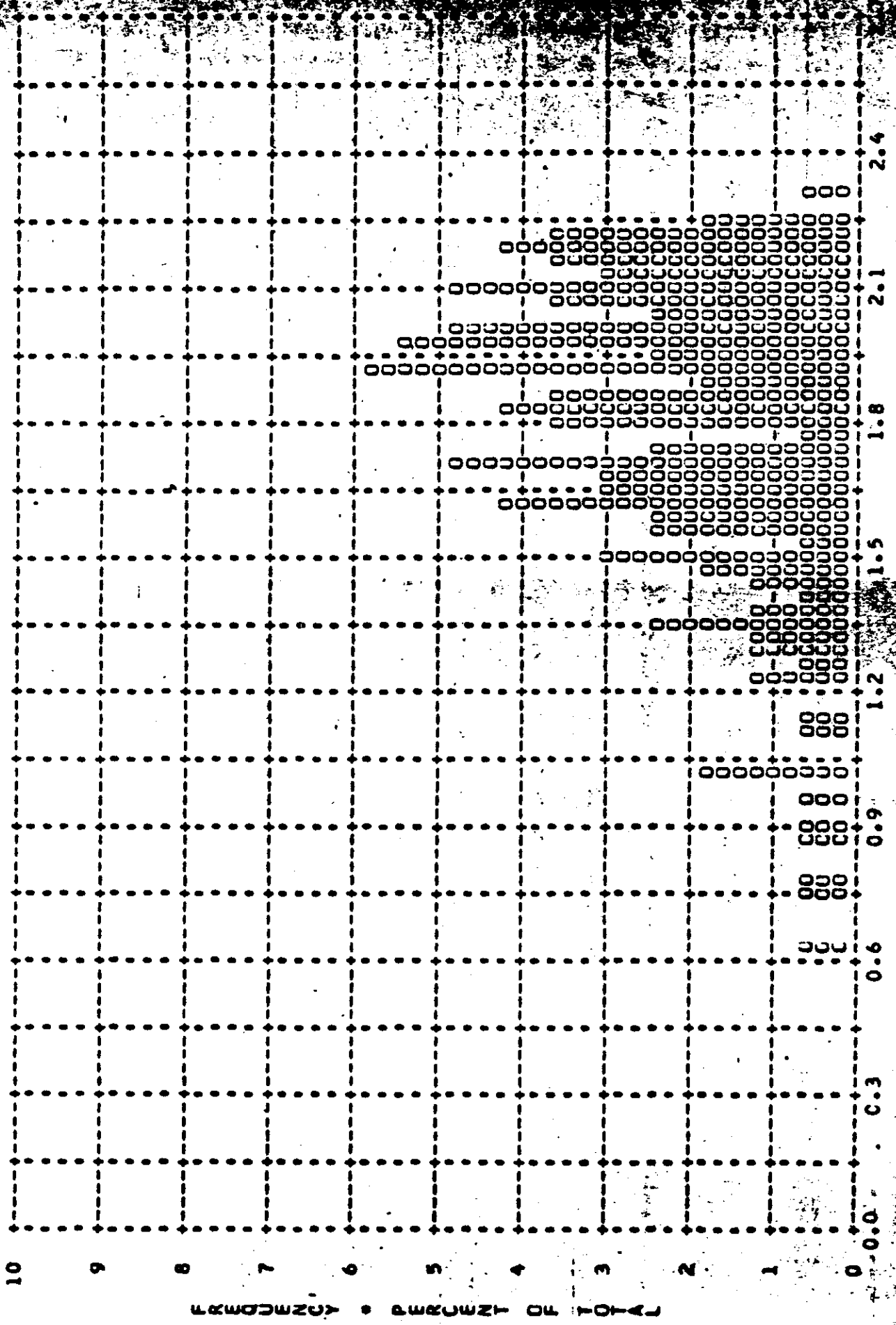


FIGURE A-8

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • FRWD • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.77 • MEDIAN • 1.83 • STD DEV • 0.34 • RANGE • 0.62 TO 2.30 WITH 173 SAMPLES



~~TOP SECRET~~

FIGURE A-9

DENSITY VALUE	PRIMARY		INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0.01	0	0	0	0	0	0	0	0	0	0	0
0.02	0	0	0	0	0	0	0	0	0	0	0
0.03	0	0	0	0	0	0	0	0	0	0	0
0.04	0	0	0	0	0	0	0	0	0	0	0
0.05	0	0	0	0	0	0	0	0	0	0	0
0.06	0	0	0	0	0	0	0	0	0	0	0
0.07	0	0	0	0	0	0	0	0	0	0	0
0.08	0	0	0	0	0	0	0	0	0	0	0
0.09	0	0	0	0	0	0	0	0	0	0	0
0.10	0	0	0	0	0	0	0	0	0	0	0
0.11	0	0	0	0	0	0	0	0	0	0	0
0.12	0	0	0	0	0	0	0	0	0	0	0
0.13	0	0	0	0	0	0	0	0	0	0	0
0.14	0	0	0	0	0	0	0	0	0	0	0
0.15	0	0	0	0	0	0	0	0	0	0	0
0.16	0	0	0	0	0	0	0	0	0	0	0
0.17	0	0	0	0	0	0	0	0	0	0	0
0.18	0	0	0	0	0	0	0	0	0	0	0
0.19	0	0	0	0	0	0	0	0	0	0	0
0.20	0	0	0	0	0	0	0	0	0	0	0
0.21	0	0	0	0	0	0	0	0	0	0	0
0.22	0	0	0	0	0	0	0	0	0	0	0
0.23	0	0	0	0	0	0	0	0	0	0	0
0.24	0	0	0	0	0	0	0	0	0	0	0
0.25	0	0	0	0	0	0	0	0	0	0	0
0.27	0	0	0	0	0	0	0	0	0	0	0
0.28	0	0	0	0	0	0	0	0	0	0	0
0.29	0	0	0	0	0	0	0	0	0	0	0
0.30	0	0	0	0	0	0	0	0	0	0	0
0.31	0	0	0	0	0	0	0	0	0	0	0
0.32	0	0	0	0	0	0	0	0	0	0	0
0.33	0	0	0	0	0	0	0	0	0	0	0
0.34	0	0	0	0	0	0	0	0	0	0	0
0.35	0	0	0	0	0	0	0	0	0	0	0
0.36	0	0	0	0	0	0	0	0	0	0	0
0.37	0	0	0	0	0	0	0	0	0	0	0
0.38	0	0	0	0	0	0	0	0	0	0	0
0.39	0	0	0	0	0	0	0	0	0	0	0
0.40	0	0	0	0	0	0	0	0	0	0	0
0.41	0	0	0	0	0	0	0	0	0	0	0
0.42	0	0	0	0	0	0	0	0	0	0	0
0.43	0	0	0	0	0	0	0	0	0	0	0
0.44	0	0	0	0	0	0	0	0	0	0	0
0.45	0	0	0	0	0	0	0	0	0	0	0
0.46	0	0	0	0	0	0	0	0	0	0	0
0.47	0	0	0	0	0	0	0	0	0	0	0
0.48	0	0	0	0	0	0	0	0	0	0	0
0.49	0	0	0	0	0	0	0	0	0	0	0
0.50	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL						196			218		

TABLE A-2

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0.51												
0.52												
0.53												
0.54												
0.55												
0.56												
0.57												
0.58												
0.59												
0.60												
0.61												
0.62												
0.63												
0.64												
0.65												
0.66												
0.67												
0.68												
0.69												
0.70												
0.71												
0.72												
0.73												
0.74												
0.75												
0.76												
0.77												
0.78												
0.79												
0.80												
0.81												
0.82												
0.83												
0.84												
0.85												
0.86												
0.87												
0.88												
0.89												
0.90												
0.91												
0.92												
0.93												
0.94												
0.95												
0.96												
0.97												
0.98												
0.99												
1.00												
SUBTOTAL												

TABLE A-2

DENSITY VALUE	PRIMARY			INTERMEDIATE			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.01									
1.02									
1.03									
1.04									
1.05									
1.06									
1.07									
1.08									
1.09									
1.10									
1.11									
1.12									
1.13									
1.14									
1.15									
1.16									
1.17									
1.18									
1.19									
1.20									
1.21									
1.22									
1.23									
1.24									
1.25									
1.26									
1.27									
1.28									
1.29									
1.30									
1.31									
1.32									
1.33									
1.34									
1.35									
1.36									
1.37									
1.38									
1.39									
1.40									
1.41									
1.42									
1.43									
1.44									
1.45									
1.46									
1.47									
1.48									
1.49									
1.50									
SUBTOTAL									

~~TOP SECRET~~

TABLE A-2

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS					
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM			
1.51			0			0			0			0			
1.52			0			0			0			0			
1.53			0			0			0			0			
1.54			0			0			0			0			
1.55			0			0			0			0			
1.56			0			0			0			0			
1.57			0			0			0			0			
1.58			0			0			0			0			
1.59			0			0			0			0			
1.60			0			0			0			0			
1.61			0			0			0			0			
1.62			0			0			0			0			
1.63			0			0			0			0			
1.64			0			0			0			0			
1.65			0			0			0			0			
1.66			0			0			0			0			
1.67			0			0			0			0			
1.68			0			0			0			0			
1.69			0			0			0			0			
1.70			0			0			0			0			
1.71			0			0			0			0			
1.72			0			0			0			0			
1.73			0			0			0			0			
1.74			0			0			0			0			
1.75			0			0			0			0			
1.76			0			0			0			0			
1.77			0			0			0			0			
1.78			0			0			0			0			
1.79			0			0			0			0			
1.80			0			0			0			0			
1.81			0			0			0			0			
1.82			0			0			0			0			
1.83			0			0			0			0			
1.84			0			0			0			0			
1.85			0			0			0			0			
1.86			0			0			0			0			
1.87			0			0			0			0			
1.88			0			0			0			0			
1.89			0			0			0			0			
1.90			0			0			0			0			
1.91			0			0			0			0			
1.92			0			0			0			0			
1.93			0			0			0			0			
1.94			0			0			0			0			
1.95			0			0			0			0			
1.96			0			0			0			0			
1.97			0			0			0			0			
1.98			0			0			0			0			
1.99			0			0			0			0			
2.00			0			0			0			0			
SUBTOTAL			0			0			0			0			0

~~TOP SECRET~~

TABLE A-2



~~TOP SECRET~~

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
0.01	0	0	0	0	0	0	0	0	0	0	0	0
0.02	0	0	0	0	0	0	0	0	0	0	0	0
0.03	0	0	0	0	0	0	0	0	0	0	0	0
0.04	0	0	0	0	0	0	0	0	0	0	0	0
0.05	0	0	0	0	0	0	0	0	0	0	0	0
0.06	0	0	0	0	0	0	0	0	0	0	0	0
0.07	0	0	0	0	0	0	0	0	0	0	0	0
0.08	0	0	0	0	0	0	0	0	0	0	0	0
0.09	0	0	0	0	0	0	0	0	0	0	0	0
0.10	0	0	0	0	0	0	0	0	0	0	0	0
0.11	0	0	0	0	0	0	0	0	0	0	0	0
0.12	0	0	0	0	0	0	0	0	0	0	0	0
0.13	0	0	0	0	0	0	0	0	0	0	0	0
0.14	0	0	0	0	0	0	0	0	0	0	0	0
0.15	0	0	0	0	0	0	0	0	0	0	0	0
0.16	0	0	0	0	0	0	0	0	0	0	0	0
0.17	0	0	0	0	0	0	0	0	0	0	0	0
0.18	0	0	0	0	0	0	0	0	0	0	0	0
0.19	0	0	0	0	0	0	0	0	0	0	0	0
0.20	0	0	0	0	0	0	0	0	0	0	0	0
0.21	0	0	0	0	0	0	0	0	0	0	0	0
0.22	0	0	0	0	0	0	0	0	0	0	0	0
0.23	0	0	0	0	0	0	0	0	0	0	0	0
0.24	0	0	0	0	0	0	0	0	0	0	0	0
0.25	0	0	0	0	0	0	0	0	0	0	0	0
0.26	0	0	0	0	0	0	0	0	0	0	0	0
0.27	0	0	0	0	0	0	0	0	0	0	0	0
0.28	0	0	0	0	0	0	0	0	0	0	0	0
0.29	0	0	0	0	0	0	0	0	0	0	0	0
0.30	0	0	0	0	0	0	0	0	0	0	0	0
0.31	0	0	0	0	0	0	0	0	0	0	0	0
0.32	0	0	0	0	0	0	0	0	0	0	0	0
0.33	0	0	0	0	0	0	0	0	0	0	0	0
0.34	0	0	0	0	0	0	0	0	0	0	0	0
0.35	0	0	0	0	0	0	0	0	0	0	0	0
0.36	0	0	0	0	0	0	0	0	0	0	0	0
0.37	0	0	0	0	0	0	0	0	0	0	0	0
0.38	0	0	0	0	0	0	0	0	0	0	0	0
0.39	0	0	0	0	0	0	0	0	0	0	0	0
0.40	0	0	0	0	0	0	0	0	0	0	0	0
0.41	0	0	0	0	0	0	0	0	0	0	0	0
0.42	0	0	0	0	0	0	0	0	0	0	0	0
0.43	0	0	0	0	0	0	0	0	0	0	0	0
0.44	0	0	0	0	0	0	0	0	0	0	0	0
0.45	0	0	0	0	0	0	0	0	0	0	0	0
0.46	0	0	0	0	0	0	0	0	0	0	0	0
0.47	0	0	0	0	0	0	0	0	0	0	0	0
0.48	0	0	0	0	0	0	0	0	0	0	0	0
0.49	0	0	0	0	0	0	0	0	0	0	0	0
0.50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL												

~~TOP SECRET~~

TABLE A-2

MISSION • 1028-1 • INSTRUMENT • AFT • 2-11-66 • DENSITY FREQ DISTR

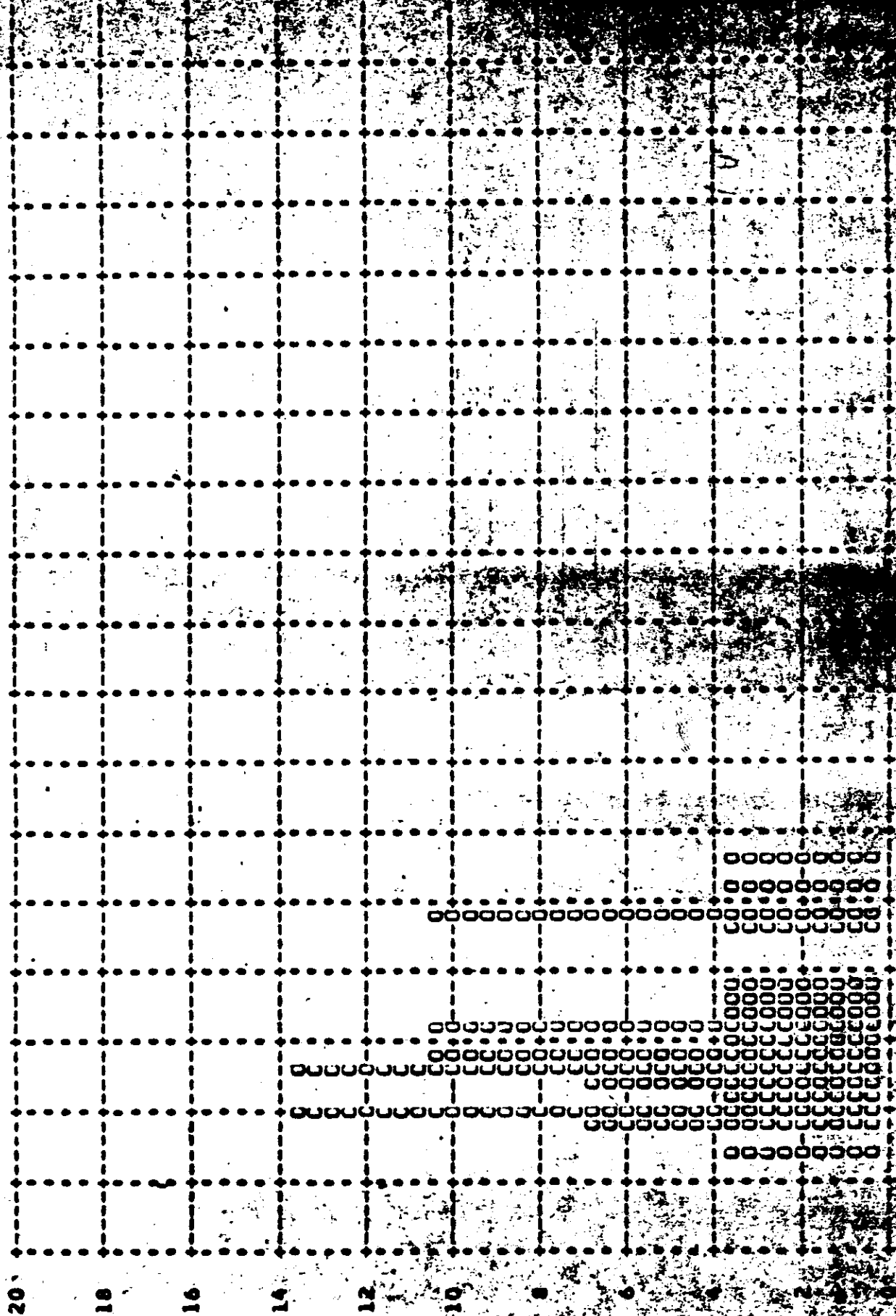
DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	C	C	0	0	0	0	0	0	0	0	0	0
2.52	C	C	0	0	0	0	0	0	0	0	0	0
2.53	C	C	0	0	0	0	0	0	0	0	0	0
2.54	C	C	0	0	0	0	0	0	0	0	0	0
2.55	C	C	0	0	0	0	0	0	0	0	0	0
2.56	C	C	0	0	0	0	0	0	0	0	0	0
2.57	C	C	0	0	0	0	0	0	0	0	0	0
2.58	C	C	0	0	0	0	0	0	0	0	0	0
2.59	C	C	0	0	0	0	0	0	0	0	0	0
2.60	C	C	0	0	0	0	0	0	0	0	0	0
2.61	C	C	0	0	0	0	0	0	0	0	0	0
2.62	C	C	0	0	0	0	0	0	0	0	0	0
2.63	C	C	0	0	0	0	0	0	0	0	0	0
2.64	C	C	0	0	0	0	0	0	0	0	0	0
2.65	C	C	0	0	0	0	0	0	0	0	0	0
2.66	C	C	0	0	0	0	0	0	0	0	0	0
2.67	C	C	0	0	0	0	0	0	0	0	0	0
2.68	C	C	0	0	0	0	0	0	0	0	0	0
2.69	C	C	0	0	0	0	0	0	0	0	0	0
2.70	C	C	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	C	C	0	0	0	0	0	0	0	0	0	0
TOTAL	C	C	0	30	30	27	237	237	131	267	267	158

MISSION 1028-1		INSTR - AFT		2-11-66		PROCESSING AND EXPOSURE AN				
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	EXPOS	EXPOS	EXPOS	EXPOS	EXPOS
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0	0	0	0	0
INTERMEDIATE	30	3 PC	43 PC	53 PC	0 PC	0	0	0	0	0
FULL	237	63 PC	0 PC	35 PC	2 PC	0	0	0	0	0
ALL LEVELS	267	56 PC	5 PC	37 PC	1 PC	0	0	0	0	0
PROCESS LEVEL	BASE + FCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	EXPOS	EXPOS	EXPOS	EXPOS	EXPOS
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91	AN			
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35	AN			
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70	AN			

TABLE A-2

FOR SCOUT

MISSION • 102B-1 • INSTR • AFT • 2-11-66 PLOT OF DRAIN • TERRAIN • PROCESSING • INTERHEADING  
ARITH MEAN • 0.45 • MEDIAN • 0.41 • STD DEV • 0.17 • RANGE • 0.20 TO 0.82 WITH 30 SAMPLES



PLANT • ACCOUNT OF TOTAL • AVERAGE

0 2 4 6 8 10 12 14 16 18 20

0 2 4 6 8 10

TOP SECRET

MISSION • 1028-1 • INSTR • AFI • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE  
ARITH MEAN • 1.44 • MEDIAN • 1.42 • STD DEV • 0.30 • RANGE • 0.85 TO 2.10 WITH 30 SAMPLES

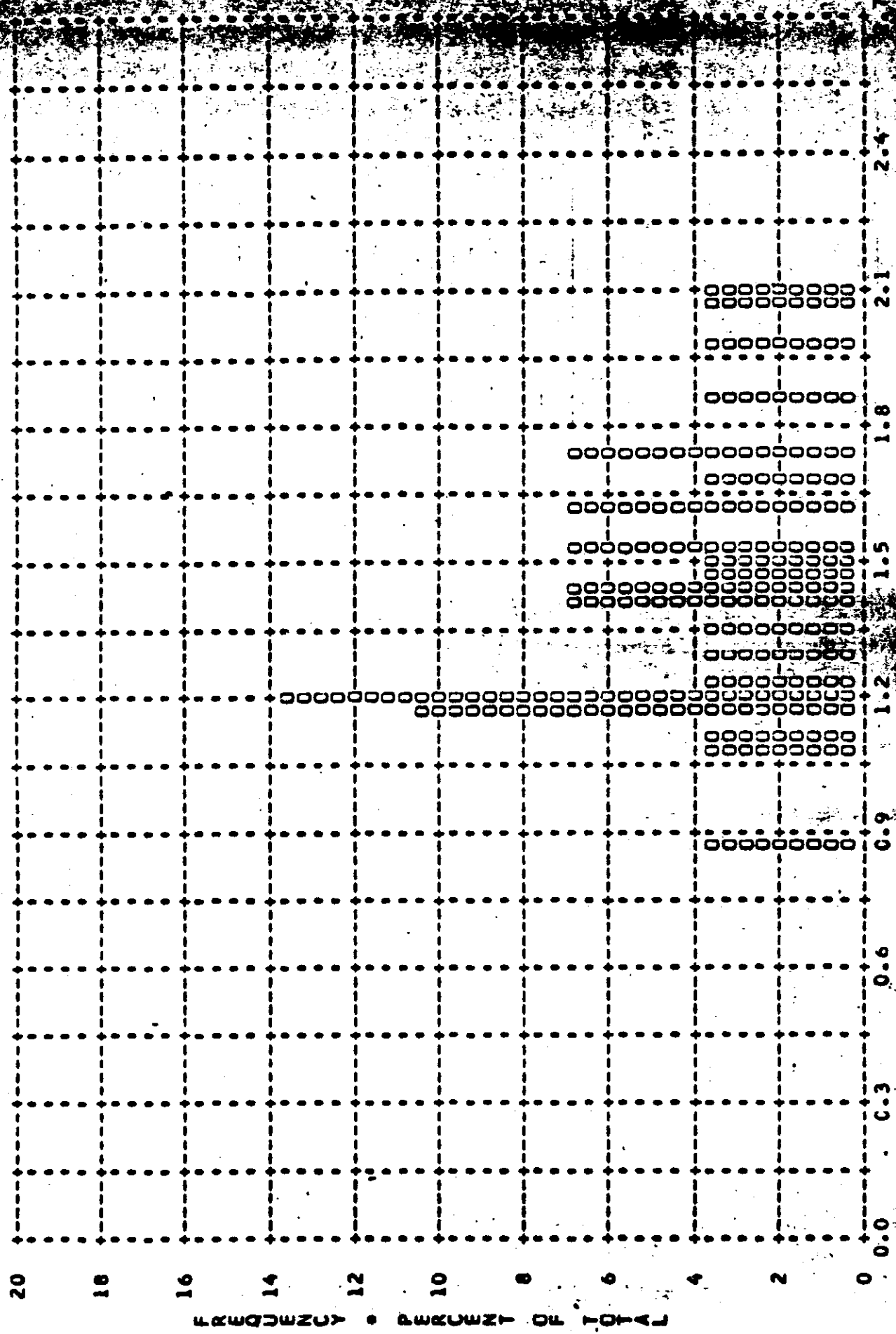


FIGURE A-11

~~TOP SECRET~~

MISSION • IC28-1 • INSTR • AFI • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE  
ARITH MEAN • 1.75 • MEDIAN • 1.83 • STD DEV • 0.34 • RANGE • 1.01 TO 2.26 WITH 27 SAMPLES

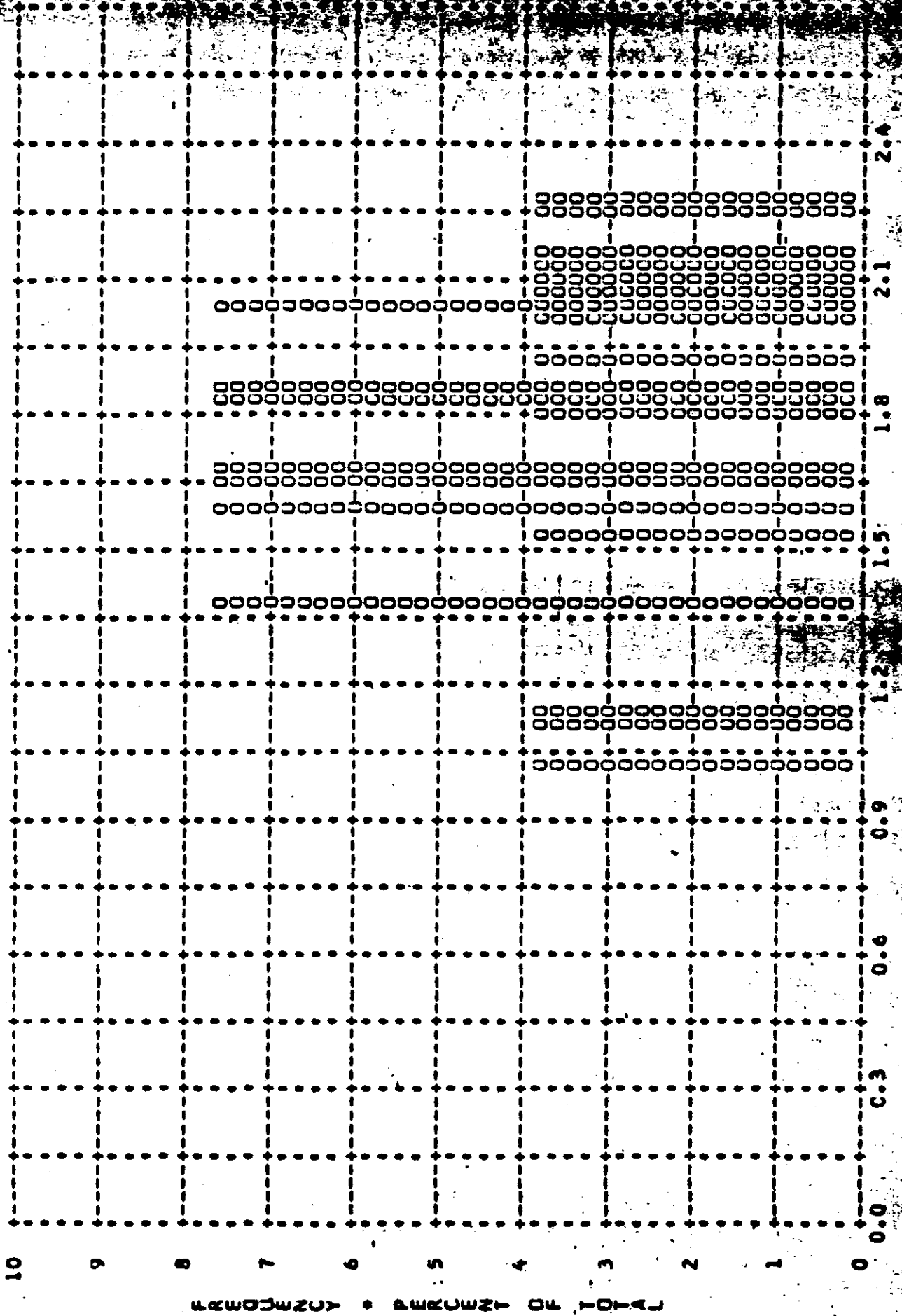


FIGURE A-12

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-1 • I-STR • AFT • 2-11-66 PLOT OF 0 MIN • TERRAIN • PROCESSING • FULL  
ARITH MEAN • 0.4C • MELIAN • C.36 • STD DEV • 0.14 • RANGE • 0.23 TO 1.01 WITH 237 SAMPLES

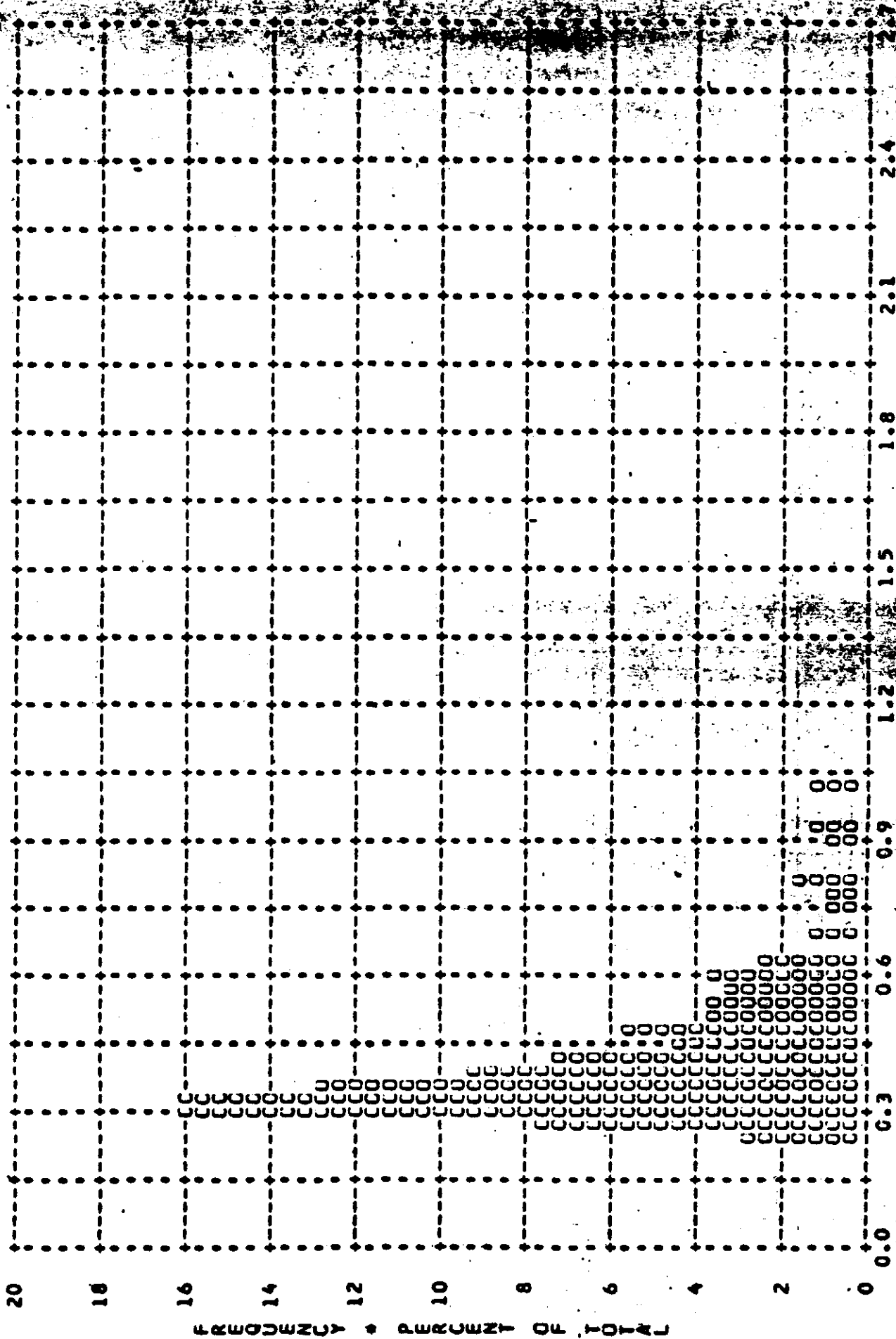
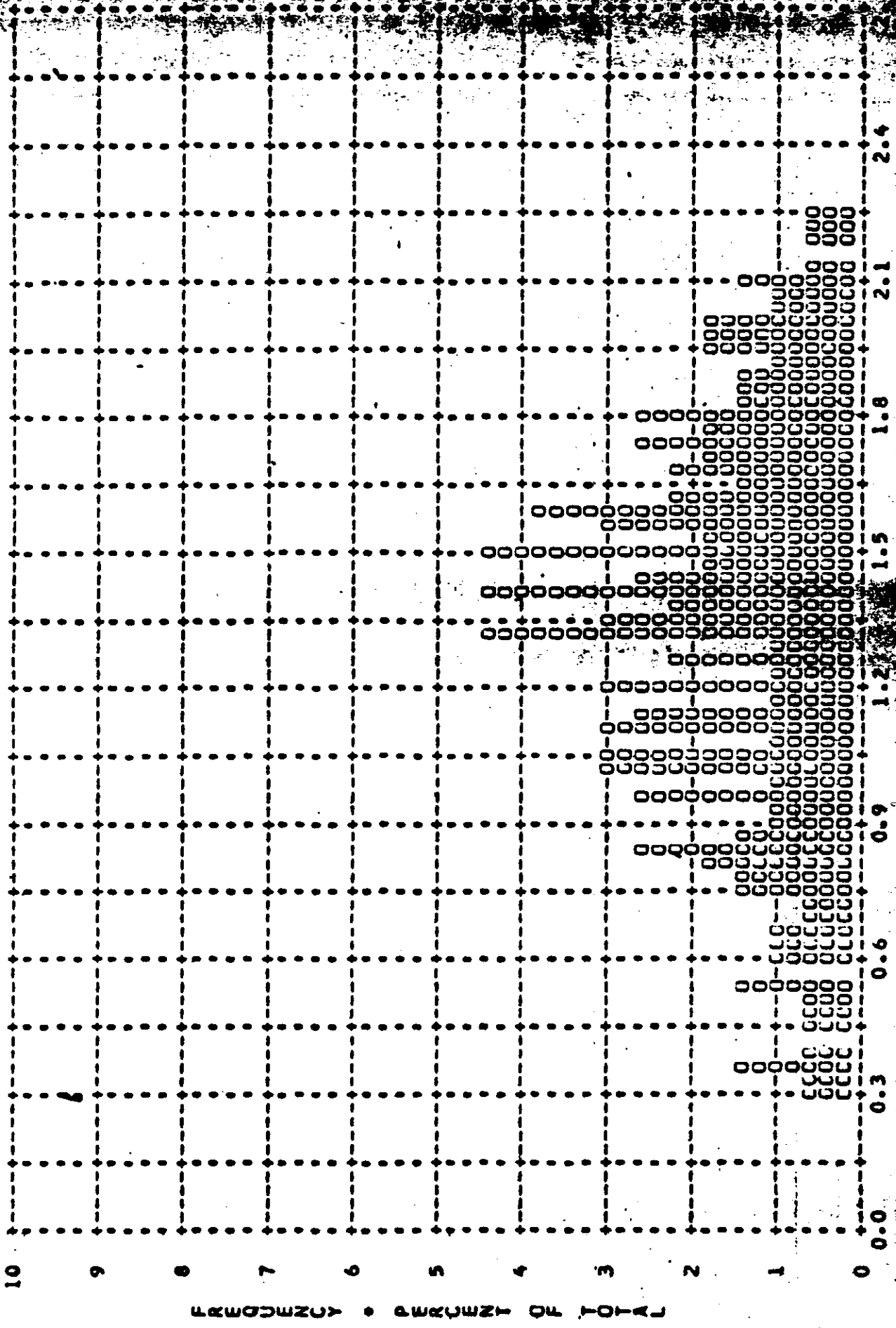


FIGURE A-13

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • AFT • 2-11-66 PLOT OF U MAX • TERRAIN • PROCESSING • FULL  
ARITH MEAN • 1.34 • MEDIAN • 1.37 • STD DEV • 0.43 • RANGE • 0.30 TO 2.23 WITH 237 SAMPLES



~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • AFT • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • FULL  
ARITH MEAN • 1.71 • MEDIAN • 1.76 • STD DEV • 0.36 • RANGE • 0.68 TO 2.26 WITH 131 SAMPLES

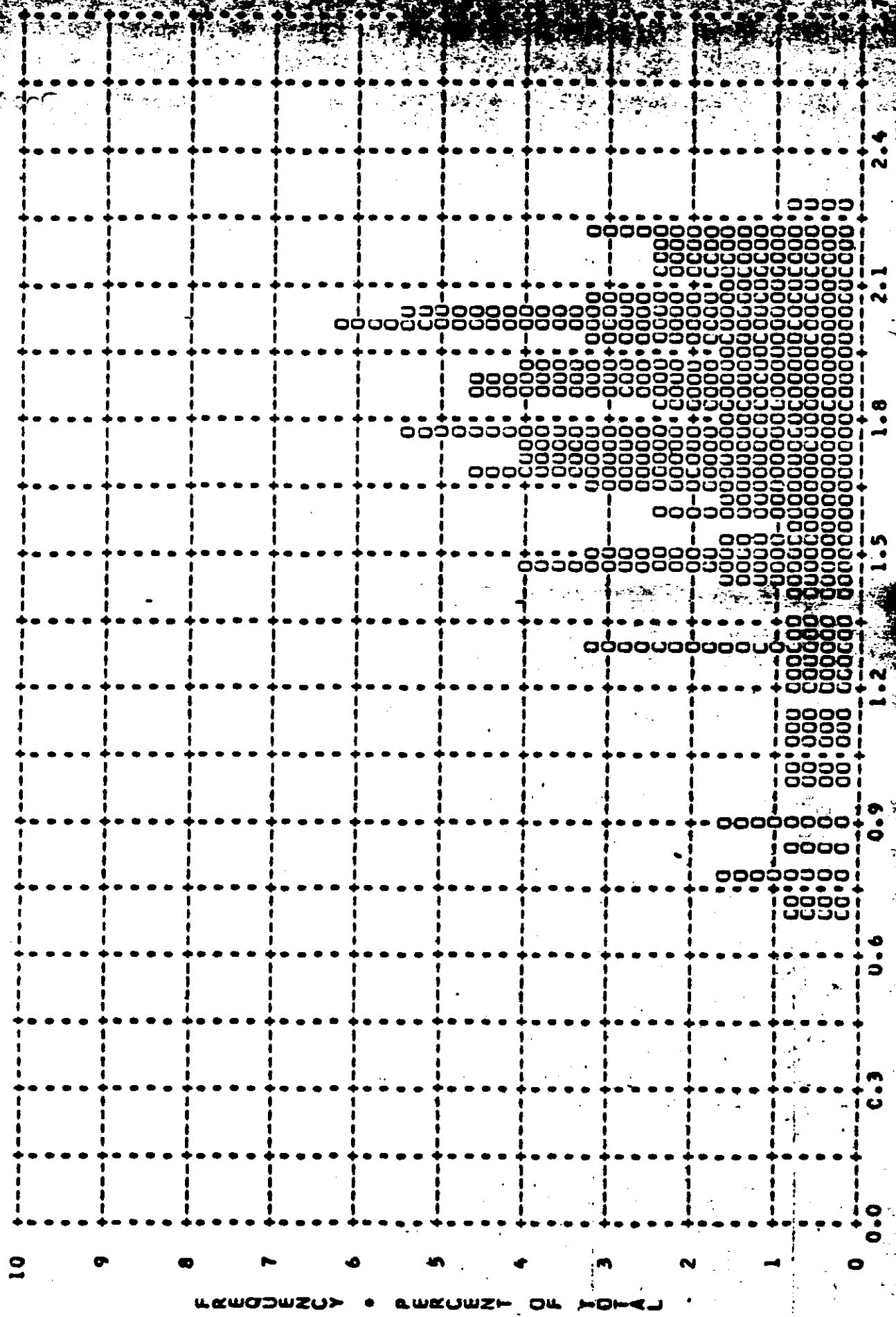


FIGURE A-15

~~TOP SECRET~~



~~TOP SECRET~~

MISSION • 1028-1 • INSTR • AFI • 2-11-66 PLOT OF 0 MIN • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • 0.41 • MEDIAN • 0.36 • STD DEV • 0.14 • RANGE • 0.20 TO 1.01 WITH 267 SAMPLES

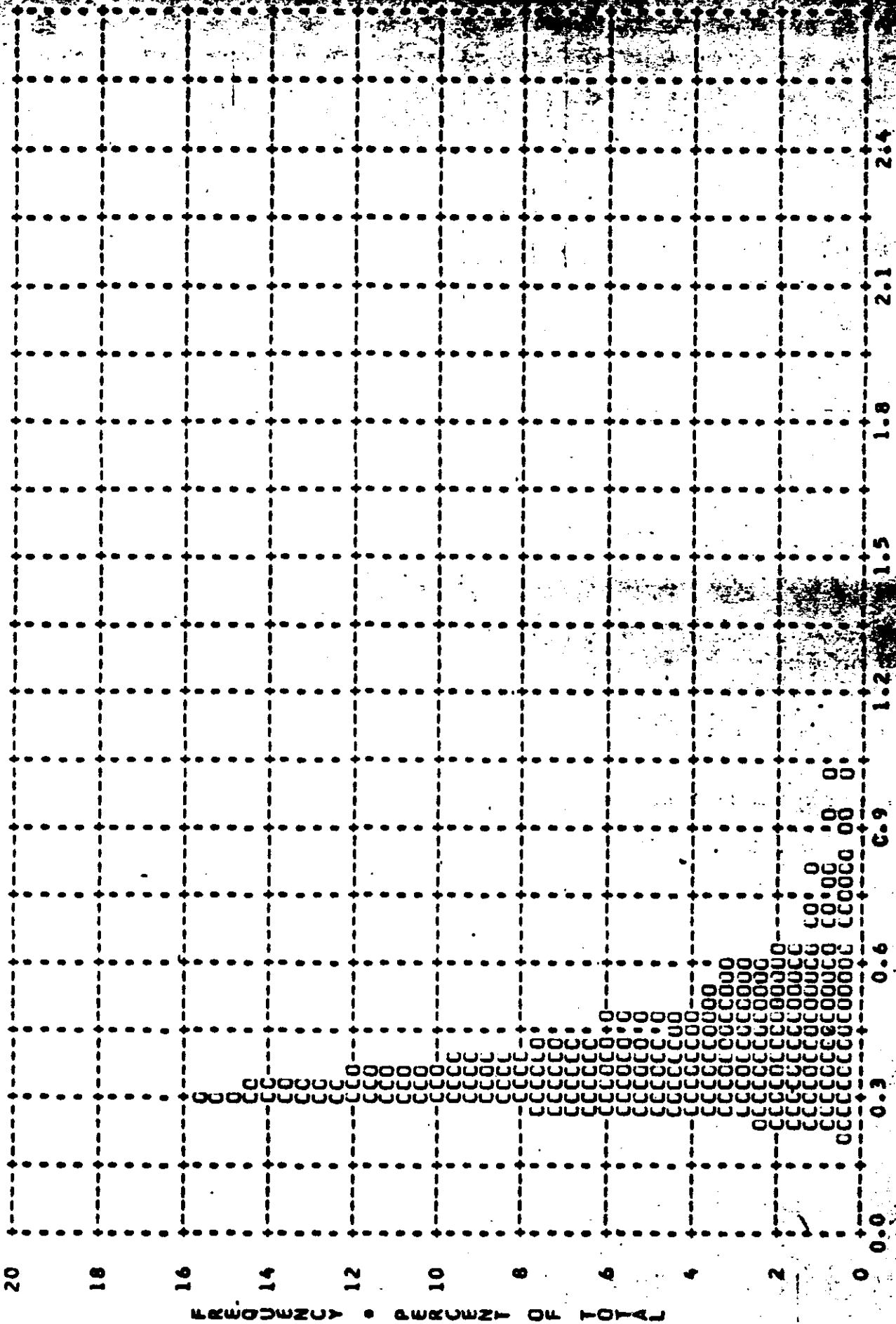


FIGURE A-16

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-1 • INSTR • AFT • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.35 • MELIAN • 1.40 • STD DEV • 0.42 • RANGE • 0.30 TO 2.23 WITH 267 SAMPLES

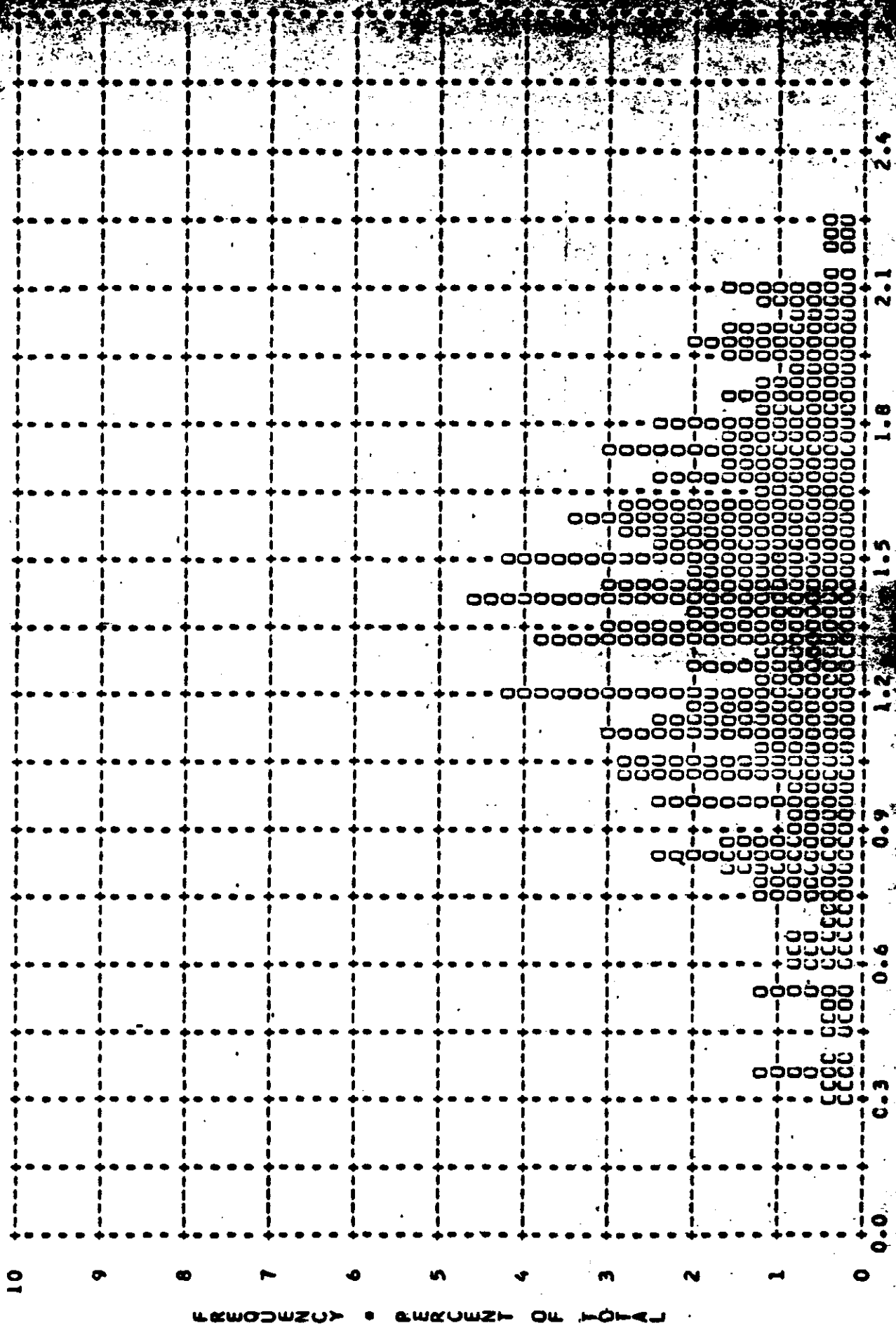
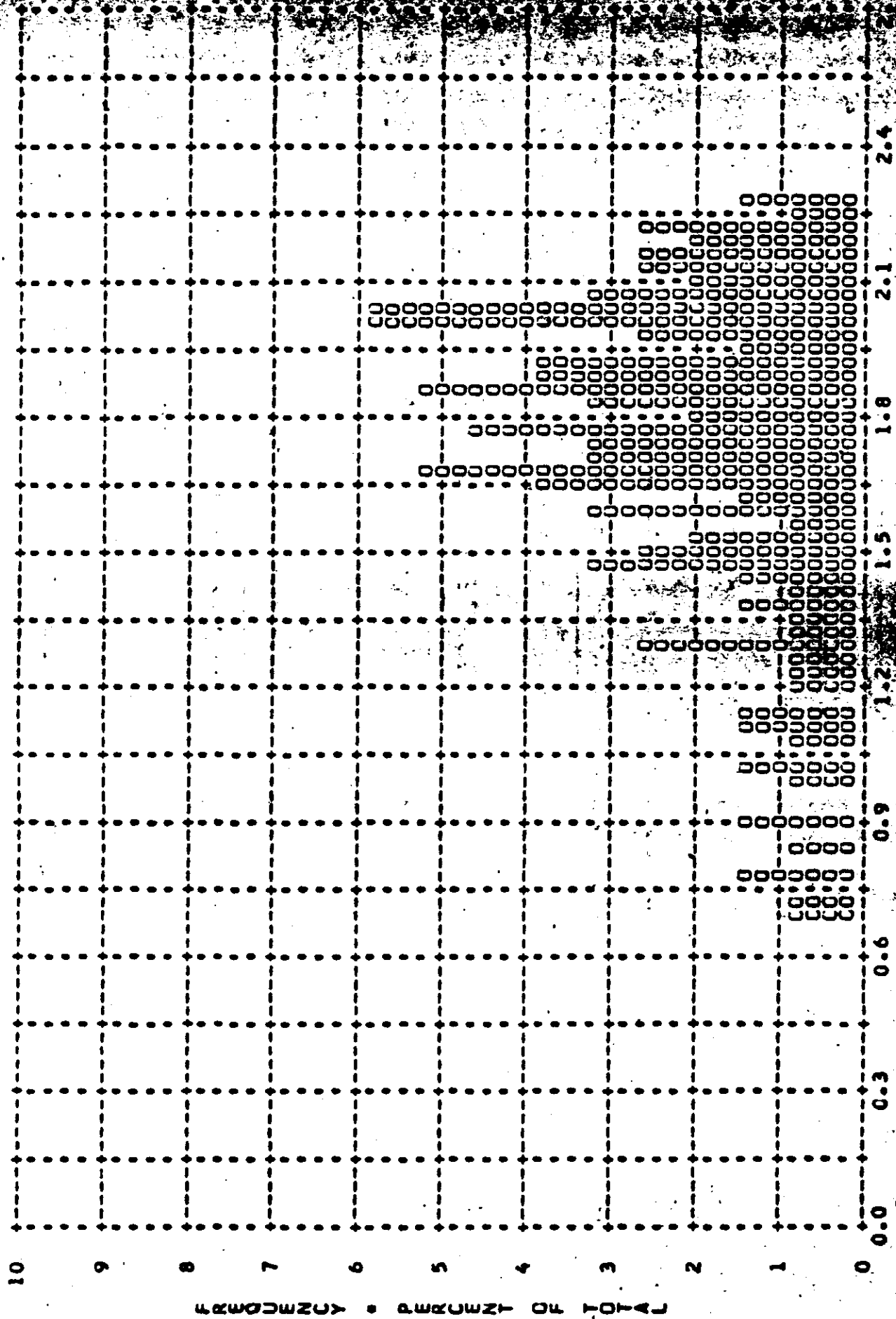


FIGURE A-17

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-1 • IJSTR • AFI • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.72 • MEDIAN • 1.77 • STD DEV • 0.36 • RANGE • 0.68 TO 2.26 WITH 158 SAMPLES



~~TOP SECRET~~

FIGURE A-18

DENSITY VALUE	PRIMARY			INTERMEDIATE			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
00.01			0			0			0
00.02			0			0			0
00.03			0			0			0
00.04			0			0			0
00.05			0			0			0
00.06			0			0			0
00.07			0			0			0
00.08			0			0			0
00.09			0			0			0
00.10			0			0			0
00.11			0			0			0
00.12			0			0			0
00.13			0			0			0
00.14			0			0			0
00.15			0			0			0
00.16			0			0			0
00.17			0			0			0
00.18			0			0			0
00.19			0			0			0
00.20			0			0			0
00.21			0			0			0
00.22			0			0			0
00.23			0			0			0
00.24			0			0			0
00.25			0			0			0
00.26			0			0			0
00.27			0			0			0
00.28			0			0			0
00.29			0			0			0
00.30			0			0			0
00.31			0			0			0
00.32			0			0			0
00.33			0			0			0
00.34			0			0			0
00.35			0			0			0
00.36			0			0			0
00.37			0			0			0
00.38			0			0			0
00.39			0			0			0
00.40			0			0			0
00.41			0			0			0
00.42			0			0			0
00.43			0			0			0
00.44			0			0			0
00.45			0			0			0
00.46			0			0			0
00.47			0			0			0
00.48			0			0			0
00.49			0			0			0
00.50			0			0			0
SUBTOTAL			18			179			197

~~TOP SECRET~~

TABLE A-3

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0.51												
0.52												
0.53												
0.54												
0.55												
0.56												
0.57												
0.58												
0.59												
0.60												
0.61												
0.62												
0.63												
0.64												
0.65												
0.66												
0.67												
0.68												
0.69												
0.70												
0.71												
0.72												
0.73												
0.74												
0.75												
0.76												
0.77												
0.78												
0.79												
0.80												
0.81												
0.82												
0.83												
0.84												
0.85												
0.86												
0.87												
0.88												
0.89												
0.90												
0.91												
0.92												
0.93												
0.94												
0.95												
0.96												
0.97												
0.98												
0.99												
1.00												
SUBTOTAL												

TABLE A-3

DENSITY VALUE      PRIMARY MIN MAX LIM      INTERMEDIATE MIN MAX LIM      ALL LEVELS MIN MAX LIM

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.01	0000000000	0000000000	0000000000
1.02	0000000000	0000000000	0000000000
1.03	0000000000	0000000000	0000000000
1.04	0000000000	0000000000	0000000000
1.05	0000000000	0000000000	0000000000
1.06	0000000000	0000000000	0000000000
1.07	0000000000	0000000000	0000000000
1.08	0000000000	0000000000	0000000000
1.09	0000000000	0000000000	0000000000
1.10	0000000000	0000000000	0000000000
1.11	0000000000	0000000000	0000000000
1.12	0000000000	0000000000	0000000000
1.13	0000000000	0000000000	0000000000
1.14	0000000000	0000000000	0000000000
1.15	0000000000	0000000000	0000000000
1.16	0000000000	0000000000	0000000000
1.17	0000000000	0000000000	0000000000
1.18	0000000000	0000000000	0000000000
1.19	0000000000	0000000000	0000000000
1.20	0000000000	0000000000	0000000000
1.21	0000000000	0000000000	0000000000
1.22	0000000000	0000000000	0000000000
1.23	0000000000	0000000000	0000000000
1.24	0000000000	0000000000	0000000000
1.25	0000000000	0000000000	0000000000
1.26	0000000000	0000000000	0000000000
1.27	0000000000	0000000000	0000000000
1.28	0000000000	0000000000	0000000000
1.29	0000000000	0000000000	0000000000
1.30	0000000000	0000000000	0000000000
1.31	0000000000	0000000000	0000000000
1.32	0000000000	0000000000	0000000000
1.33	0000000000	0000000000	0000000000
1.34	0000000000	0000000000	0000000000
1.35	0000000000	0000000000	0000000000
1.36	0000000000	0000000000	0000000000
1.37	0000000000	0000000000	0000000000
1.38	0000000000	0000000000	0000000000
1.39	0000000000	0000000000	0000000000
1.40	0000000000	0000000000	0000000000
1.41	0000000000	0000000000	0000000000
1.42	0000000000	0000000000	0000000000
1.43	0000000000	0000000000	0000000000
1.44	0000000000	0000000000	0000000000
1.45	0000000000	0000000000	0000000000
1.46	0000000000	0000000000	0000000000
1.47	0000000000	0000000000	0000000000
1.48	0000000000	0000000000	0000000000
1.49	0000000000	0000000000	0000000000
1.50	0000000000	0000000000	0000000000
SUBTOTAL		26	26

~~TOP SECRET~~

TABLE A-3

DENSITY VALUE	PRIMARY		INTERMEDIATE			FULL			ALL LEVELS			
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
1.51			0			0			0			0
1.52			0			0			0			0
1.53			0			0			0			0
1.54			0			0			0			0
1.55			0			0			0			0
1.56			0			0			0			0
1.57			0			0			0			0
1.58			0			0			0			0
1.59			0			0			0			0
1.60			0			0			0			0
1.61			0			0			0			0
1.62			0			0			0			0
1.63			0			0			0			0
1.64			0			0			0			0
1.65			0			0			0			0
1.66			0			0			0			0
1.67			0			0			0			0
1.68			0			0			0			0
1.69			0			0			0			0
1.70			0			0			0			0
1.71			0			0			0			0
1.72			0			0			0			0
1.73			0			0			0			0
1.74			0			0			0			0
1.75			0			0			0			0
1.76			0			0			0			0
1.77			0			0			0			0
1.78			0			0			0			0
1.79			0			0			0			0
1.80			0			0			0			0
1.81			0			0			0			0
1.82			0			0			0			0
1.83			0			0			0			0
1.84			0			0			0			0
1.85			0			0			0			0
1.86			0			0			0			0
1.87			0			0			0			0
1.88			0			0			0			0
1.89			0			0			0			0
1.90			0			0			0			0
1.91			0			0			0			0
1.92			0			0			0			0
1.93			0			0			0			0
1.94			0			0			0			0
1.95			0			0			0			0
1.96			0			0			0			0
1.97			0			0			0			0
1.98			0			0			0			0
1.99			0			0			0			0
2.00			0			0			0			0
SUBTOTAL			0			0			0			0

TABLE A-3

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALC LEVEL					
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM			
01															
02															
03															
04															
05															
06															
07															
08															
09															
10															
11															
12															
13															
14															
15															
16															
17															
18															
19															
20															
21															
22															
23															
24															
25															
26															
27															
28															
29															
30															
31															
32															
33															
34															
35															
36															
37															
38															
39															
40															
41															
42															
43															
44															
45															
46															
47															
48															
49															
50															
SUBTOTAL															

TOP SECRET

TABLE A-3



DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			TOTAL		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	36	36	27	206	206	155	242	242	182

MISSION 1028-2 INSTR - FRWD 2-11-66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	36	0 PC	19 PC	11 PC	0 PC	0 PC
FULL	206	69 PC	0 PC	30 PC	0 PC	0 PC
ALL LEVELS	242	59 PC	3 PC	37 PC	0 PC	0 PC

PROCESS LEVEL	BASE + FCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-C.09	0.01-C.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP
INTERMED	0.10-C.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

TOP SECRET

TABLE A-3

~~TOP SECRET~~

MISSION • 1028-2 • INSTK • FRWD • 2-11-66 PLOT OF D MIN • TERRAIN • PROCESSING • INTERMEDIATE  
ARITH MEAN • 0.55 • MEDIAN • 0.52 • STD DEV • 0.17 • RANGE • 0.24 TO 0.90 WITH 36 SAMPLES

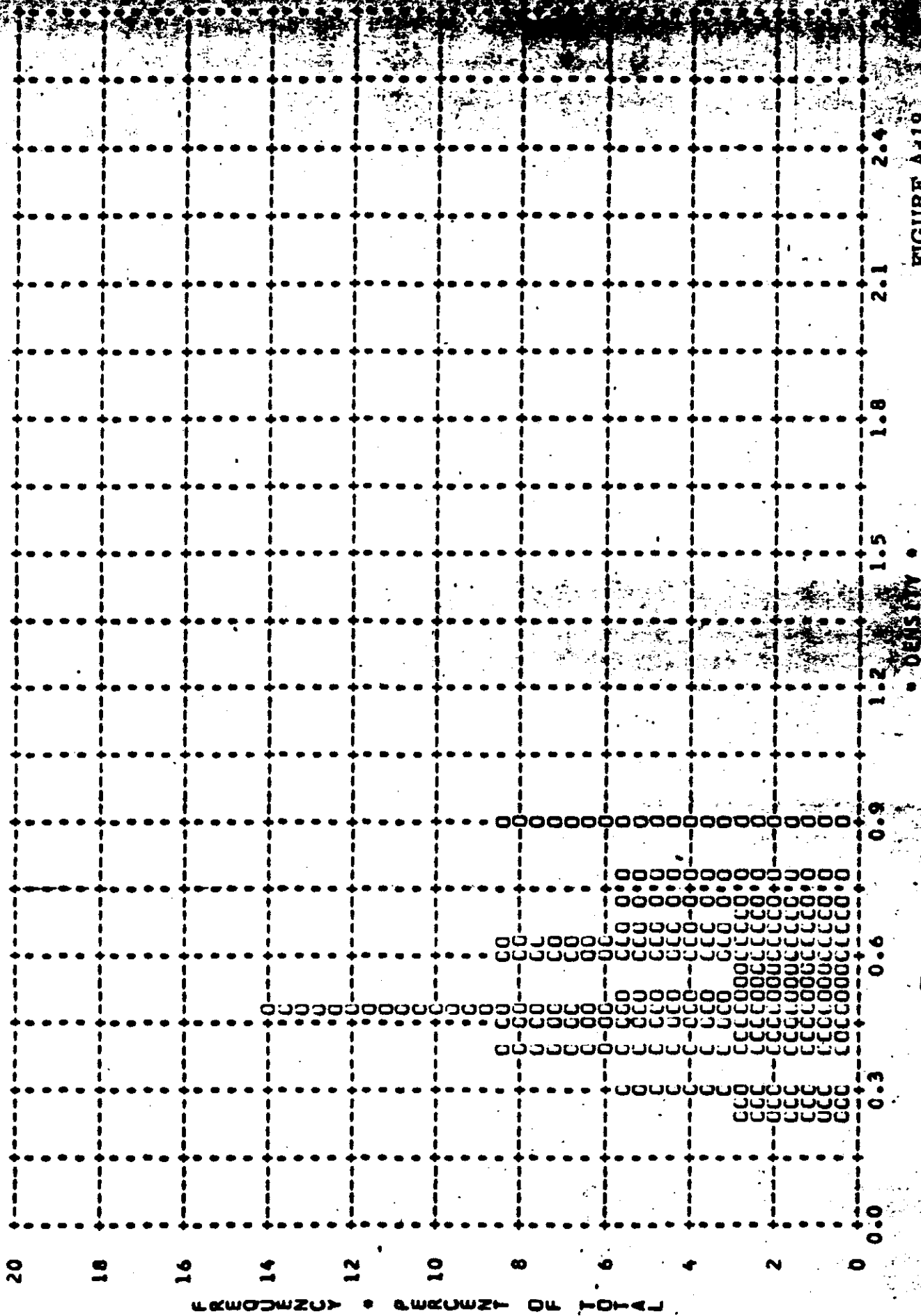


FIGURE A-19

~~TOP SECRET~~

MISSION \* 102R-2 \* INSTR \* FRWD \* 2-11-66 PLOT OF D MAX \* TERRAIN \* PROCESSING \* INTERMEDIATE  
 ARITH MEAN \* 1.35 \* MEDIAN \* 1.40 \* STD DEV \* 0.25 \* RANGE \* 0.90 TO 2.14 WITH 36 SAMPLES

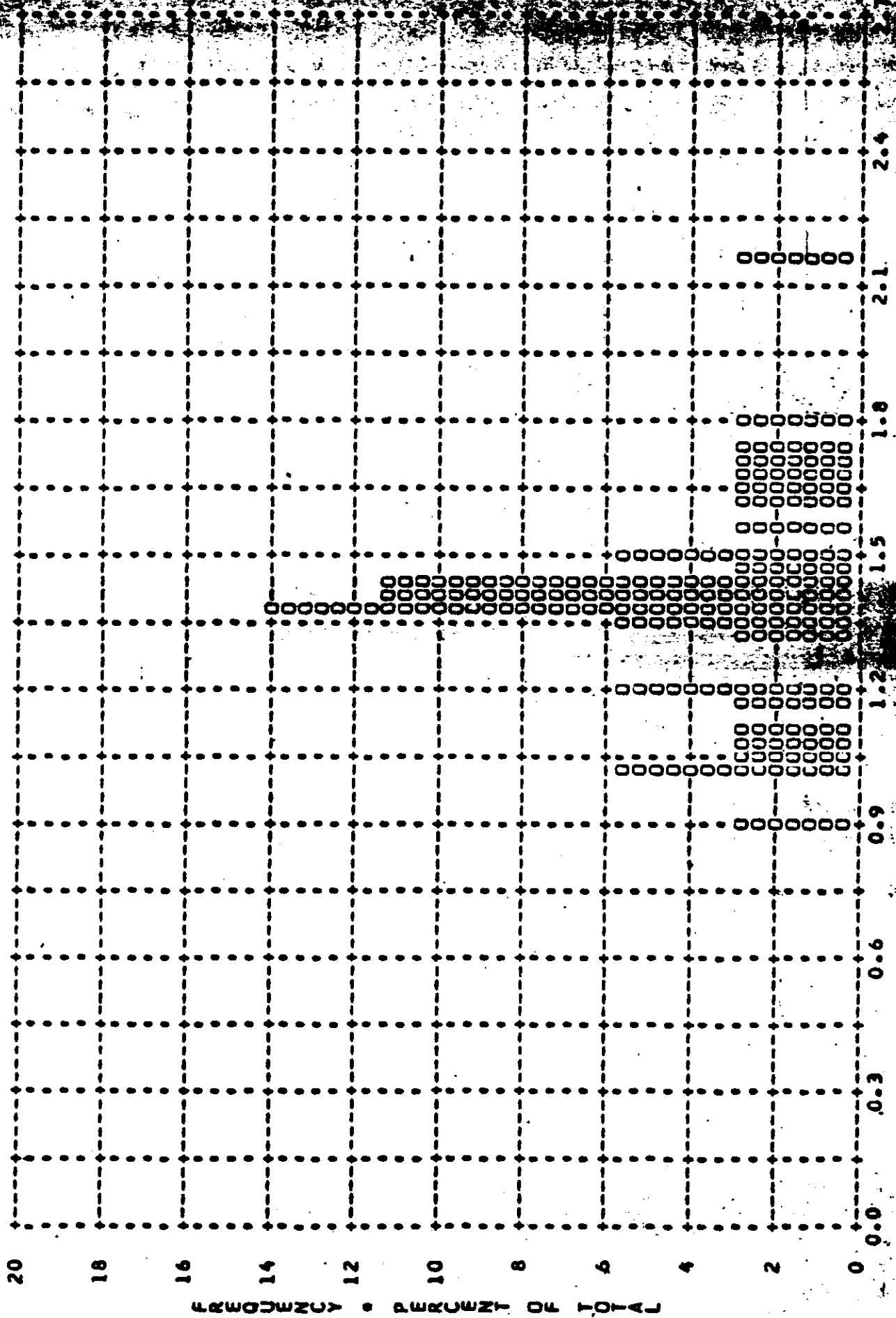


FIGURE A-20

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • FRMD • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE  
ARITH MEAN • 1.66 • MEDIAN • 1.70 • STD DEV • 0.23 • RANGE • 1.08 TO 2.00 WITH 27 SAMPLES

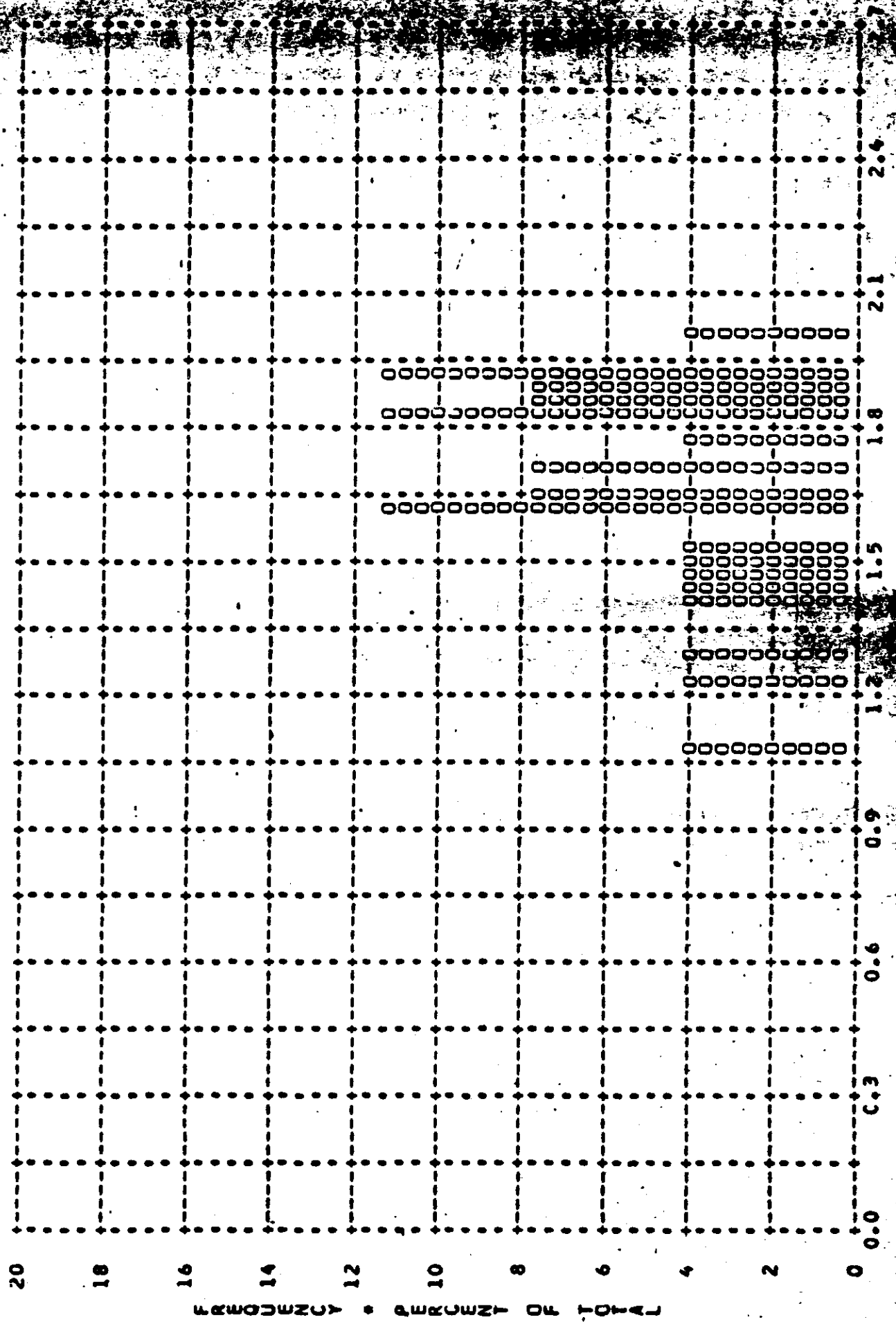
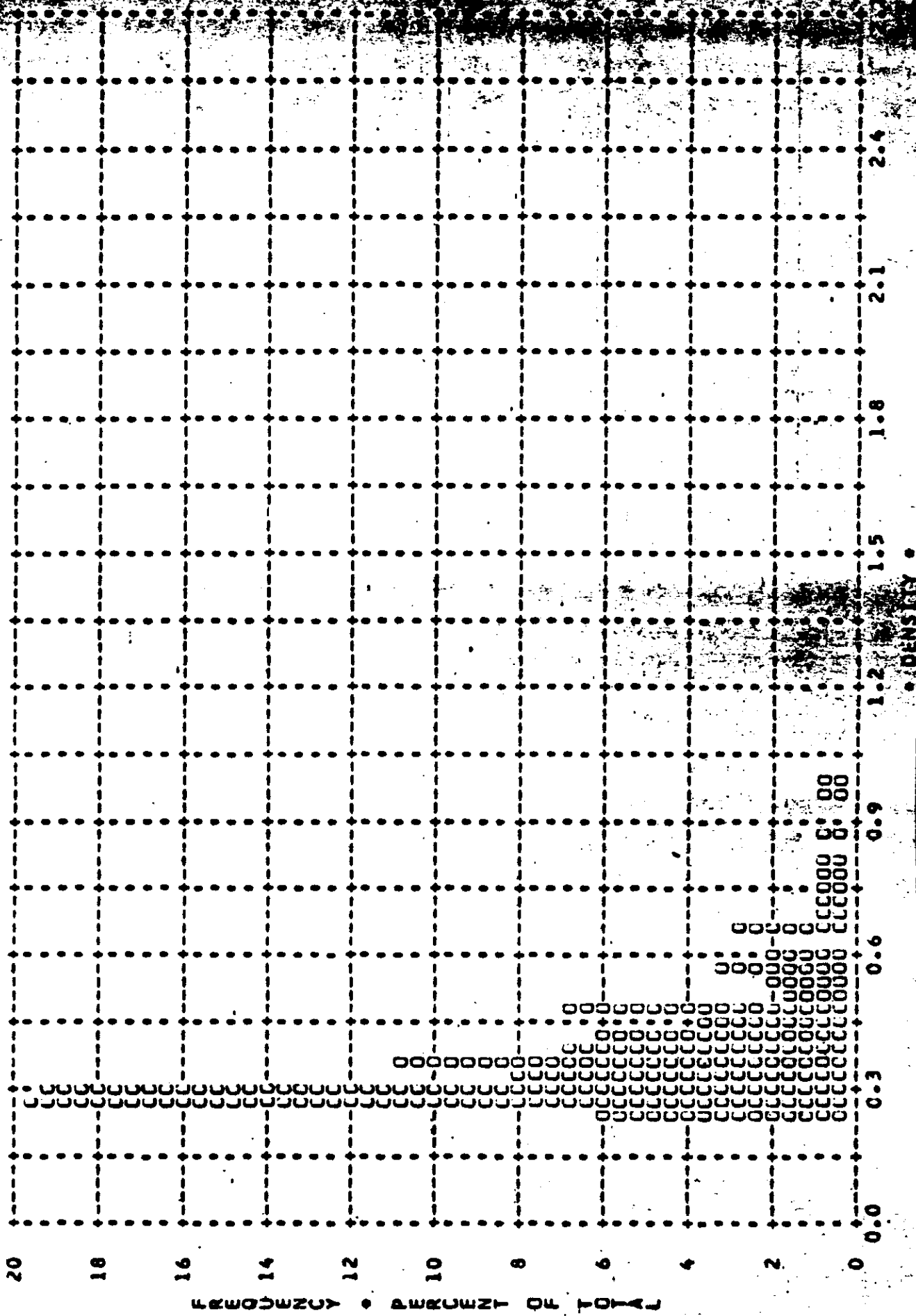


FIGURE A-21

~~TOP SECRET~~

~~TOP SECRET~~

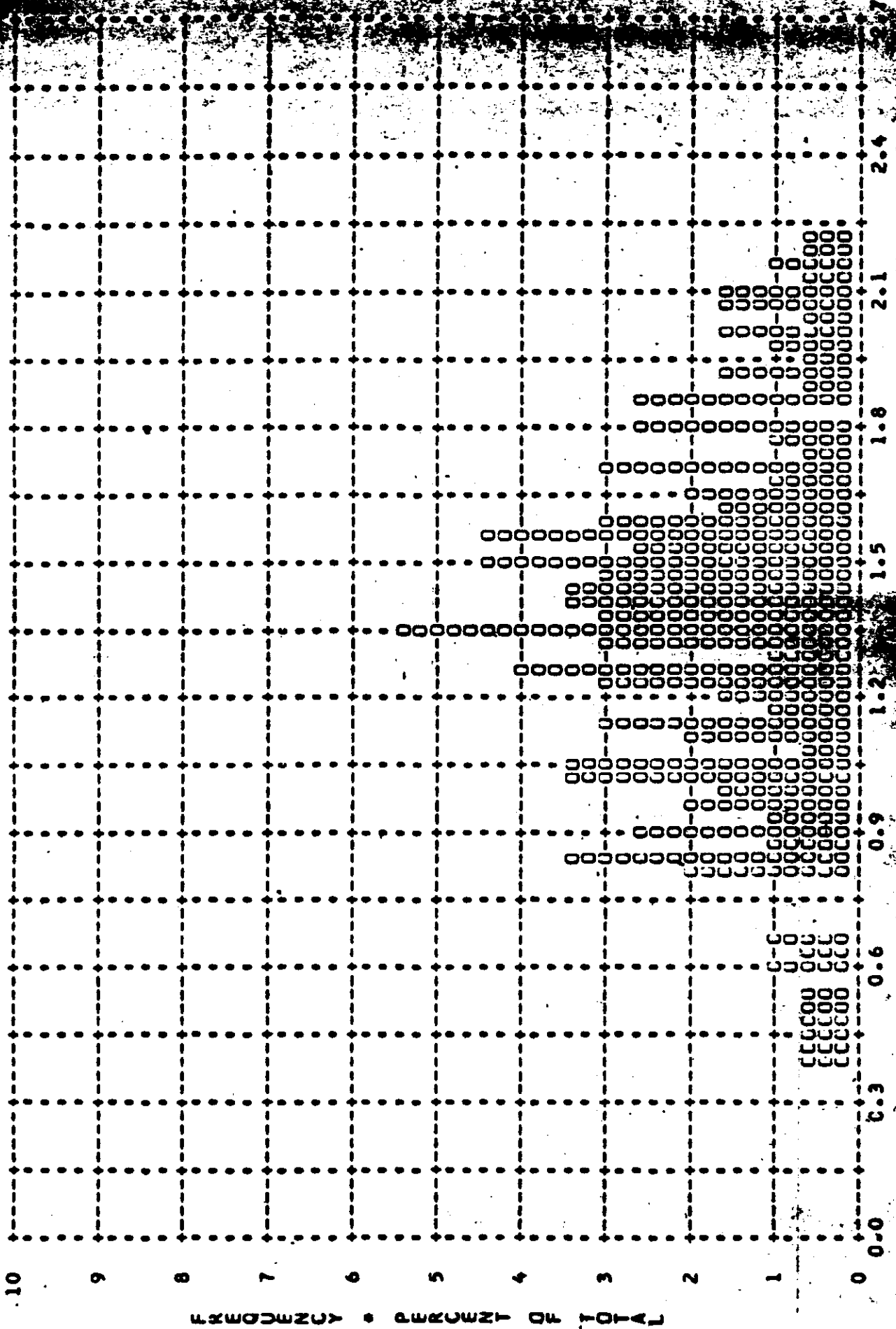
MISSION • 1028-2 • INSTR • FRWD • 2-11-66 PLOT OF D MIN • TERRAIN • PROCESSING • FULL  
ARITH MEAN • 0.37 • MEDIAN • 0.32 • STD DEV • 0.14 • RANGE • 0.23 TO 0.98 WITH 206 SAMPLES



~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • FRWD • 2-11-66 PLOT OF U MAX • TERRAIN • PROCESSING • FULL  
ARITH MEAN • 1.35 • MEDIAN • 1.37 • STD DEV • 0.39 • RANGE • 0.37 TO 2.20 WITH 206 SAMPLES



~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • FRWD • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • FULL  
ARITH MEAN • 1.73 • MEDIAN • 1.79 • STD DEV • 0.36 • RANGE • 0.30 TO 2.33 WITH 155 SAMPLES

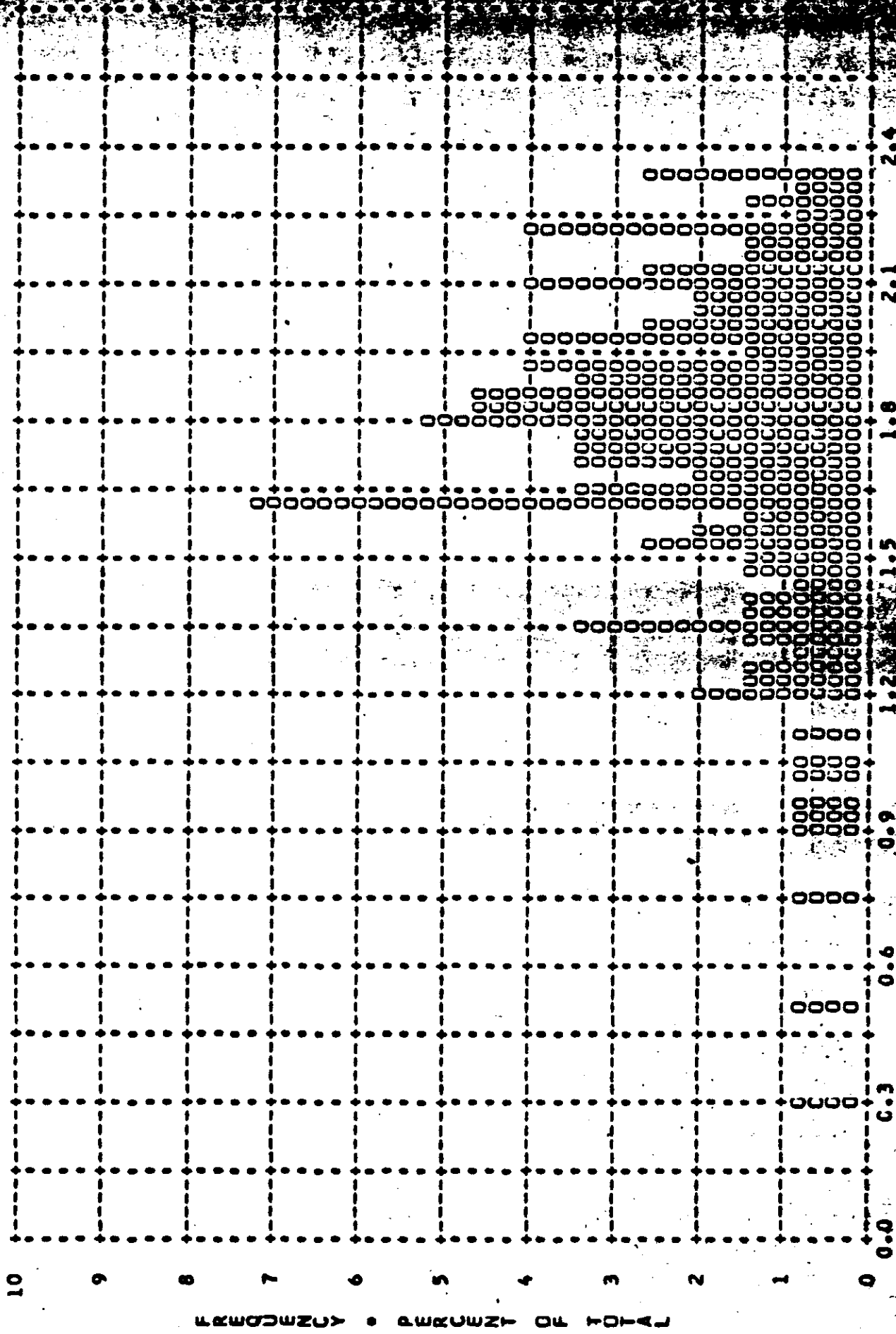


FIGURE A-24

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • FRMD • 2-11-66 PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • 0.40 • MEDIAN • 0.35 • STD DEV • 0.15 • RANGE • 0.23 TO 0.98 WITH 242 SAMPLES

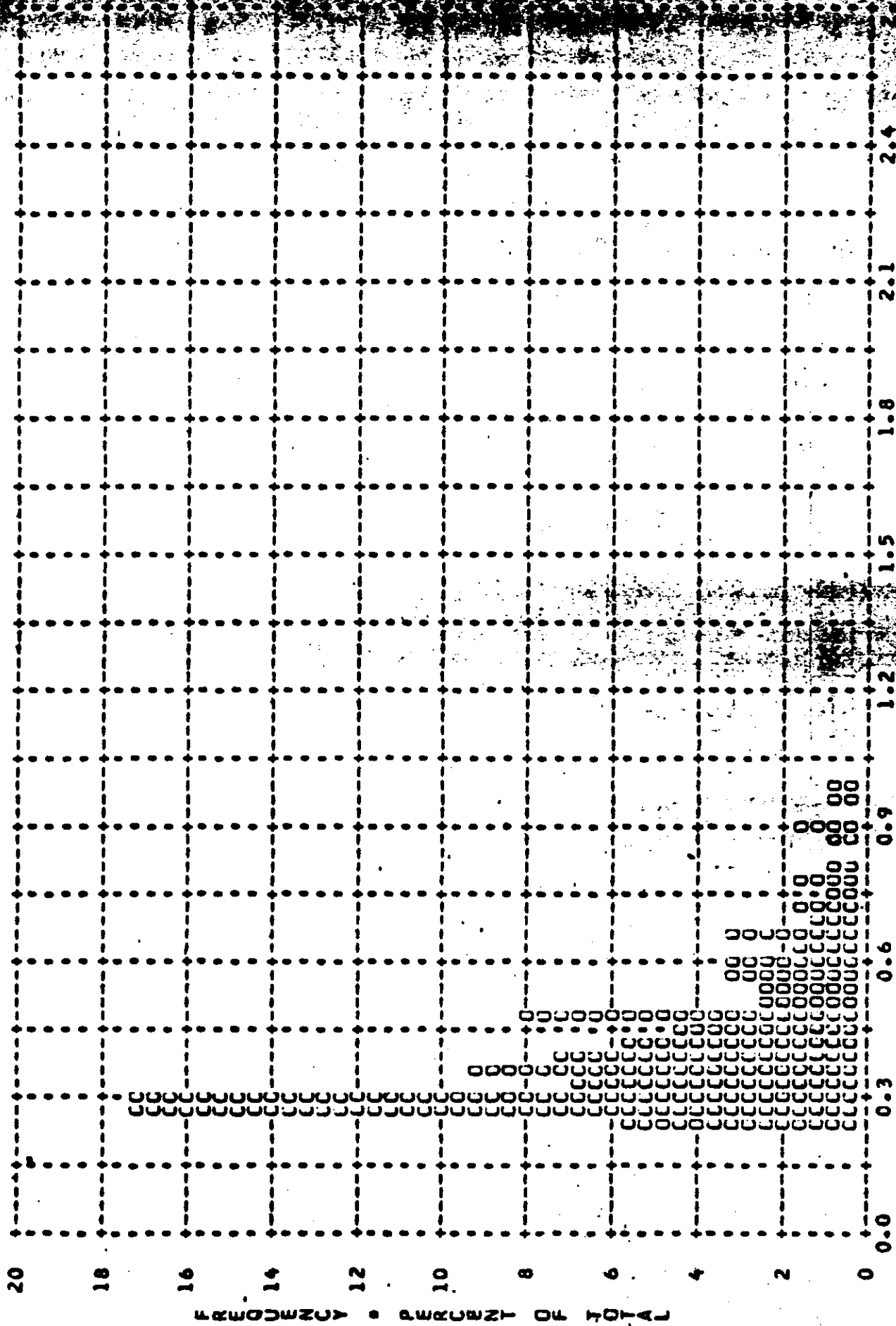


FIGURE A-25

• DENSITY •

~~TOP SECRET~~



~~TOP SECRET~~

MISSION • 1028-2 • INSTR • FRND • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.36 • MEDIAN • 1.38 • STD DEV • 0.38 • RANGE • 0.37 TO 2.20 WITH 242 SAMPLES

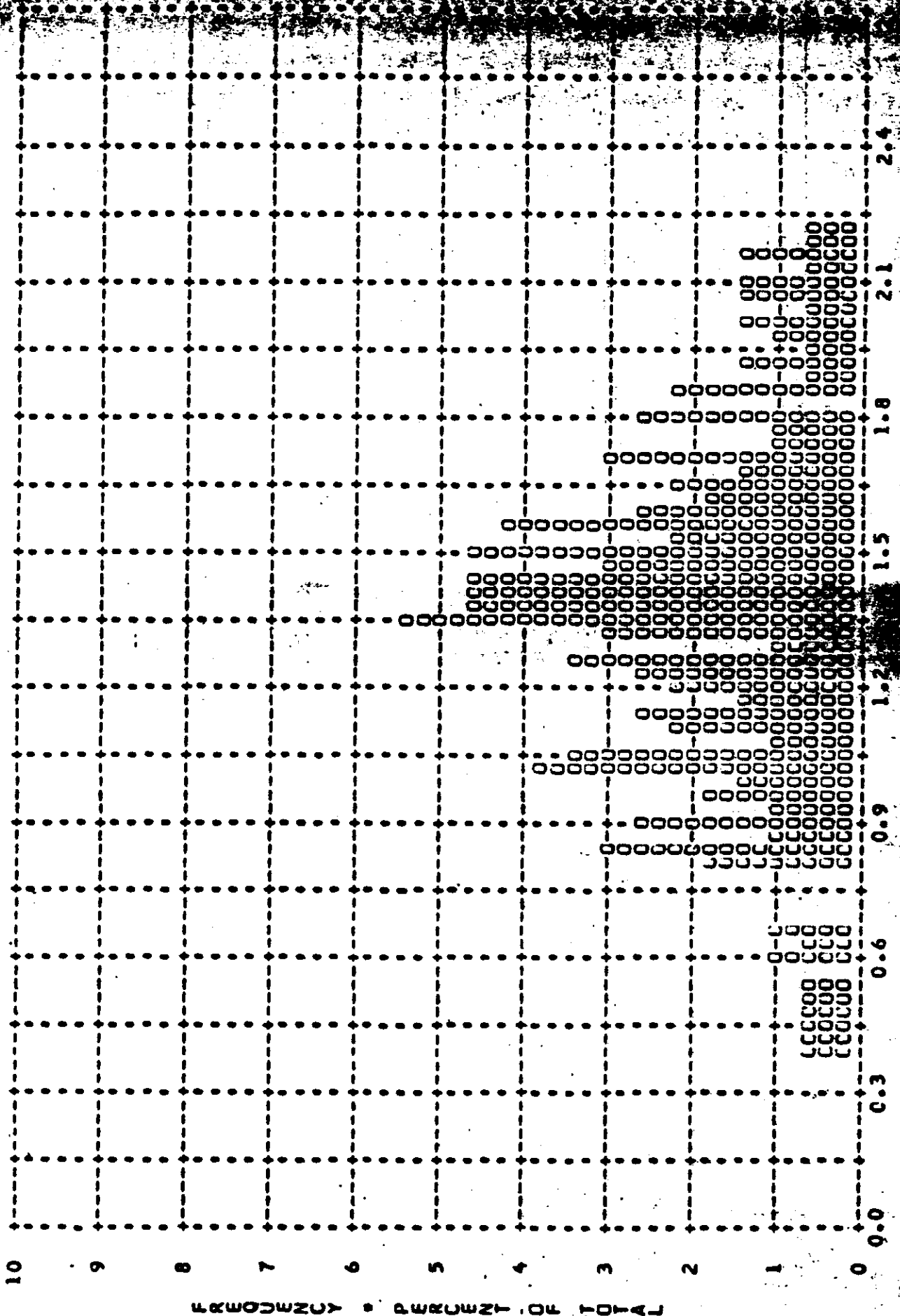
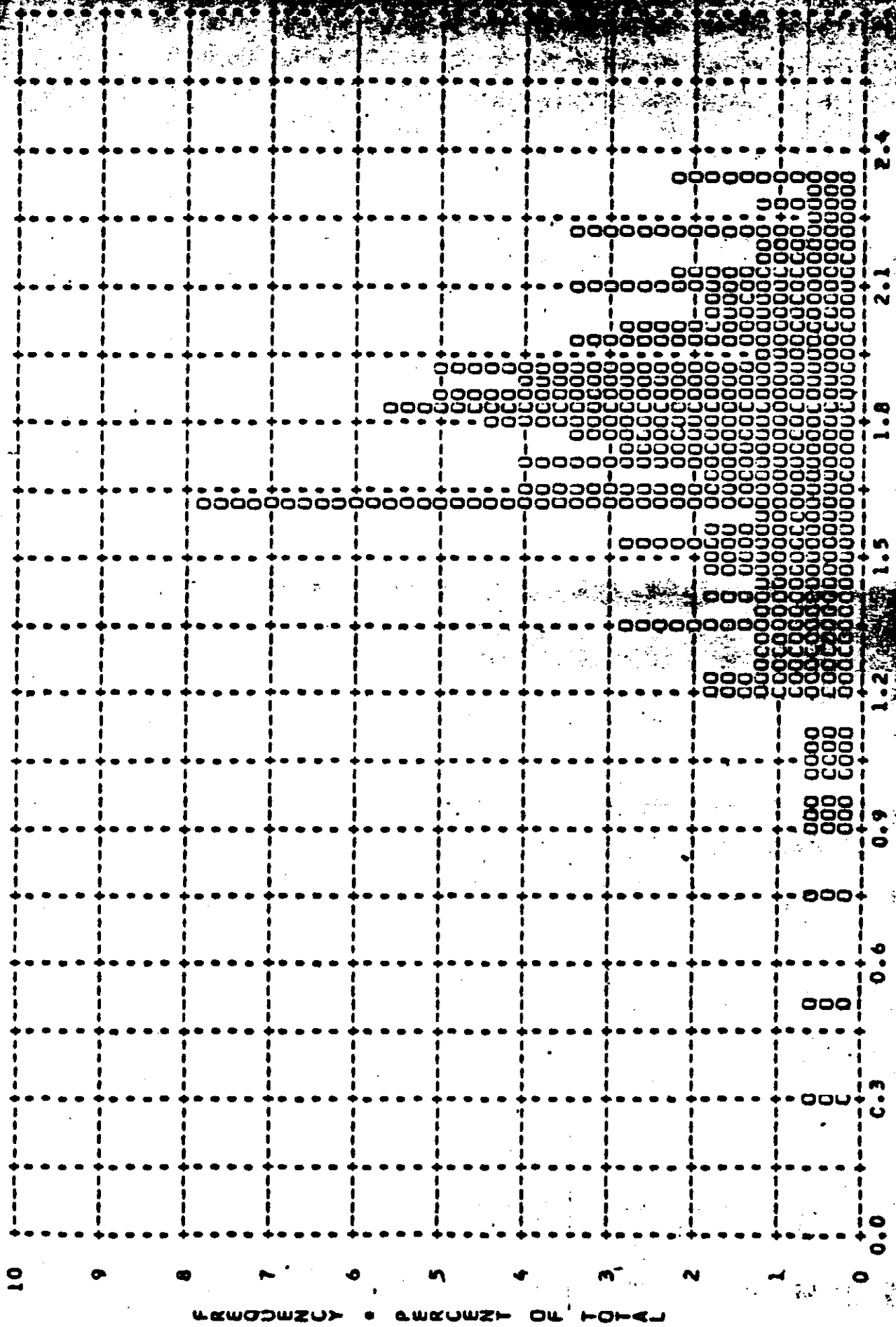


FIGURE A-26

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • FRWD • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.72 • MEDIAN • 1.77 • STD DEV • 0.35 • RANGE • 0.30 TO 2.33 WITH 182 SAMPLES



~~TOP SECRET~~

FIGURE A-27

~~TOP SECRET~~

MISSION • 1020-2 • INSTR • FRWD • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.72 • MEDIAN • 1.77 • STD DEV • 0.35 • RANGE • 0.30 TO 2.33 WITH 182 SAMPLES

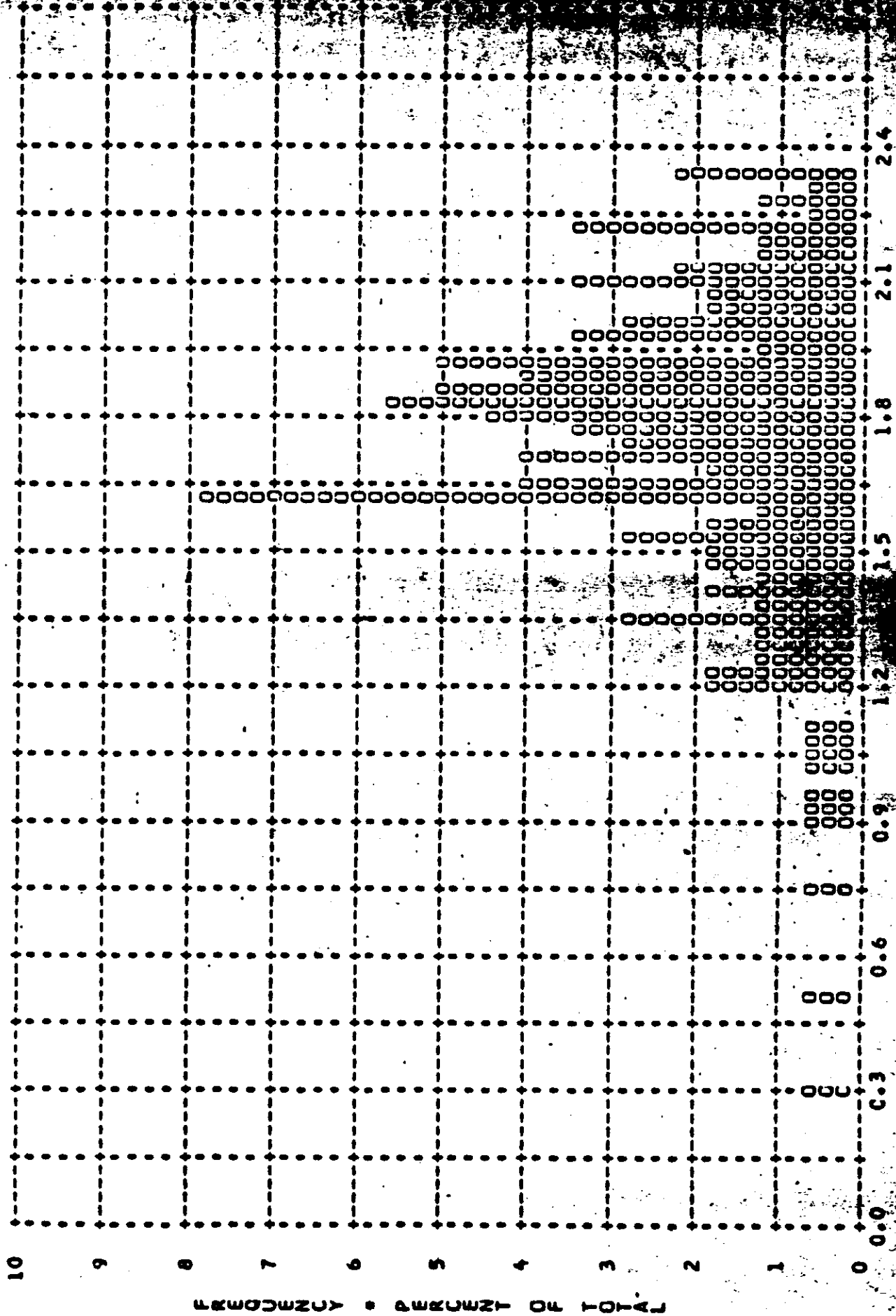


FIGURE A-28

~~TOP SECRET~~

DENSITY VALUE	PRIMARY			INTERMEDIATE			HIGH LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
0.01									
0.02									
0.03									
0.04									
0.05									
0.06									
0.07									
0.08									
0.09									
0.10									
0.11									
0.12									
0.13									
0.14									
0.15									
0.16									
0.17									
0.18									
0.19									
0.20									
0.21									
0.22									
0.23									
0.24									
0.25									
0.26									
0.27									
0.28									
0.29									
0.30									
0.31									
0.32									
0.33									
0.34									
0.35									
0.36									
0.37									
0.38									
0.39									
0.40									
0.41									
0.42									
0.43									
0.44									
0.45									
0.46									
0.47									
0.48									
0.49									
0.50									
SUBTOTAL									

~~TOP SECRET~~ [REDACTED]

TABLE A-4

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
00.51												
00.52												
00.53												
00.54												
00.55												
00.56												
00.57												
00.58												
00.59												
00.60												
00.61												
00.62												
00.63												
00.64												
00.65												
00.66												
00.67												
00.68												
00.69												
00.70												
00.71												
00.72												
00.73												
00.74												
00.75												
00.76												
00.77												
00.78												
00.79												
00.80												
00.81												
00.82												
00.83												
00.84												
00.85												
00.86												
00.87												
00.88												
00.89												
00.90												
00.91												
00.92												
00.93												
00.94												
00.95												
00.96												
00.97												
00.98												
00.99												
01.00												
SUBTOTAL												
TOTAL												

TABLE A-4

DENSITY VALUE	PRIMARY			INTERMEDIATE			ALL LEVELS					
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM			
1.01	0	0	0	0	0	0	0	2	0	2	0	
1.02	0	0	0	0	0	0	0	1	0	1	0	
1.03	0	0	0	0	0	0	0	0	0	0	0	
1.04	0	0	0	0	0	0	0	0	0	0	0	
1.05	0	0	0	0	0	0	0	0	0	0	0	
1.06	0	0	0	0	0	0	0	1	0	1	0	
1.07	0	0	0	0	0	0	0	1	1	1	1	
1.08	0	0	0	0	0	0	0	1	1	1	1	
1.09	0	0	0	0	0	0	0	1	1	1	1	
1.10	0	0	0	0	0	0	0	1	1	1	1	
1.11	0	0	0	0	0	0	0	1	1	1	1	
1.12	0	0	0	0	0	0	0	2	0	2	0	
1.13	0	0	0	0	0	0	0	3	0	3	0	
1.14	0	0	0	0	0	0	0	0	0	0	0	
1.15	0	0	0	0	0	0	0	1	0	1	0	
1.16	0	0	0	0	0	0	0	5	0	5	0	
1.17	0	0	0	0	0	0	0	4	0	4	0	
1.18	0	0	0	0	0	0	0	4	0	4	0	
1.19	0	0	0	0	0	0	0	1	0	1	0	
1.20	0	0	0	0	0	0	0	3	0	3	0	
1.21	0	0	0	0	0	0	0	1	2	1	2	
1.22	0	0	0	0	0	0	0	1	1	1	1	
1.23	0	0	0	0	0	0	0	1	0	1	0	
1.24	0	0	0	0	0	0	0	1	0	1	0	
1.25	0	0	0	0	0	0	0	3	1	3	1	
1.26	0	0	0	0	0	0	0	4	1	4	1	
1.27	0	0	0	0	0	0	0	4	0	4	0	
1.28	0	0	0	0	0	0	0	1	2	1	2	
1.29	0	0	0	0	0	0	0	1	0	1	0	
1.30	0	0	0	0	0	0	0	6	0	6	0	
1.31	0	0	0	0	0	0	0	2	0	2	0	
1.32	0	0	0	0	0	0	0	1	1	1	1	
1.33	0	0	0	0	0	0	0	0	0	0	0	
1.34	0	0	0	0	0	0	0	0	0	0	0	
1.35	0	0	0	0	0	0	0	0	0	0	0	
1.36	0	0	0	0	0	0	0	0	0	0	0	
1.37	0	0	0	0	0	0	0	0	0	0	0	
1.38	0	0	0	0	0	0	0	0	0	0	0	
1.39	0	0	0	0	0	0	0	0	0	0	0	
1.40	0	0	0	0	0	0	0	1	0	1	0	
1.41	0	0	0	0	0	0	0	2	0	2	0	
1.42	0	0	0	0	0	0	0	2	0	2	0	
1.43	0	0	0	0	0	0	0	4	0	4	0	
1.44	0	0	0	0	0	0	0	1	2	1	2	
1.45	0	0	0	0	0	0	0	1	0	1	0	
1.46	0	0	0	0	0	0	0	3	0	3	0	
1.47	0	0	0	0	0	0	0	4	0	4	0	
1.48	0	0	0	0	0	0	0	1	1	1	1	
1.49	0	0	0	0	0	0	0	1	1	1	1	
1.50	0	0	0	0	0	0	0	0	0	0	0	
SUBTOTAL								104	32	12	111	32

TOP SECRET

TABLE A-4

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.51												
1.52												
1.53												
1.54												
1.55												
1.56												
1.57												
1.58												
1.59												
1.60												
1.61												
1.62												
1.63												
1.64												
1.65												
1.66												
1.67												
1.68												
1.69												
1.70												
1.71												
1.72												
1.73												
1.74												
1.75												
1.76												
1.77												
1.78												
1.79												
1.80												
1.81												
1.82												
1.83												
1.84												
1.85												
1.86												
1.87												
1.88												
1.89												
1.90												
1.91												
1.92												
1.93												
1.94												
1.95												
1.96												
1.97												
1.98												
1.99												
2.00												
SUBTOTAL												

TOP SECRET

TABLE A-4

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.01	0	0	0	0	0	0	0	0	0	0	3	0
2.02	0	0	0	0	0	0	0	0	0	0	1	0
2.03	0	0	0	0	0	0	0	0	0	0	1	0
2.04	0	0	0	0	0	0	0	0	0	0	1	0
2.05	0	0	0	0	0	0	0	0	0	0	1	0
2.06	0	0	0	0	0	0	0	0	0	0	1	0
2.07	0	0	0	0	0	0	0	0	0	0	1	0
2.08	0	0	0	0	0	0	0	0	0	0	1	0
2.09	0	0	0	0	0	0	0	0	0	0	1	0
2.10	0	0	0	0	0	0	0	0	0	0	1	0
2.11	0	0	0	0	0	0	0	0	0	0	1	0
2.12	0	0	0	0	0	0	0	0	0	0	1	0
2.13	0	0	0	0	0	0	0	0	0	0	1	0
2.14	0	0	0	0	0	0	0	0	0	0	1	0
2.15	0	0	0	0	0	0	0	0	0	0	1	0
2.16	0	0	0	0	0	0	0	0	0	0	1	0
2.17	0	0	0	0	0	0	0	0	0	0	1	0
2.18	0	0	0	0	0	0	0	0	0	0	1	0
2.19	0	0	0	0	0	0	0	0	0	0	1	0
2.20	0	0	0	0	0	0	0	0	0	0	1	0
2.21	0	0	0	0	0	0	0	0	0	0	1	0
2.22	0	0	0	0	0	0	0	0	0	0	1	0
2.23	0	0	0	0	0	0	0	0	0	0	1	0
2.24	0	0	0	0	0	0	0	0	0	0	1	0
2.25	0	0	0	0	0	0	0	0	0	0	1	0
2.26	0	0	0	0	0	0	0	0	0	0	1	0
2.27	0	0	0	0	0	0	0	0	0	0	1	0
2.28	0	0	0	0	0	0	0	0	0	0	1	0
2.29	0	0	0	0	0	0	0	0	0	0	1	0
2.30	0	0	0	0	0	0	0	0	0	0	1	0
2.31	0	0	0	0	0	0	0	0	0	0	1	0
2.32	0	0	0	0	0	0	0	0	0	0	1	0
2.33	0	0	0	0	0	0	0	0	0	0	1	0
2.34	0	0	0	0	0	0	0	0	0	0	1	0
2.35	0	0	0	0	0	0	0	0	0	0	1	0
2.36	0	0	0	0	0	0	0	0	0	0	1	0
2.37	0	0	0	0	0	0	0	0	0	0	1	0
2.38	0	0	0	0	0	0	0	0	0	0	1	0
2.39	0	0	0	0	0	0	0	0	0	0	1	0
2.40	0	0	0	0	0	0	0	0	0	0	1	0
2.41	0	0	0	0	0	0	0	0	0	0	1	0
2.42	0	0	0	0	0	0	0	0	0	0	1	0
2.43	0	0	0	0	0	0	0	0	0	0	1	0
2.44	0	0	0	0	0	0	0	0	0	0	1	0
2.45	0	0	0	0	0	0	0	0	0	0	1	0
2.46	0	0	0	0	0	0	0	0	0	0	1	0
2.47	0	0	0	0	0	0	0	0	0	0	1	0
2.48	0	0	0	0	0	0	0	0	0	0	1	0
2.49	0	0	0	0	0	0	0	0	0	0	1	0
2.50	0	0	0	0	0	0	0	0	0	0	1	0
SUBTOTAL	0	0	0	0	0	0	0	24	32	0	24	32

TABLE A-4



DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			TOTAL		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
.51	0	0	0	0	0	0	0	0	0	0	0	0
.52	0	0	0	0	0	0	0	0	0	0	0	0
.53	0	0	0	0	0	0	0	0	0	0	0	0
.54	0	0	0	0	0	0	0	0	0	0	0	0
.55	0	0	0	0	0	0	0	0	0	0	0	0
.56	0	0	0	0	0	0	0	0	0	0	0	0
.57	0	0	0	0	0	0	0	0	0	0	0	0
.58	0	0	0	0	0	0	0	0	0	0	0	0
.59	0	0	0	0	0	0	0	0	0	0	0	0
.60	0	0	0	0	0	0	0	0	0	0	0	0
.61	0	0	0	0	0	0	0	0	0	0	0	0
.62	0	0	0	0	0	0	0	0	0	0	0	0
.63	0	0	0	0	0	0	0	0	0	0	0	0
.64	0	0	0	0	0	0	0	0	0	0	0	0
.65	0	0	0	0	0	0	0	0	0	0	0	0
.66	0	0	0	0	0	0	0	0	0	0	0	0
.67	0	0	0	0	0	0	0	0	0	0	0	0
.68	0	0	0	0	0	0	0	0	0	0	0	0
.69	0	0	0	0	0	0	0	0	0	0	0	0
.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	15	15	3	234	234	169	249	249	172

MISSION 1028-2		INSTR - AFT		2-11-66		PROCESSING AND EXPOSURE ANALYSIS				
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED				
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC				
INTERMEDIATE	15	0 PC	13 PC	40 PC	33 PC	13 PC				
FULL	234	50 PC	0 PC	44 PC	6 PC					
ALL LEVELS	249	47 PC	1 PC	44 PC	7 PC					
PROCESS LEVEL	BASE + FCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED				
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP				
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP				
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP				

~~TOP SECRET~~

TABLE A-4

MISSION # 102B-2

INSTR # APR 68 211-66

FLIGHT # TERRAIN # PROCESSING # INTER

ARITH MEAN # 0.52 # MEDIAN # 0.87 # STD DEV # 0.32 # RANGE # 0.27 TO 1.40 WITH 15 SAMPLES

20

18

16

14

12

10

8

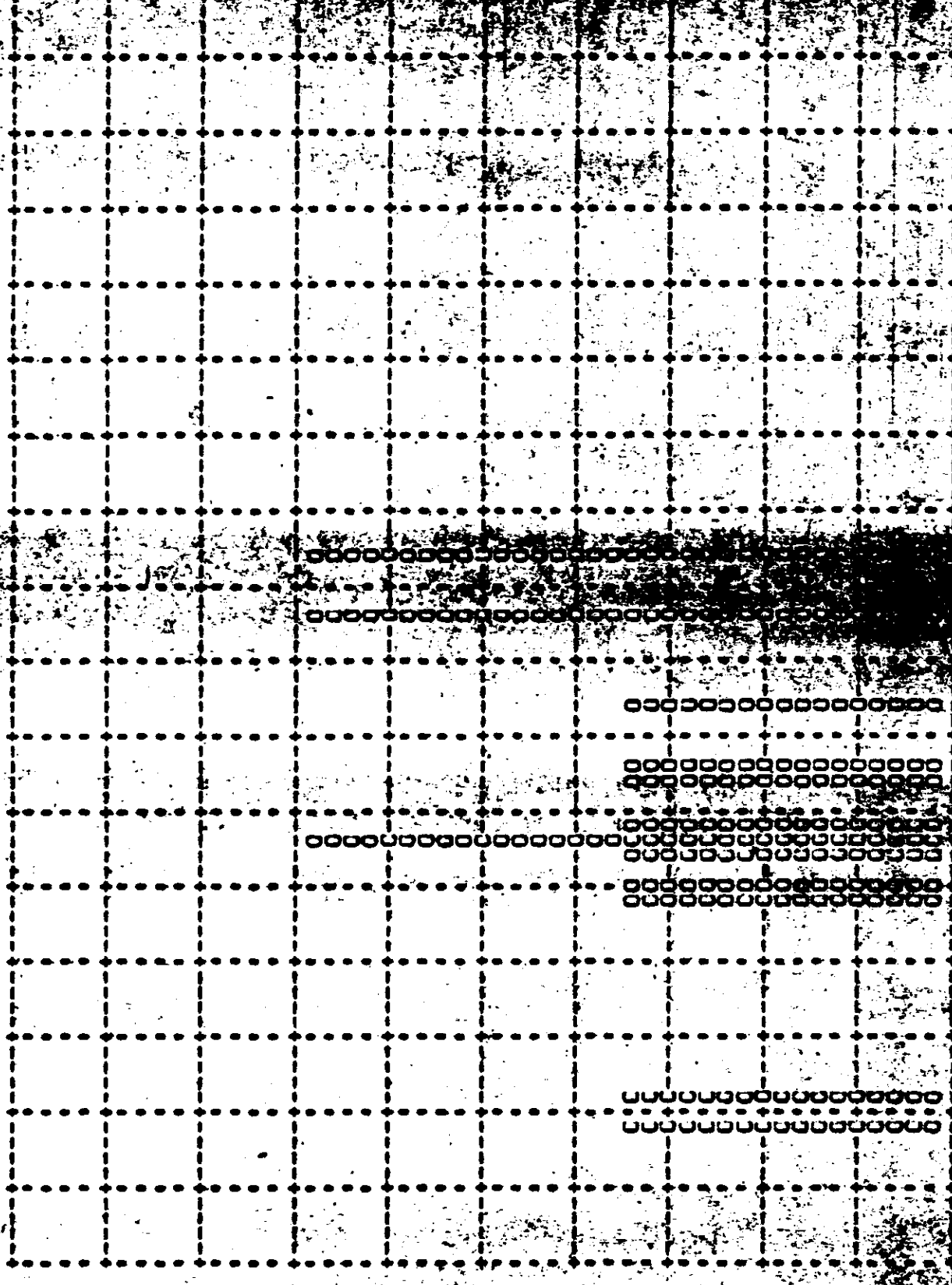
6

4

2

0

LEWIS & CLARK # BURDEN # TOTAL



2.1

1.6

1.1

0.6

0.1

0.6

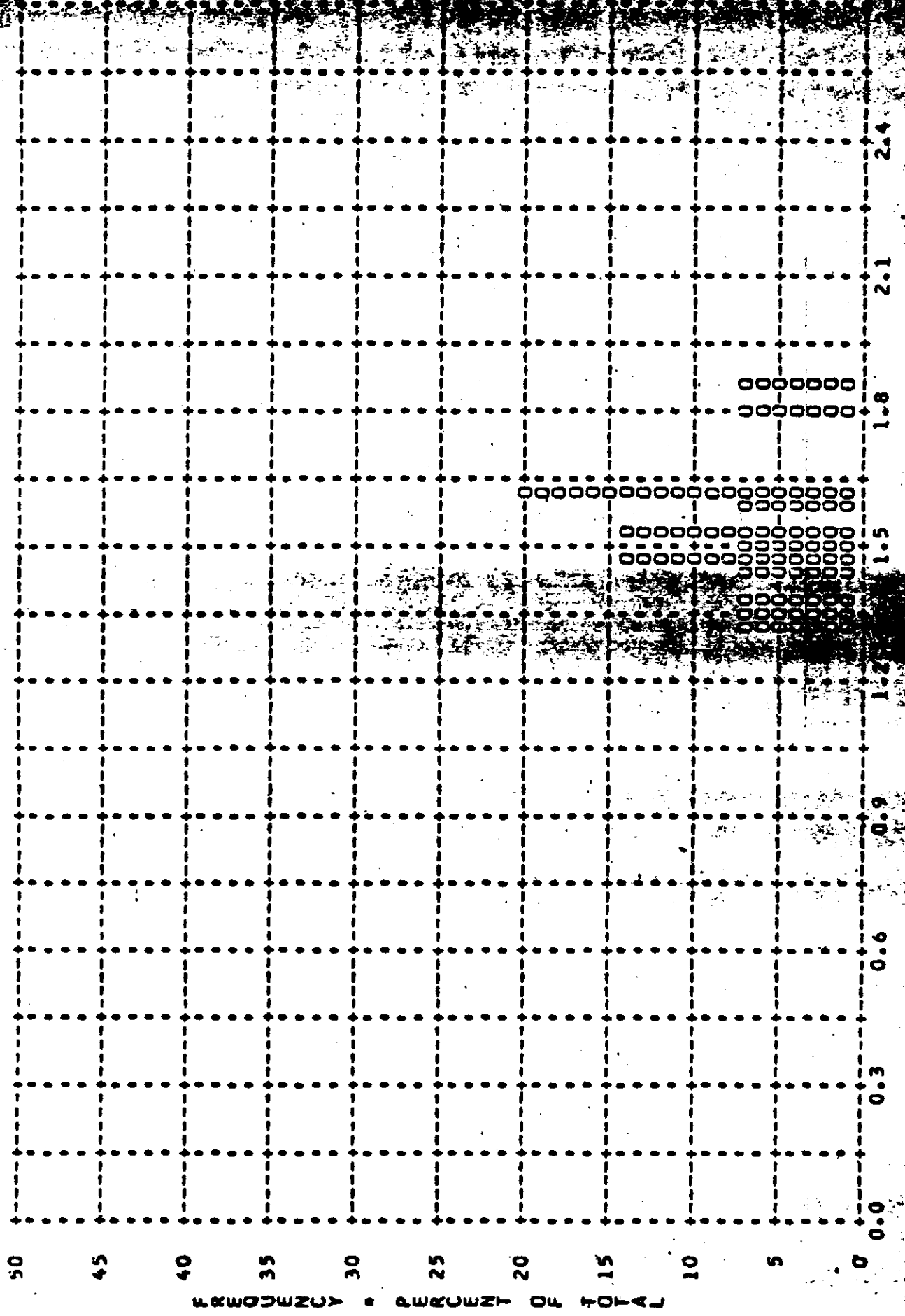
1.1

1.6

2.1

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • AFT • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE  
ARITH MEAN • 1.53 • MEDIAN • 1.52 • STD DEV • 0.15 • RANGE • 1.30 TO 1.86 WITH 15 SAMPLES

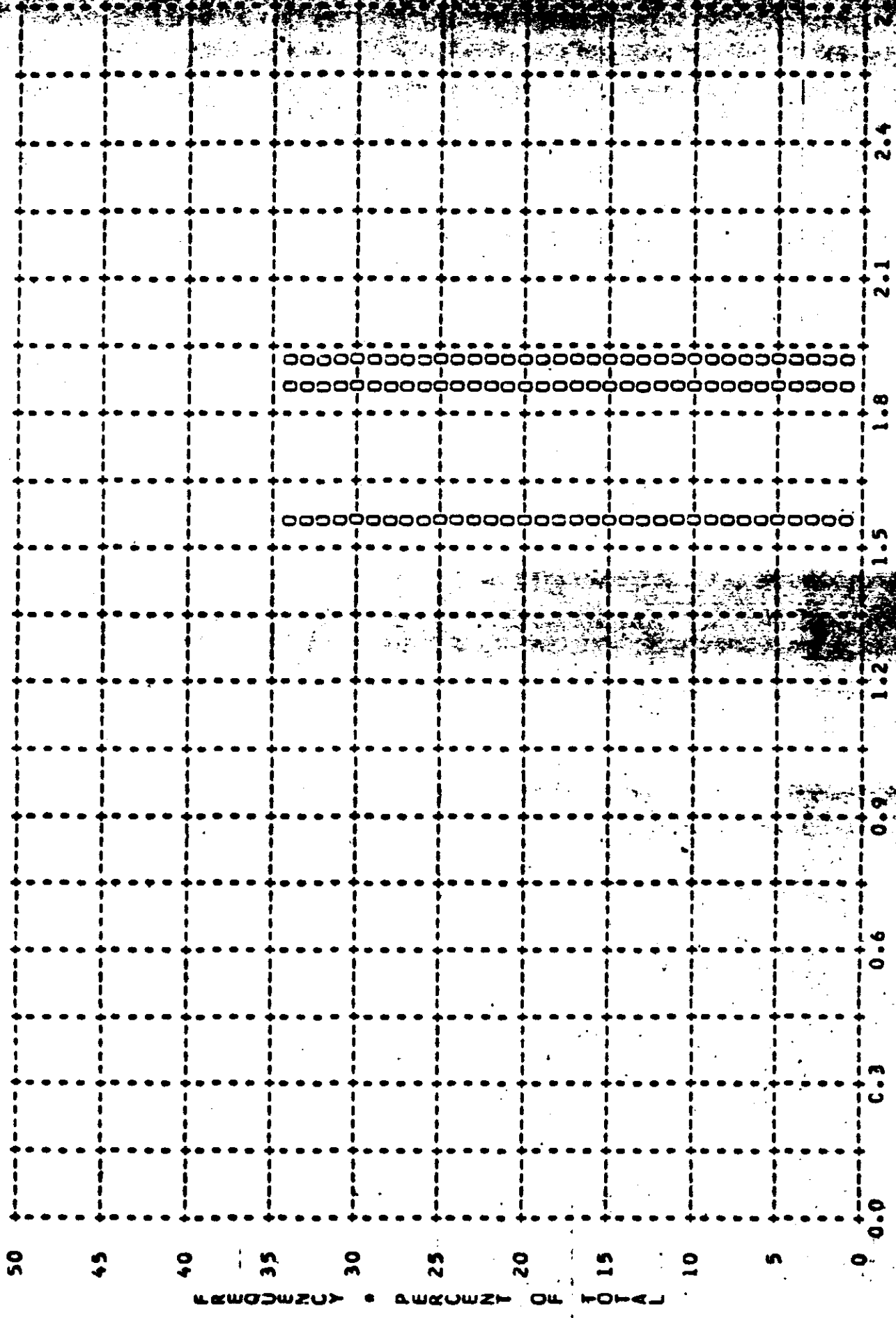


~~TOP SECRET~~

FIGURE A-30

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • AFT • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE  
ARITH MEAN • 1.78 • MEDIAN • 1.86 • STD DEV • 0.19 • RANGE • 1.56 TO 1.92 WITH 3 SAMPLES



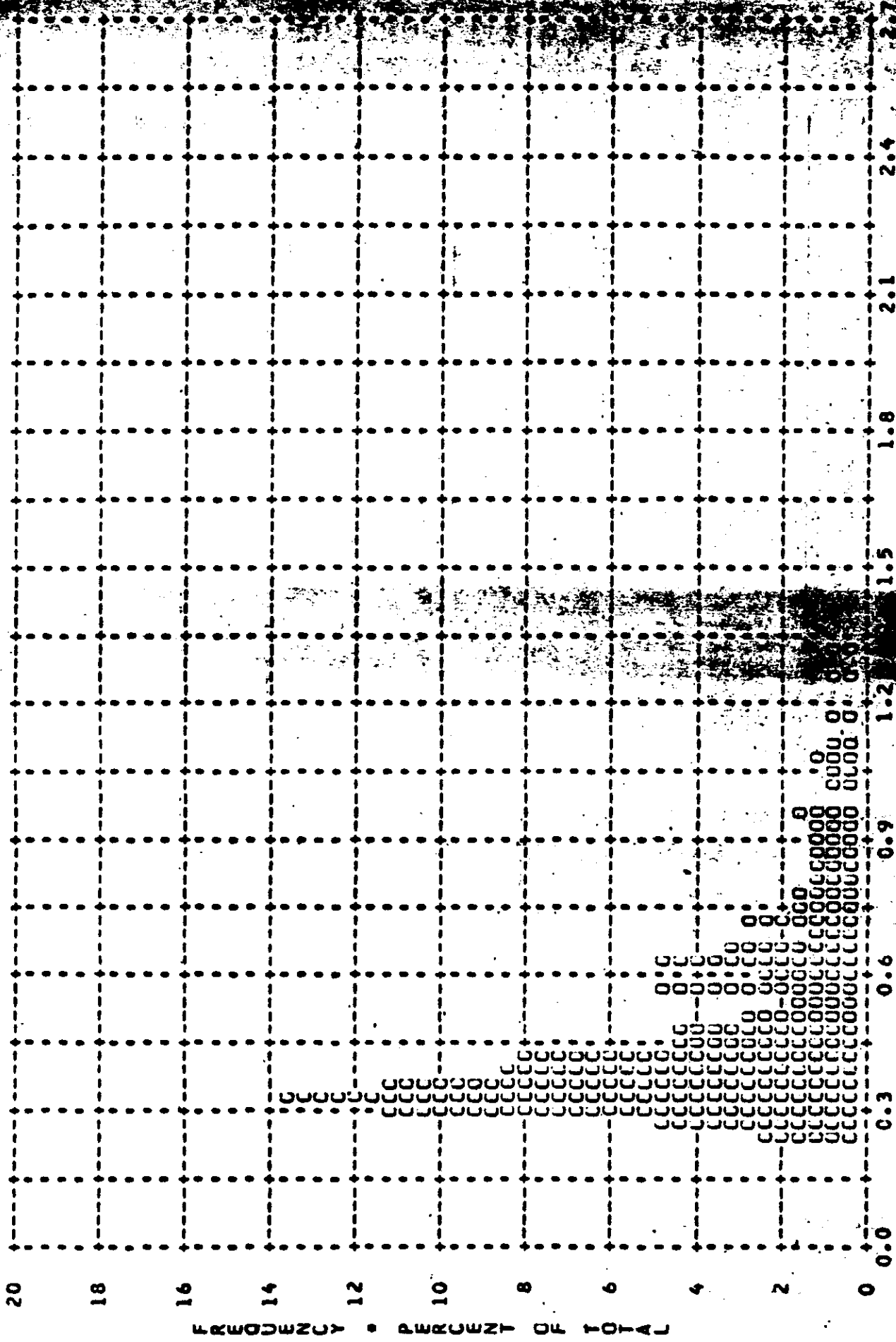
A-55

~~TOP SECRET~~

FIGURE A-31

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • AFT • 2-11-66 PLOT OF U MIN • TERRAIN • PROCESSING • FULL  
ARITH MEAN • 0.47 • MEDIAN • 0.39 • STD DEV • 0.21 • RANGE • 0.22 TO 1.30 WITH 234 SAMPLES

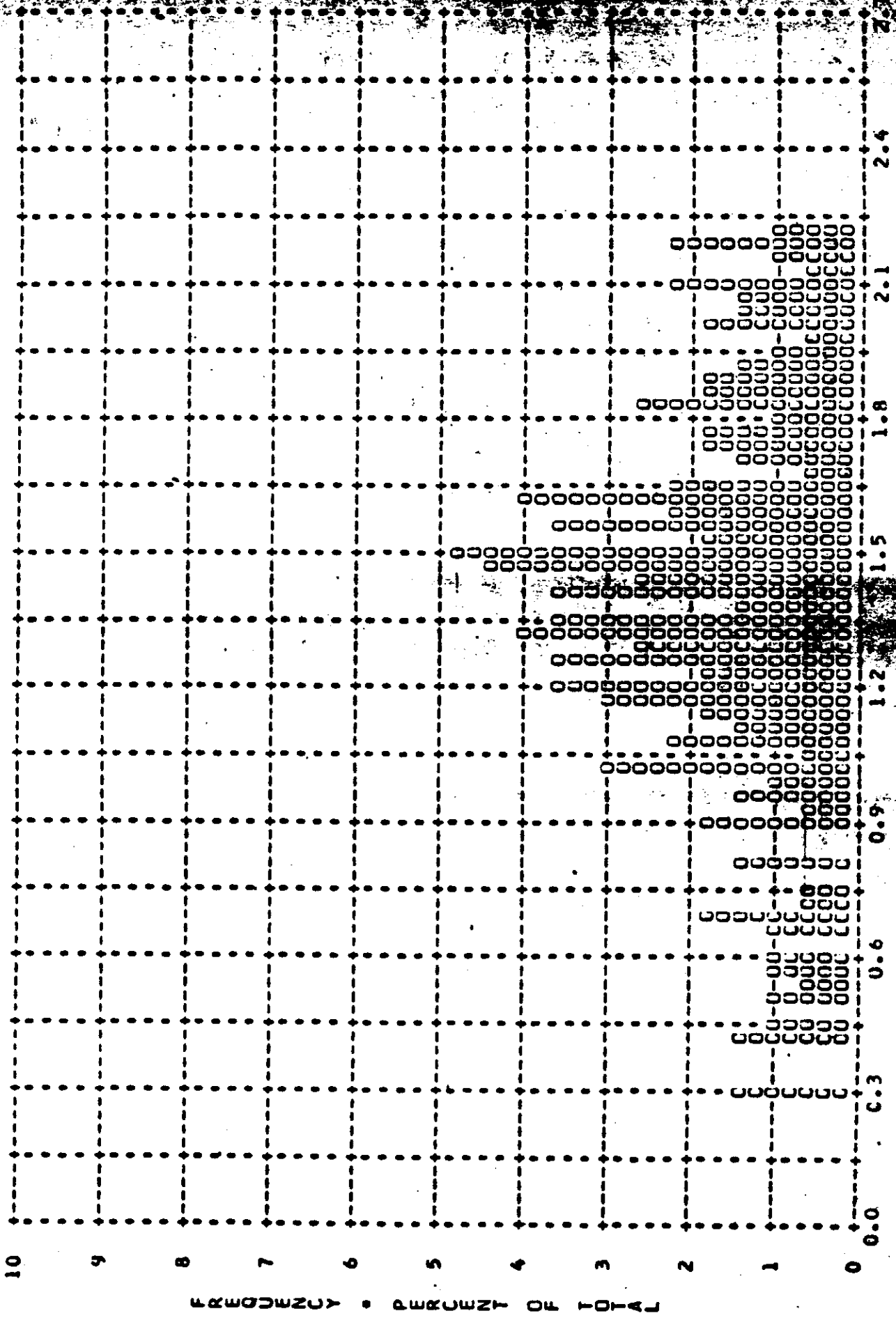


~~TOP SECRET~~

FIGURE A-32

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • AFT • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • FULL  
ARITH MEAN • 1.39 • MEDIAN • 1.42 • STD DEV • 0.44 • RANGE • 0.28 TO 2.21 WITH 234 SAMPLES



~~TOP SECRET~~

FIGURE A-33

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • AFI • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • FULL  
ARITH MEAN • 1.69 • MEDIAN • 1.75 • STD DEV • 0.40 • RANGE • 0.30 TO 2.35 WITH 169 SAMPLES

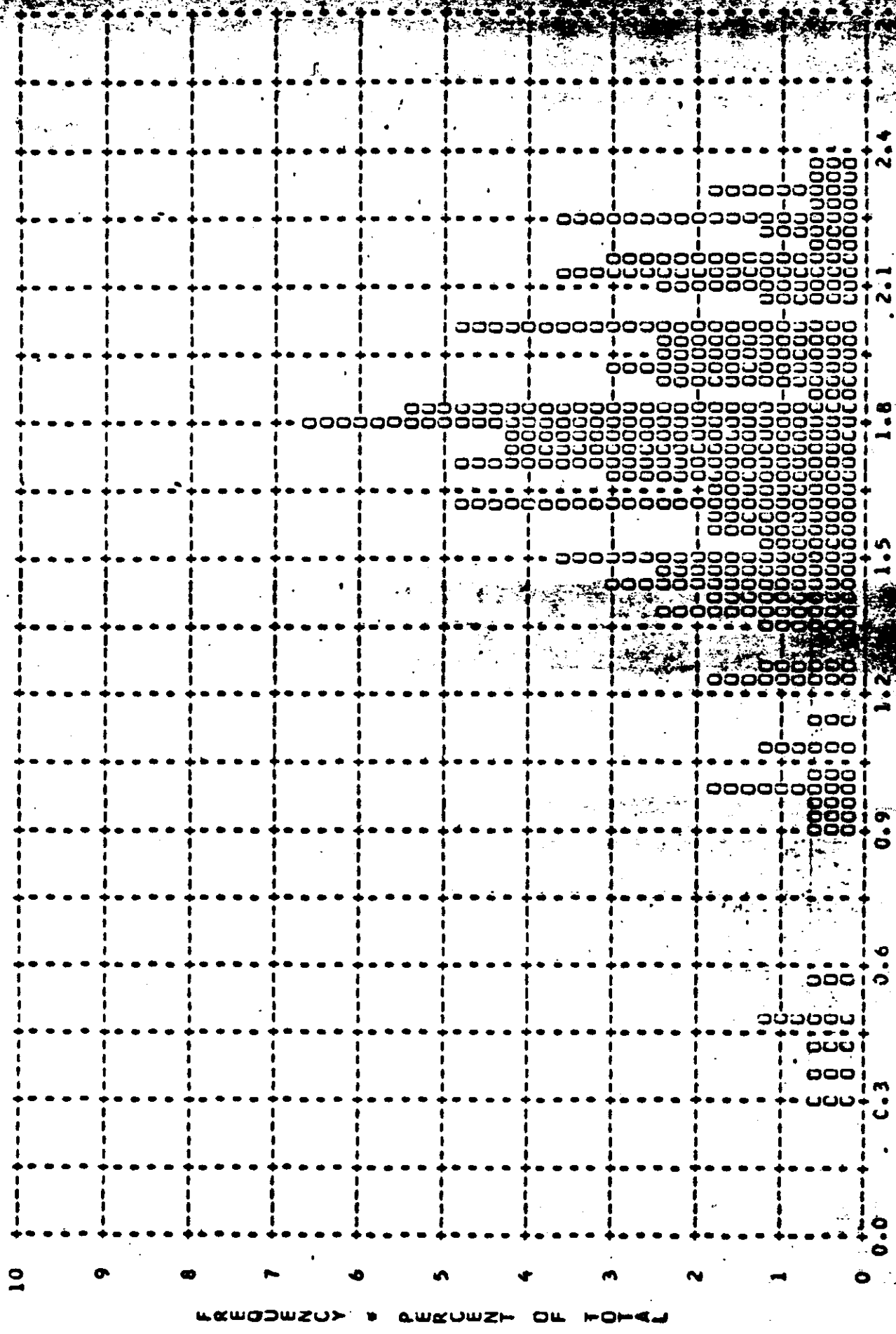
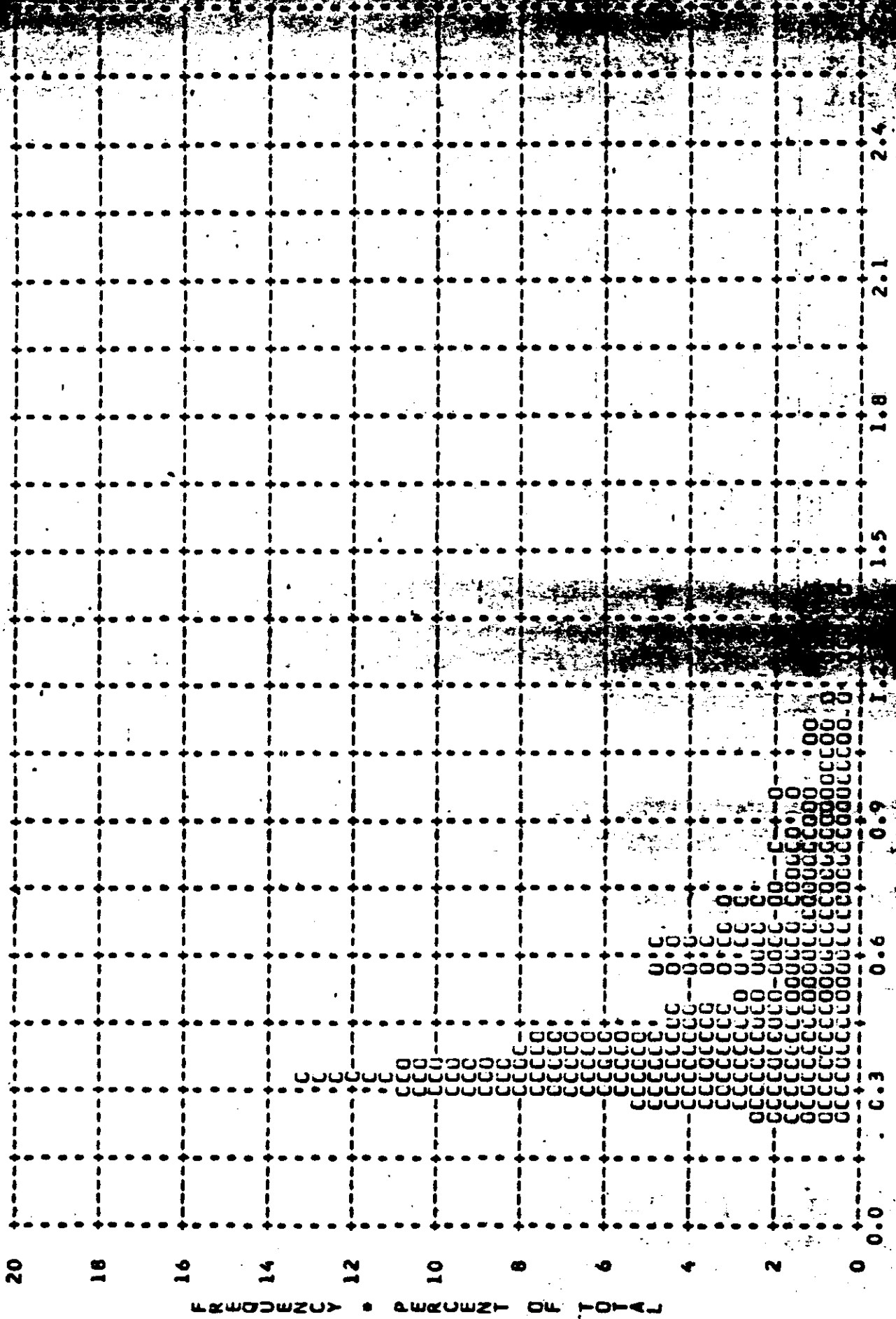


FIGURE A-34

~~TOP SECRET~~

~~TOP SECRET~~

MISSION • 1028-2 • INSTR • AFT • 2-11-66 PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • 0.50 • MEDIAN • 0.40 • STD DEV • 0.24 • RANGE • 0.22 TO 1.40 WITH 249 SAMPLES



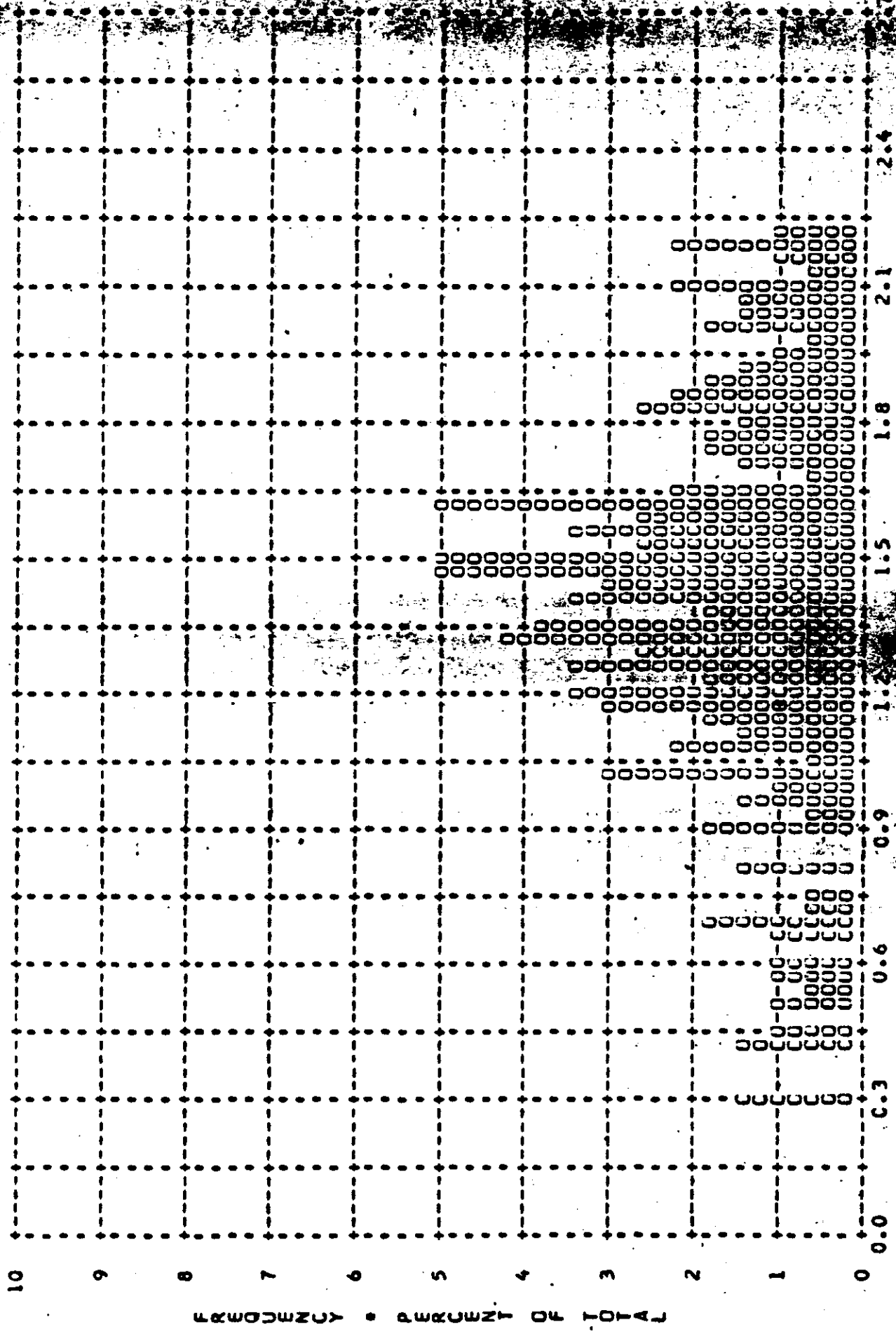
~~TOP SECRET~~

FIGURE A-35



~~TOP SECRET~~

MISSION • 1G28-2 • INSTR • AFT • 2-11-66 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS  
ARITH MEAN • 1.43 • MEDIAN • 1.43 • STD DEV • 0.42 • RANGE • 0.28 IG 2.21 WITH 249 SAMPLES

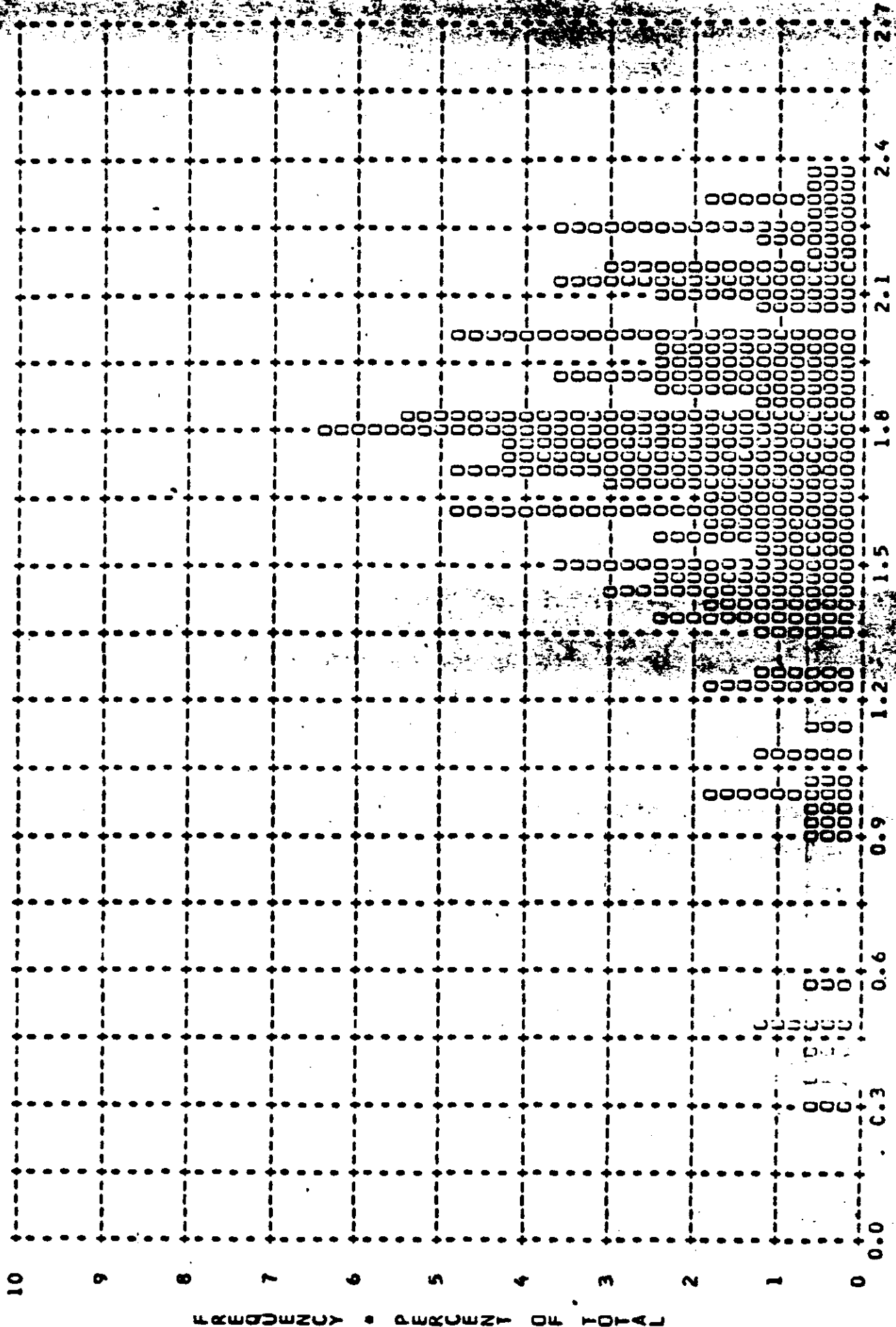


A-60

~~TOP SECRET~~

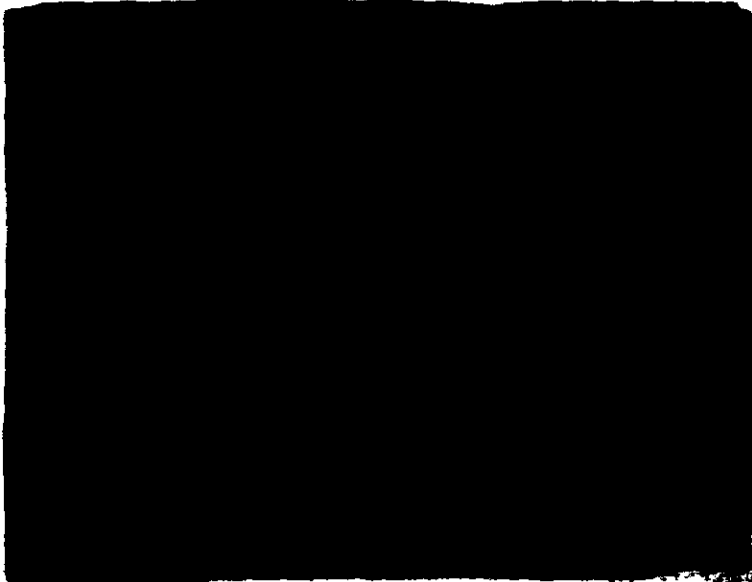
FIGURE A-38

MISSION • 102H-2 • INSTR • AFT • 2-11-66 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS  
 ARITH MEAN • 1.65 • MEDIAN • 1.75 • STD DEV • 0.40 • RANGE • 0.30 TO 2.35 WITH 172 SAMPLES



~~TOP SECRET~~ [REDACTED]

Distribution:



~~TOP SECRET~~ [REDACTED]